

T.C.
İSTANBUL VALİLİĞİ
İSTANBUL PROJE KOORDİNASYON BİRİMİ
(İPKB)

Proje Müşaviri

OPTIMAL PROJE YÖNETİMİ



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İşin Adı

İSTANBUL ÜNİVERSİTESİ CERRAHPAŞA AVCILAR YERLEŞKESİ
YURT BİNALARI

	Adı Soyadı	Meslek	Oda Sicil No	İmza
Yapan	AHMET HABERDAR	İnşaat Mühendisi	79793	
Çizen	VILDAN BAKKAL	Teknik Ressam	---	
Kontrol Eden	ÖZGÜR ŞENTÜRK	İnşaat Mühendisi	71647	
Proje Müdürü	ALİ FUAT EYÜBOĞLU	İnşaat Mühendisi	78486	

Proje Adı	İSTANBUL ÜNİVERSİTESİ CERRAHPAŞA AVCILAR YERLEŞKESİ YURT BİNALARI	PARSEL	-
Aşama	YAĞMUR SUYU DEPOSU STATİK UYGULAMA PROJESİ		
Çizim no.			
Ölçek	1/50 - 1/25	Teslim Tarihi	09/2025

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DÖŞEME YÜK ANALİZİ

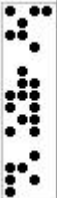
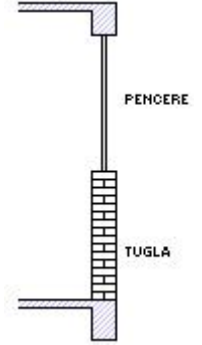
MARLEY KAPLAMA				
Kaplama (MARLEY)	0.050 t/m ³ ×	0.003 m	:	0.000
Kaplama harcı	2.200 t/m ³ ×	0.020 m	:	0.044
Tesviye betonu	2.000 t/m ³ ×	0.030 m	:	0.060
Sıva	2.200 t/m ³ ×	0.020 m	:	0.044
TOPLAM.....				0.148
FAYANS KAPLAMA				
Kaplama (FAYANS)	2.200 t/m ³ ×	0.010 m	:	0.022
Kaplama harcı	2.200 t/m ³ ×	0.020 m	:	0.044
Tesviye betonu	2.000 t/m ³ ×	0.030 m	:	0.060
Sıva	2.200 t/m ³ ×	0.020 m	:	0.044
TOPLAM.....				0.170
KARO KAPLAMA				
Kaplama (KARO MOZAİK)	2.200 t/m ³ ×	0.020 m	:	0.044
Kaplama harcı	2.200 t/m ³ ×	0.020 m	:	0.044
Tesviye betonu	2.000 t/m ³ ×	0.040 m	:	0.080
Sıva	2.200 t/m ³ ×	0.020 m	:	0.044
TOPLAM.....				0.212
DUSUK DOSEME				
Kaplama (FAYANS)	2.200 t/m ³ ×	0.010 m	:	0.022
Kaplama harcı	2.200 t/m ³ ×	0.030 m	:	0.066
Tesviye betonu	2.000 t/m ³ ×	0.050 m	:	0.100
Sıva	2.200 t/m ³ ×	0.020 m	:	0.044
Dolgu	1.500 t/m ³ ×	0.200 m	:	0.300
TOPLAM.....				0.532
CATI DOSEMESI				
Kaplama (IZOLASYON)	0.100 t/m ³ ×	0.050 m	:	0.005
Tesviye betonu	2.000 t/m ³ ×	0.050 m	:	0.100
Sıva	2.200 t/m ³ ×	0.020 m	:	0.044
TOPLAM.....				0.149
MERDIVEN				
Kaplama (MERMER)	2.200 t/m ³ ×	0.020 m	:	0.044
Kaplama harcı	2.200 t/m ³ ×	0.020 m	:	0.044
Sıva	2.200 t/m ³ ×	0.020 m	:	0.044
Dolgu	2.200 t/m ³ ×	0.100 m	:	0.220
TOPLAM.....				0.352
SAHANLIK				
Kaplama (MERMER)	2.200 t/m ³ ×	0.020 m	:	0.044
Kaplama harcı	2.200 t/m ³ ×	0.020 m	:	0.044
Tesviye betonu	2.000 t/m ³ ×	0.030 m	:	0.060
Sıva	2.200 t/m ³ ×	0.020 m	:	0.044
TOPLAM.....				0.192

(Döşeme zatipleri, döşeme yük hesabında ilave edilecek)

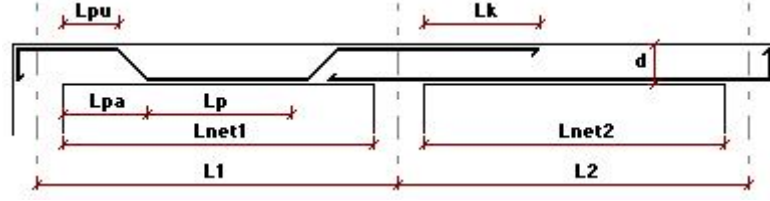
KIRIŞ YÜK ANALİZİ

19cm Tugla Duvar yükü (19 cm)	0.320 t/m ² × 2.500 m:	0.800
13cm Tugla Duvar yükü (13 cm)	0.250 t/m ² × 2.500 m:	0.625
9cm Tugla Duvar yükü (9 cm)	0.200 t/m ² × 2.500 m:	0.500
19cm Tug. pen Duvar yükü (19 cm)	0.320 t/m ² × 1.000 m:	0.320
Pencere	0.050 t/m ² × 1.500 m:	0.075
TOPLAM.....		0.395
13cm Tug. pen Duvar yükü (13 cm)	0.250 t/m ² × 1.000 m:	0.250
Pencere	0.050 t/m ² × 1.500 m:	0.075
TOPLAM.....		0.325
9cm Tug. pen. Duvar yükü (9 cm)	0.200 t/m ² × 1.000 m:	0.200
Pencere	0.050 t/m ² × 1.500 m:	0.075
TOPLAM.....		0.275
Cam Bolme Duvar yükü (2 cm)	0.050 t/m ² × 2.700 m:	0.135
25cm Tugla Duvar yükü (25 cm)	0.380 t/m ² × 2.500 m:	0.950
20cm GazBeton Duvar yükü (20 cm)	0.190 t/m ² × 2.500 m:	0.475
15cm GazBeton Duvar yükü (15 cm)	0.160 t/m ² × 2.500 m:	0.400
10cm GazBeton Duvar yükü (10 cm)	0.130 t/m ² × 2.500 m:	0.325
20cm GazB.pen. Duvar yükü (20 cm)	0.190 t/m ² × 1.000 m:	0.190
Pencere	0.050 t/m ² × 1.500 m:	0.075
TOPLAM.....		0.265
15cm GazB.pen. Duvar yükü (15 cm)	0.160 t/m ² × 1.000 m:	0.160
Pencere	0.050 t/m ² × 1.500 m:	0.075
TOPLAM.....		0.235
10cm GazB.pen. Duvar yükü (10 cm)	0.130 t/m ² × 1.000 m:	0.130
Pencere	0.050 t/m ² × 1.500 m:	0.075
TOPLAM.....		0.205
Panel duvar Duvar yükü (5 cm)	0.050 t/m ² × 2.700 m:	0.135
25cm GazBeton Duvar yükü (25 cm)	0.216 t/m ² × 2.500 m:	0.540
10cm FabrikPan. Duvar yükü (10 cm)	0.130 t/m ² × 2.500 m:	0.325
40cm Tas duvar Duvar yükü (40 cm)	1.098 t/m ² × 1.000 m:	1.098

(Kiriş zati, Kiriş yük hesabında ilave edilecek)



GENEL BETONARME CIZIM OPSİYONLARI

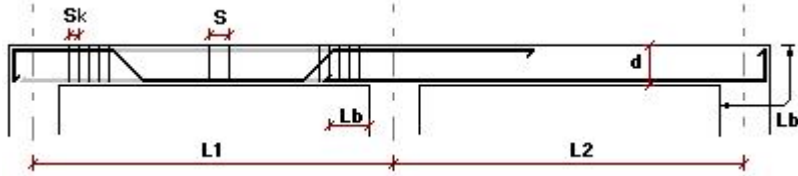


Maximum demir boyu.....cm.= 1200
 Minimum demir bindirme boyu oranı.....= $\emptyset \times 50$
 min. Lp.....= Lnet1 / 2
 Lpa.....= Lnet1 / 5
 min. Lpu.....cm.= 30
 min. Lpu= d / 2
 min. Lk= Lnet2 / 4
 Pilye kayma donatısı katılım oranı.....= 0
 Genel kanca boyu= $\emptyset \times 10$
 Kiriş donatısının, kolon içindeki aderans boyu.....= $\emptyset \times 50$
 Kirişlerde sık etriye opsiyonu.....= zorunlu
 Kirişlerde Pilye opsiyonu.....= pilyesiz
 Minimum pilye açıklık oranı.....= Lnet/2
 Tek donatılarda, pilye ve düz donatı tercihi.....= düz
 Kirişlerde minimum iki demir aralığı.....cm.= 2.5

DOSEME BETONARME OPSİYONLARI

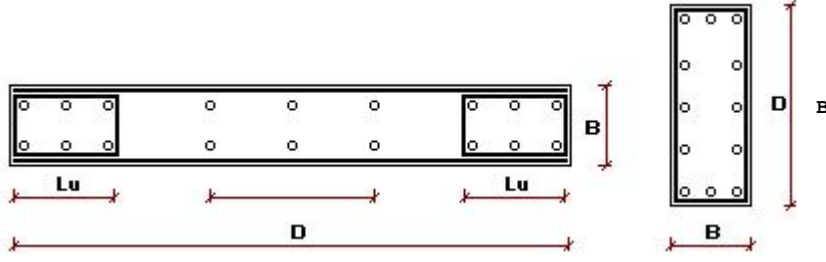
Plaklarda paspayı.....cm.= 3
 Maksimum demir aralığı.....cm.= 20, d x 1,5
 İki yonlu plak-minimum çekme bölgesi pürsantaji = 0.002
 Tek yonlu plak-minimum çekme bölgesi pürsantaji = 0.003
 Nervur Max. Etriye aralığı.....cm.= 20, d/2
 Lk : üst donatı uzatma boyu.....cm.= 50 $\emptyset$, Ln/4

KIRIS BETONARME OPSİYONLARI



Etriye paspayı / Boyuna donatı paspayıcm.= 3,5 / 5
 Maksimum sehım sınırı (bölme duvarsız)= L / 360
 Maksimum sehım sınırı (bölme duvarlı)= L / 240
 Min. çekme bölgesi TS500-2000 'e göre= 0.003
 As min= 0.8 x fctd / fyd alınacaktır.
 Minimum düz ve pilye donatı çapı $\emptyset$. = 12
 Minimum montaj donatı çapı $\emptyset$. = 12
 Minimum gövde donatı çapı $\emptyset$. = 12
 Minimum etriye donatı çapı $\emptyset$. = 8
 Pilye açısı..... $^{\circ}$. = 45
 Minimum gövde demirsiz kiriş yüksekliği.....cm.= 59
 Minimum düz ve montaj demir aralığıcm.= 20
 Kayma donatısı beton katılım oranı.....= .8
 Süreklilik için max. kolon genişliği.....cm.= 200
 Minimum montaj donatı oranı(% maxAs). = .25
 Maksimum etriye aralığı..S.....cm.= 20
 Minimum etriye aralığı..S.....cm.= 10
 Maksimum etriye aralığı. Sk.(1).....cm.= 15
 Maksimum etriye aralığı. Sk.(2).....= d/4
 Maksimum etriye aralığı. Sk.(3).....= $\emptyset \times 8$
 Maksimum tek etriye genişliğicm.= 40
 min.(alt As/üst As)= .5
 min.üst As== 0,8 x fctd / fyd
 min Lb =.....= $\emptyset \times 50$
 Alt ilaveye, düz donatıları L/4 uzatarak katılımı.....= Hayır
 Üst ilaveye, montaj donatı. L/4 uzatarak katılımı.....= Hayır

KOLON-PERDE BETONARME OPSİYONLARI



KOLON ve PERDELERİN betonarme opsiyonları :

Etriye paspayı / Boyuna donatı paspayıcm.= 3,5 / 5

Min.kolon çekme bölgesi.....= .002

Min.kolon toplam kesit= .01

Kolon eksenel yük eksantirisite etkisinin alınması..= evet

Minimum etriye aralığı.....cm.= 10

Maximum etriye aralığı.(1).....cm.= 20

Maximum etriye aralığı (2).....min.= $\emptyset \times 12$

Minimum çiroz aralığı.....min.= $\emptyset \times 25$

Minimum donatı çapı= 14

Minimum etriye çapı= 8

Perde/Kolon oranı (D/B).....= 6

Perde uzun etriyelerinde gönye.....= Gönyeli

Nervürlü etriye kanca açısı..... (90°,135°)= 135

min.Hcr yüksekliği< D x 2

max.Hcr yüksekliği>= D x 1

max.Hcr yüksekliği>= Hw/6

Min.başlık bölgesi.(Hcr).....= .002

Min.başlık bölgesi.....= .001

Min.gövde bölgesi.....= .0025

Min.başlık bölgesi.....Lu= 20 cm

Min.başlık bölgesi.(Hcr).....Lu=B x 2

Min.başlık bölgesi.(Hcr).....Lu=D x .2

Min.başlık bölgesi.....Lu=B x 1

Min.başlık bölgesi.....Lu=D x .1

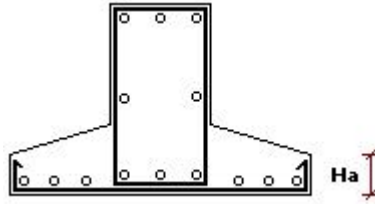
Başlık bölgesi min. donatı çapı= 14

Gövde bölgesi min. donatı çapı= 12

Perdelerde tasarım eğilme momenti.....= Evet

Kolonlarda minimum iki demir aralığı.....cm.= 4.0

TEMEL BETONARME OPSİYONLARI



Etriye paspayı / Boyuna donatı paspayıcm.= 5,5 / 7

Min. çekme bölgesi TS500-2000 (As min=0,8.fctd/fyd).= 0.003

Min. toplam kesit= .005

Minimum basınç bölgesi donatı oranı= .333

Pilye açısı.....= 60

Minimum etriye aralığı.....cm.= 10

Maximum etriye aralığı.....cm.= 20

Maximum etriye genişliği.....cm.= 60

Minimum düz ve montaj demir aralığıcm.= 20

Temelde, Kolon donatı filiz boyu.....cm.= 50

Müt. temel min. etriye çapı.....= 8

Müt. temel min. düz ve pilye çapı.....= 12

Müt. temel min. montaj çapı.....= 12

Müt. temel min. gövde çapı.....= 12

Temel min. ampatman çapı.....= 12

Ampatman kenar yüksekliği.(Ha).....cm.= 20

STA4-CAD PROGRAMI

ÇOK KATLI BETONARME YAPILARIN STATİK ve BETONARME ANALİZ PROGRAMI Ver.14.1 Rev.(5.6.2025)

PROJE İSMİ.....: CERRAHPAŞA YURT SU DEPOSU
 KAT ADEDİ.....: 1
 Bir kattaki KOLON SAYISI.....: 15
 X yönü aks sayısı.....: 9
 Y yönü aks sayısı.....: 5
 DEPREM YER HAREKETİ DÜZEYİ.....: DD2 50 yılda aşılma olasılığı %10
 ZEMİN SINIFI.....: ZD
 BİNA KOORDİNATI..... (ENLEM/BOYLAM) : 40.98416° / 28.72894°
 YEREL SPECTRAL İVME KATSAYISI..... S_s/S₁ : 1.250 / 0.338
 YAPI DAVRANIŞ KATSAYISI..... R : 8.00
 SİSTEM DAYANIM FAZLALIĞI KATSAYISI..... D ...: 3
 SPEKTRUM KAREKTERİSTİK PERYODU..... (Ta/Tb) : 0.107 / 0.533
 HAREKETLİ YÜK KATSAYISI.....(n)...: 0.8
 SIFIR RÖLATİF HAREKET YÜKSEKLİĞİ..... (m)...: 4.50
 HAREKETLİ YÜK AZALTMA KATSAYISI.....(Cz)...: 0.0
 ZEMİN TAŞIMA GÜCÜ TASARIM GERİLMESİ. (t/m²)...: 38.0
 ZEMİN YATAK KATSAYISI..... (t/m³)...: 2000.0
 BETON YOĞUNLUĞU.....(t/m³)...: 2.5
 GENLEŞME ISI FARKI.....(°C)...: 0.0
 STATİK ANALİZ YÖNTEMİ: FEA3D LINEER ANALİZ / Birim Mesh Genisliği 1m
 DEPREM STANDARDI: TBDY2018 CODE
 BETONARME HESAP YÖNTEMİ: TAŞIMA GÜCÜ YÖNTEMİ TS500-2000
 BETONARME KESİT DONATI HESAP YÖNTEMİ: BRÜT KESİTE GÖRE
 DEPREM HESABI YÖNTEMİ: MOD SÜPERPOZİSYONU İLE MODAL ANALİZ
 TEMEL ANALİZ OPSİYONU.....: TEMELLER DİKKATE ALINMADAN, YAPI ANALİZİ
 Zemin gerilmesi hareketli yük azaltma değeri..: 1.00
 Kolonun oturduğu kiriş tesir çarpanı.....: Düşey deprem analizi yapılmıştır.
 Kiriş & Kolon rijitlik bölgesi opsiyonu.....: Yarı Sonsuz Rijit davranış
 Kiriş uçlarında elastik ankastrelik opsiyonu : Elastik ankastre

STA4CAD CERTIFICATE

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ÇATLAMIS KESİT ETKİN KESİT RİJİTLİĞİ BİLGİLERİ

Elemanlar	Eğilme	Eksenel	Lokal X kesme	Lokal Y kesme
Perde	0.25	0.50	0.50	1.00
Bodrum perdesi	0.50	0.80	0.50	1.00
Döşeme	0.25	0.25	0.25	1.00
Çerçeve kirişi	0.35	1.00	1.00	1.00
Çerçeve kolonu	0.70	1.00	1.00	1.00
Bağ kirişi	0.15	1.00	1.00	1.00
Perde çubuk	0.50	1.00	0.50	0.50

BETON ve ÇELİK MALZEME BİLGİLERİ

(kg/cm²)

Yapı Elemanı	Malzeme	Elastisite Modülü E G		Beton dayanım gerilmesi	Çelik akma (Genel)	gerilmesi (Etriye)	Birim Ağırlık t/m³	
Plak/Nervür	E1	C35	332000	132800	350	4200	4200	2.50
HNP		C35	332000	132800	350	4200	4200	2.50
Temel	E1	C35	332000	132800	350	4200	4200	2.50
Kiriş\Kolon	E1	C35	332000	132800	350	4200	4200	2.50

HNP : Hazır Nervürlü Plak

TAŞIMA GÜCÜ MALZEME KATSAYILARI	BETON 1.50	ÇELİK 1.15
TAŞIMA GÜCÜ YÜK KATSAYILARI	SABİT YÜK 1.40	HAREKETLİ YÜK 1.60

BETONARME HESAP YÜK KOMBİNASYONU

Ölü yük Cg	Hareketli yük Cq	Zemin Cs	Deprem ± Ce	Rüzgar ± Cw	Isı Ct
1.40	1.60	0.00	0.00	0.00	0.00
1.40	1.60	1.60	0.00	0.00	0.00
1.00	1.20	0.00	0.00	0.00	1.20
1.00	1.00	0.00	1.00	0.00	0.00
1.00	1.00	1.00	1.00	0.00	0.00
0.90	0.00	0.00	1.00	0.00	0.00
1.00	1.30	0.00	0.00	1.30	0.00
1.00	1.30	1.00	0.00	1.30	0.00
0.90	0.00	0.00	0.00	1.30	0.00
0.90	0.00	0.90	0.00	1.30	0.00

TBDY2018 Düşey Deprem Kombinasyonu : G + Q + 0.2 S + Edh + 0.3 Edz, 0.9 G + H + Edh - 0.3 Edz
CODE:TS500T.COD

ZEMİN GERİLMESİ YÜK KOMBİNASYONU $q_0 < q_t$

ZEMİN GERİLMESİ OPSİYONU:ZEMİN TAŞIMA GÜCÜ TASARIM GERİLMESİ

Ölü yük Cg	Hareketli yük Cq	Zemin Cs	Deprem ± Ce	Rüzgar ± Cw	Isı Ct
1.40	1.60	0.00	0.00	0.00	0.00
1.40	1.60	1.60	0.00	0.00	0.00
1.00	1.20	0.00	0.00	0.00	1.20
1.00	1.00	0.00	1.00	0.00	0.00
1.00	1.00	1.00	1.00	0.00	0.00
0.90	0.00	0.00	1.00	0.00	0.00
1.00	1.30	0.00	0.00	1.30	0.00
1.00	1.30	1.00	0.00	1.30	0.00
0.90	0.00	0.00	0.00	1.30	0.00
0.90	0.00	0.90	0.00	1.30	0.00

RÜZGAR YÜKÜ VE KATSAYILARI

RÜZGAR YÜKÜ BASINÇ KATSAYISI : 0.8

RÜZGAR YÜKÜ EMME KATSAYISI : 0.4

Yükseklik bölgesi	H	Qw
1. bölge	8.00	0.05
2. bölge	20.00	0.08
3. bölge	100.00	0.11

YAPI AKS BİLGİLERİ

X yönü aks bilgileri

no	isim	Ax	Bx
1	1	0.00	-5.50
2		0.00	-19.20
3		0.00	-14.60
4		0.00	-5.00
5		0.00	-14.00
6		0.00	-8.80
7	3	0.00	-11.50
8	2	0.00	-16.50
9	4	0.00	-7.30

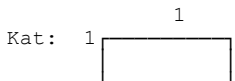
Y yönü aks bilgileri

no	isim	Ay	By
1	C	0.00	7.60
2		0.00	16.20
3		0.00	9.40
4		0.00	7.10
5		0.00	15.70

1. KAT KOLONLARI AKS BİLGİLERİ

Kolon no	X aksı	Y aksı	dx	dy	alt yük.
101	2X	1Y	-0.1	-0.1	0.00
103	5X	1Y	0.0	-0.1	0.00
105	6X	1Y	0.1	-0.1	0.00
107	1X	1Y	0.1	-0.1	0.00
109	1X	3Y	0.1	-0.1	0.00
111	8X	2Y	0.0	0.1	0.00
113	7X	2Y	0.0	0.1	0.00
115	1X	2Y	0.1	0.1	0.00

Kolon no	X aksı	Y aksı	dx	dy	alt yük.
102	8X	1Y	0.0	-0.1	0.00
104	7X	1Y	0.0	-0.1	0.00
106	9X	1Y	-30.0	-0.1	0.00
108	6X	3Y	0.1	-0.1	0.00
110	2X	2Y	-0.1	0.1	0.00
112	5X	2Y	0.0	0.1	0.00
114	6X	2Y	0.1	0.1	0.00

KAT DIYAFRAMLARI

DEPREM RAPORU

DEPREM STANDARDI : TBDY2018 CODE
 DEPREM ANALİZİ : MOD SÜPERPOZİSYONU İLE MODAL ANALİZ
 DEPREM YER HAREKETİ DÜZEYİ : DD2 50 yılda aşılma olasılığı %10
 ZEMİN SINIFI : ZD
 BİNA KOORDİNATI (ENLEM/BOYLAM) : 40.98416° / 28.72894°
 YEREL SPECTRAL İVME KATSAYISI S_s/S_1 : 1.250 / 0.338
 TASARIM SPECTRAL İVME KATSAYISI S_{ds}/S_{d1} : 1.245 / 0.663 DD2, 0.661 / 0.285 DD3
 YAPI DAVRANIŞ KATSAYISI R : 8.00 TÜMÜ YS. ÇERÇEVELİ YAPILAR - A11
 SİSTEM DAYANIM FAZLALIĞI KATSAYISI D : 3
 DEPREM TASARIM SINIFI DTS : 1a
 BİNA YÜKSEKLİK SINIFI BYS : 8 $H_n=0.1m$
 BİNA KULLANIM SINIFI BKS : 1 $I = 1.5$
 Modal Analiz min. deprem yükü oranı β : 0.9
 Deprem yükü eksantirisitesi : 0.050
 Deprem modal analiz CQC sönüm oranı : %5
 PERFORMANS HEDEFLERİ :
 DD2 } Normal Performans Hedefi : KH (Kontrollü Hasar)
 Değerlendirme/Tasarım : DGT (Dayanıma Göre Tasarım)

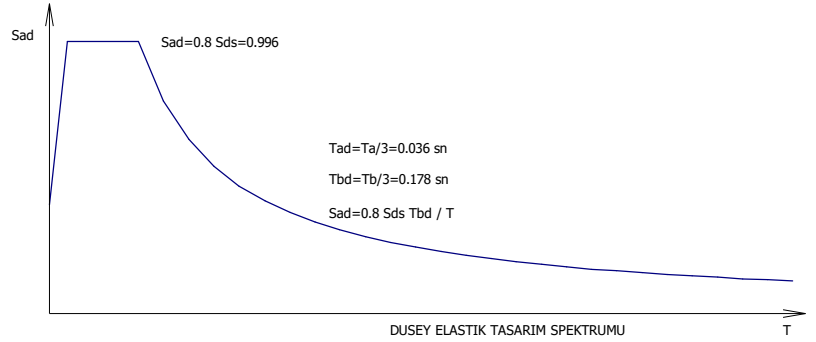
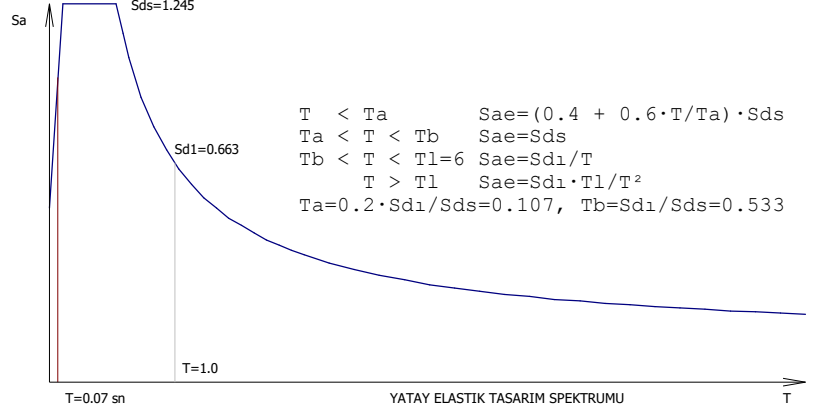
DİYAFRAM SAYISI : 1

Diyafram tanımı : KAT(diyafram no)

DİNAMİK ANALİZ BİLGİLERİ

TASARIM SPECTURUM BİLGİSİ (TBDY 2018 SPEKTRUM)

T (s)	Sa
0.00	0.498
0.11	1.245
0.53	1.245
0.58	1.138
0.63	1.048
0.73	0.905
0.83	0.796
0.93	0.711
1.03	0.642
1.13	0.585
1.23	0.538
1.33	0.498
1.43	0.463
1.53	0.433
1.63	0.406
1.73	0.383
1.83	0.362
1.93	0.343
2.03	0.326
2.23	0.297
2.43	0.273
2.63	0.252
2.83	0.234
3.03	0.219
3.23	0.205
3.43	0.193
3.63	0.183
3.83	0.173
4.03	0.164
4.23	0.157
4.43	0.150
4.63	0.143
4.83	0.137
5.03	0.132
5.23	0.127
5.43	0.122
5.63	0.118
5.83	0.114
6.03	0.110



Düsey deprem etkisi hesabında tüm taşıyıcı sistemler için $R/I = 1$ ve $D = 1$ alınacaktır.

$$R_a(T)x = 3.266 \quad R_a(T)y = 3.299 \quad T < T_b \Rightarrow R_a(T) = D + (R/I - D) \cdot T/T_b$$

MODAL ANALİZ - YAPI PERİYOD ve VEKTORLERİ

Fea Mod sayısı=3 Fea nokta sayısı=552

Mod	1.mod	2.mod	3.mod
ω	92.23	103.46	203.38
T	0.0681	0.0607	0.0309
Mxr%	0.026	95.229	0.088
Myr%	81.628	0.176	14.791

$$\Sigma = 95.34$$

$$\Sigma = 96.59$$

$M_r = \sum (m_i \cdot \Phi_{xir}^2 + m_i \cdot \Phi_{yir}^2 + m_{\theta i} \cdot \Phi_{\theta ir}^2)$
 $M_{xr} = \sum [(\sum m \cdot \Phi)^2 / M_r] = 95.34 > 95.00$ Dinamik kütle oranı yeterli.
 $M_{yr} = \sum [(\sum m \cdot \Phi)^2 / M_r] = 96.59 > 95.00$ Dinamik kütle oranı yeterli.

EŞDEĞER DEPREM HESABI 1. DOĞAL TİTREŞİM PERİYODUNUN KONTROLÜ

$H_n = 0.1m$ $C_{tx} = 0.1$ $C_{ty} = 0.1$

$T_{lx} = C_{tx} \cdot H_n^{3/4} = 0.018 \text{ s.}, T_x = 0.061 \text{ s.} > 1.4 \times 0.018 \text{ s.} \gg T_{x1} = 0.025 \text{ s.}$

$T_{ly} = C_{ty} \cdot H_n^{3/4} = 0.018 \text{ s.}, T_y = 0.068 \text{ s.} > 1.4 \times 0.018 \text{ s.} \gg T_{y1} = 0.025 \text{ s.}$

KAT KÜTLESİ ve RİJİTLİK MERKEZİ (t)

Kat (dyf)	H (m)	Wg	Wq	n	R Rx/Ry	D Dx/Dy	$\sum W_k$
1	4.60	410.19	57.29	0.80	3.11	1.5/1.8	456.027

$\sum W_t = 456.027$

EŞDEĞER DEPREM FORMÜLÜ $F_{di} = (V_t - F_t) \frac{W_i \cdot H_i}{\sum W_i \cdot H_i}$

DEPREM KUVVETİ (t)

Deprem tepe yükü $F_{tx} = 0.74$ $F_{ty} = 0.74$ (t)

X YÖNÜ					Y YÖNÜ			
Kat no	Modal Analiz	Eşdeğer dep.yön.	Deprem yükü	Kat tipi	Modal Analiz	Eşdeğer dep.yön.	Deprem yükü	Kat tipi
1	85.136	98.670	88.803	NORMAL	90.256	98.670	90.256	NORMAL
$\sum$	85.136	98.670	88.803	GENEL	90.256	98.670	90.256	GENEL

Fea3d analizde ek dışmerkezlilik etkisi; $\Delta m_i = m_i \cdot e^2$ kütle artımı ile düzenlenmiştir.

$V_{tx} = 98.67 > 0.04 \cdot I \cdot S_{ds} \cdot W = 34.07$ TBDY2018 4.7.1.1

$V_{ty} = 98.67 > 0.04 \cdot I \cdot S_{ds} \cdot W = 34.07$

X Deprem kontrol: $0.90 \times 98.670 = 88.803 > 85.136 \gg 88.803$

Y Deprem kontrol: $0.90 \times 98.670 = 88.803 < 90.256 \gg 90.256$

TBDY-2018 BODRURLU YAPI PERİYOD VE KÜTLE KATILIM KONTROLÜ

(Bodrum kütleleri hesaba katılmadan tüm yapının periyod ve kütle katılım kontrolü TBDY2018-3.3.1.1)

Mod	1.mod	2.mod	3.mod	4.mod	5.mod	6.mod
ω	92.12	103.10	142.80	183.59	215.26	325.05
T	0.0682	0.0609	0.0440	0.0342	0.0292	0.0193
Mxr%	0.136	96.526	0.152	0.012	0.488	0.163
Myr%	82.653	0.189	3.396	3.195	7.667	0.301

$T_x \text{ tum} = 0.061s < 1.1 \times T_x \text{ ust}(0.061s) = 0.067s \checkmark$

$T_y \text{ tum} = 0.068s < 1.1 \times T_y \text{ ust}(0.068s) = 0.075s \checkmark$

TBDY-2018 YAPI Ralt ve Dalt KATSAYILARININ BULUNMASI (TBDY 4.3.6.1)

Eşdeğer deprem:

$S_a(T_{x1}) = S_a(0.025) = 0.673, S_a(T_{y1}) = S_a(0.025) = 0.673$

$V_{\text{tum}X} = V_{\text{ust}X} + S_a(T_{x1}) \times W_b / 1.5 = 88.803 + \times 0.673 / 1.5 = 88.803$

$V_{\text{tum}Y} = V_{\text{ust}Y} + S_a(T_{y1}) \times W_b / 1.5 = 90.256 + \times 0.673 / 1.5 = 90.256$

X yönü $v_{\text{ust}X} = V_{\text{ust}X} / V_{\text{tum}X} = 98.670 / 98.670 = 1.000, Y \text{ yönü } v_{\text{ust}Y} = V_{\text{ust}Y} / V_{\text{tum}Y} = 98.670 / 98.670 = 1.000$

$v_{\text{xalt}} = (1 - v_{\text{ust}X}) \times R_a / 1.5 = 0.000, v_{\text{yalt}} = (1 - v_{\text{ust}Y}) \times R_a / 1.5 = 0.000$

$v_x = v_{\text{xust}} + v_{\text{xalt}} = 1.000, v_y = v_{\text{yust}} + v_{\text{yalt}} = 1.000$

$D_{\text{alt}X} = (0.6 \times v_{\text{xust}} \times D_{\text{ust}} + v_{\text{xalt}} \times 1.5) / v_x = 1.800$

$D_{\text{alt}Y} = (0.6 \times v_{\text{yust}} \times D_{\text{ust}} + v_{\text{yalt}} \times 1.5) / v_y = 1.800$

$R_{\text{alt}X} = R_a / v_x = 8.000, R_{\text{alt}Y} = R_a / v_y = 8.000$

Modal analiz:

$v_{\text{ust}X} = 0, v_{\text{ust}Y} = 0$ alındı.

$D_{\text{alt}X} = (0.6 \times v_{\text{xust}} \times D_{\text{ust}} + v_{\text{xalt}} \times 1.5) / v_x = 1.500$

$D_{\text{alt}Y} = (0.6 \times v_{\text{yust}} \times D_{\text{ust}} + v_{\text{yalt}} \times 1.5) / v_y = 1.500$

$R_{\text{alt}X} = R_a / v_x = 1.500, R_{\text{alt}Y} = R_a / v_y = 1.500$

YAPI DEPREM YÜKLERİ (t)

Yapı periyodları $T_x = 0.061$ $T_y = 0.068$ $R = 8.0$

$T_x < T_b \gg R_{ax} = D + (R / I - D) T_x / T_b = 3.11$ $T_y < T_b \gg R_{ay} = D + (R / I - D) T_y / T_b = 3.11$

X yönü $W = 456.09$ $F_{\text{deprem}} = 98.67$ tepe yükü $F_d = 0.74$

Y yönü $W = 456.09$ $F_{\text{deprem}} = 98.67$ tepe yükü $F_d = 0.74$

Kat (Dyf)	F modal X	F eşdeğer X	F deprem X	F modal Y	F eşdeğer Y	F deprem Y
1(1)	85.14	98.67	88.80	90.26	98.67	90.26
$\sum$	85.14	98.67	88.80	90.26	98.67	90.26

X Deprem kontrol: $0.90 \times 98.670 = 88.803 > 85.136 \gg 88.803$

Y Deprem kontrol: $0.90 \times 98.670 = 88.803 < 90.256 \gg 90.256$

Rüzgar kuvvetleri (t)

Kat (dyf)	X-yönü F	X-yönü ey m	Y-yönü F	Y-yönü ex m
1	2.374	-12.350	3.781	11.900

Yapıda Deprem Perdesi bulunamadı.

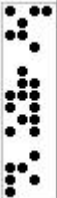
Deprem perde taban devrilme oranı $M_{dev}/M_o = 0.00$

Bina Taşıyıcı Sistem seçimi : Süneklilik düzeyi Yüksek taşıyıcı sistem

$H_n = H - H_{bodrum} = 4.6 - 4.5 = 0.1m >> BYS=8$

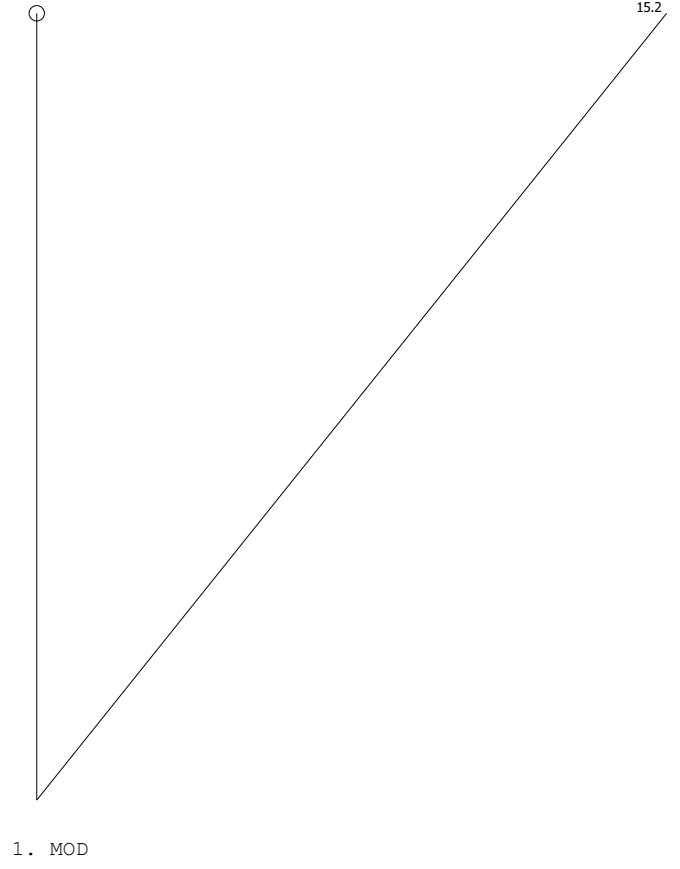
TBDY2018 4.3.4.3 koşulu sağlanmaktadır. $BYS=8 \geq 3$ ✓

Kenar aks perdesi bulunmamıştır.

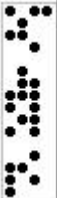
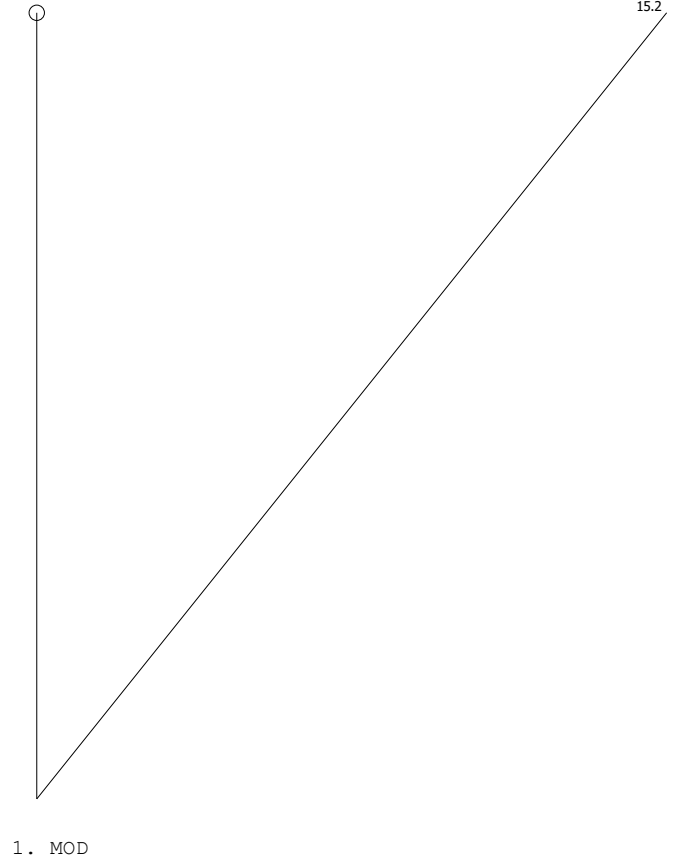


MODAL ANALİZ MOD GRAFİĞİ (1000 x Dep. vektörü)

X yönü



Y yönü



DEPREM YAPI DEVRİLME KONTROLU

Kat deprem momenti (tm)

Kat	H (m)	Fx	Fx . H	H (m)	Fy	Fy . H
1	4.60	88.80	408.50	4.60	90.26	415.18
		88.80	408.50		90.26	415.18

Kat düşey yük momenti (tm)

X=-5.5m

Y=16.2m

moment noktası

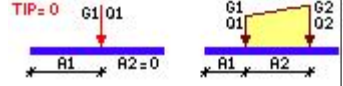
Kat	Wg+0.8.Wq	Xg-X	(Xg-X) . (Wg+0.8.Wq)	Yg-Y	(Yg-Y) . (Wg+0.8.Wq)
1	456.03 147.28	6.781 6.850	3092.15 1008.83	4.277 4.300	1950.44 633.28
			4100.99		2583.72

X yönü devrilme kontrolu=4100.986/408.495=10.039 > 1.5 ✓

Y yönü devrilme kontrolu=2583.724/415.178=6.223 > 1.5 ✓

KİRİŞ DÜŞEY YÜK BİLGİLERİ

Kiriş no	A1 m	A2 m	G1 t/m	G2 t/m	Q1 t/m	Q2 t/m	Yük elemanı no
K101	0.15	0.60	0.28	1.39	0.08	0.37	D105
K101	0.75	0.75	1.39	0.00	0.37	0.00	D105
K101	0.15	1.50	0.28	3.05	0.08	0.82	D106
K101	0.00	1.50	3.05	0.28	0.82	0.07	D106
K102	0.15	8.00	2.36	2.36	0.64	0.64	D101
K102	0.15	8.00	2.31	2.31	0.63	0.63	D102
K103	0.15	8.00	2.31	2.31	0.63	0.63	D102
K103	0.15	8.00	2.31	2.31	0.63	0.63	D103
K104	0.15	8.00	2.31	2.31	0.63	0.63	D103
K104	0.15	8.00	2.36	2.36	0.64	0.64	D104
K105	0.15	0.60	0.28	1.39	0.07	0.37	D105
K105	0.75	0.35	1.39	1.39	0.37	0.37	D105
K105	1.10	0.55	1.39	0.00	0.37	0.00	D105
P110	0.50	0.60	0.28	1.39	0.08	0.37	D105
P110	1.10	0.60	1.39	0.28	0.37	0.08	D105
P116	0.50	1.50	0.28	3.05	0.08	0.82	D106
P116	2.00	1.50	3.05	0.28	0.82	0.07	D106
P117	0.50	6.60	2.36	2.36	0.64	0.64	D101
P118	0.50	5.50	2.36	2.36	0.64	0.64	D104
P118	0.50	0.85	1.48	3.05	0.40	0.82	D106
P118	1.35	3.15	3.05	3.05	0.82	0.82	D106
P118	4.50	1.50	3.05	0.28	0.82	0.07	D106
P119	0.15	1.50	2.36	2.36	0.64	0.64	D104
P119	0.15	0.60	0.28	1.39	0.07	0.37	D105
P119	0.75	0.35	1.39	1.39	0.37	0.37	D105
P119	1.10	0.55	1.39	0.37	0.37	0.10	D105
P120	0.50	0.85	1.48	3.05	0.40	0.82	D106
P120	1.35	3.15	3.05	3.05	0.82	0.82	D106
P120	4.50	0.80	3.05	1.57	0.82	0.42	D106

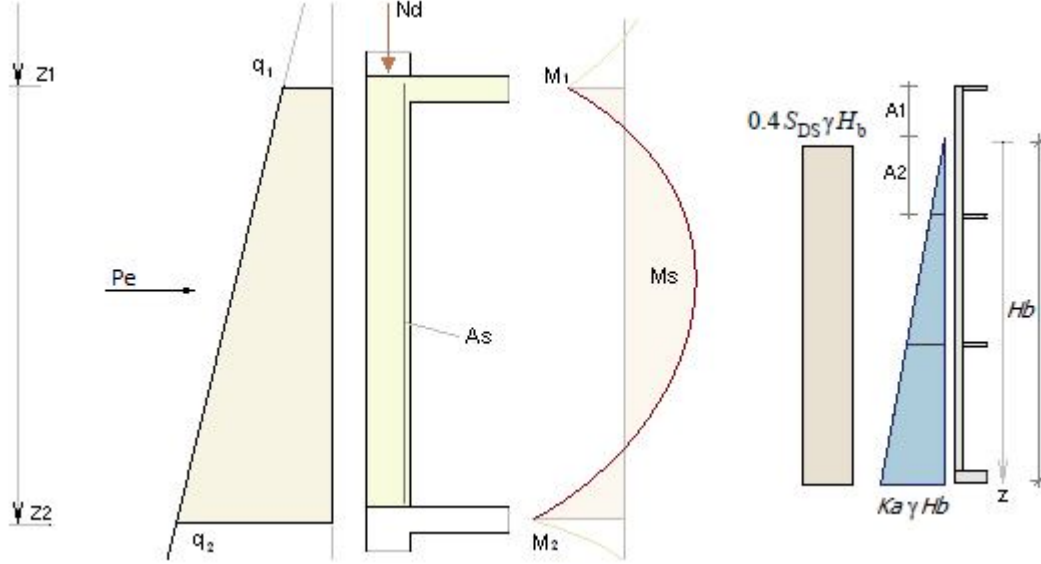


PANEL YATAY YÜK BİLGİLERİ

ZEMİN BİRİM HACİM AĞIRLIĞI=1.8 t/m³

ZEMİN İCSEL SURTUNME ACISI=30.0°

Kas=0.333 Qe = 0.4 × Sds × Y × Hb

Su deprem yuku : Qe=7/12·(0.4·Sds)·H², P(z)=7/8·(0.4·Sds) (z·H)^½

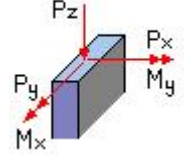
Panel no	A1 m	A2 m	Q1 t/m ²	Q2 t/m ²	Hb m	Qe t/m ²	Yük tipi
P106	0.00	4.60	3.150	3.150	4.60	4.123	Zemin yuku
P107	0.00	4.60	3.150	3.150	4.60	4.123	Zemin yuku
P108	0.00	4.60	3.150	3.150	4.60	4.123	Zemin yuku
P109	0.00	4.60	3.150	3.150	4.60	4.123	Zemin yuku
P110	0.00	4.60	3.150	3.150	4.60	4.123	Zemin yuku
P111	0.00	4.60	3.150	3.150	4.60	4.123	Zemin yuku
P117	0.00	4.60	3.150	3.150	4.60	4.123	Zemin yuku
P112	0.00	4.60	-3.150	-3.150	4.60	4.123	Zemin yuku
P113	0.00	4.60	-3.150	-3.150	4.60	4.123	Zemin yuku
P114	0.00	4.60	-3.150	-3.150	4.60	4.123	Zemin yuku
P115	0.00	4.60	-3.150	-3.150	4.60	4.123	Zemin yuku
P116	0.00	4.60	-3.150	-3.150	4.60	4.123	Zemin yuku
P120	0.00	4.60	-3.150	-3.150	4.60	4.123	Zemin yuku
P121	0.00	4.60	-3.150	-3.150	4.60	4.123	Zemin yuku
P118	1.20	3.40	3.000	3.000	4.60	4.123	Zemin yuku

PANEL YATAY YÜK BİLGİLERİ

Panel no	A1 m	A2 m	Q1 t/m ²	Q2 t/m ²	Hb m	Qe t/m ²	Yük tipi
P119	1.20	3.40	3.000	3.000	4.60	4.123	Zemin yuku

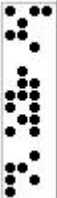
KOLON YÜK BİLGİLERİ

Kolon no	Kombinasyon	Px t	Py t	Pz t	Mx tm	My tm	Eleman no
S101	Olu yuk	0.00	0.00	2.00	0.30	0.15	D101
S101	Hareketli yuk	0.00	0.00	0.54	0.08	0.04	D101
S102	Olu yuk	0.00	0.00	0.34	0.00	0.03	D102
S102	Hareketli yuk	0.00	0.00	0.09	0.00	0.01	D102
S102	Olu yuk	0.00	0.00	0.35	0.00	0.03	D101
S102	Hareketli yuk	0.00	0.00	0.09	0.00	0.01	D101
S103	Olu yuk	0.00	0.00	0.34	0.00	0.03	D103
S103	Hareketli yuk	0.00	0.00	0.09	0.00	0.01	D103
S103	Olu yuk	0.00	0.00	0.34	0.00	0.03	D102
S103	Hareketli yuk	0.00	0.00	0.09	0.00	0.01	D102
S104	Olu yuk	0.00	0.00	0.35	0.00	0.03	D104
S104	Hareketli yuk	0.00	0.00	0.09	0.00	0.01	D104
S104	Olu yuk	0.00	0.00	0.34	0.00	0.03	D103
S104	Hareketli yuk	0.00	0.00	0.09	0.00	0.01	D103
S105	Olu yuk	0.00	0.00	0.02	-0.01	0.00	D105
S105	Olu yuk	0.00	0.00	0.02	-0.01	0.00	D105
S105	Olu yuk	0.00	0.00	0.35	-0.18	0.03	D104
S105	Hareketli yuk	0.00	0.00	0.09	-0.05	0.01	D104
S106	Olu yuk	0.00	0.00	0.02	0.01	0.00	D105
S106	Olu yuk	0.00	0.00	0.02	0.00	0.00	D105
S108	Olu yuk	0.00	0.00	0.02	0.00	0.01	D106
S108	Olu yuk	0.00	0.00	0.02	0.00	0.01	D105
S108	Olu yuk	0.00	0.00	0.04	-0.01	0.02	D105
S108	Hareketli yuk	0.00	0.00	0.01	0.00	0.01	D105
S108	Olu yuk	0.00	0.00	0.59	-0.09	0.06	D106
S108	Hareketli yuk	0.00	0.00	0.16	-0.02	0.02	D106
S108	Olu yuk	0.00	0.00	2.36	-0.35	0.35	D104
S108	Hareketli yuk	0.00	0.00	0.64	-0.09	0.10	D104
S109	Olu yuk	0.00	0.00	0.02	0.00	0.01	D106
S109	Olu yuk	0.00	0.00	0.59	-0.09	0.06	D106
S109	Hareketli yuk	0.00	0.00	0.16	-0.02	0.02	D106
S110	Olu yuk	0.00	0.00	2.00	0.30	0.45	D101
S110	Hareketli yuk	0.00	0.00	0.54	0.08	0.12	D101
S111	Olu yuk	0.00	0.00	0.34	0.00	0.08	D102
S111	Hareketli yuk	0.00	0.00	0.09	0.00	0.02	D102
S111	Olu yuk	0.00	0.00	0.35	0.00	0.08	D101
S111	Hareketli yuk	0.00	0.00	0.09	0.00	0.02	D101
S112	Olu yuk	0.00	0.00	0.34	0.00	0.08	D102
S112	Hareketli yuk	0.00	0.00	0.09	0.00	0.02	D102
S112	Olu yuk	0.00	0.00	0.34	0.00	0.08	D103
S112	Hareketli yuk	0.00	0.00	0.09	0.00	0.02	D103
S113	Olu yuk	0.00	0.00	0.34	0.00	0.08	D103
S113	Hareketli yuk	0.00	0.00	0.09	0.00	0.02	D103
S113	Olu yuk	0.00	0.00	0.35	0.00	0.08	D104
S113	Hareketli yuk	0.00	0.00	0.09	0.00	0.02	D104
S114	Olu yuk	0.00	0.00	0.02	-0.01	0.00	D106
S114	Olu yuk	0.00	0.00	0.02	-0.01	0.01	D106
S114	Olu yuk	0.00	0.00	0.35	-0.18	0.08	D104
S114	Hareketli yuk	0.00	0.00	0.09	-0.05	0.02	D104
S115	Olu yuk	0.00	0.00	0.02	0.00	-0.01	D106
S115	Olu yuk	0.00	0.00	0.67	-0.10	0.18	D106
S115	Hareketli yuk	0.00	0.00	0.18	-0.03	0.05	D106



DÖŞEME ŞERİT BİLGİLERİ

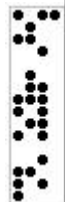
YÖN	DÖŞEME ŞERİTİ
X	-D101-D102-D103-D104-D106-
X	-D101-D102-D103-D104-D105-
Y	-D105-D106-



DÖŞEME BİLGİLERİ

Döşeme no	Sol Aks	Sag Aks	Üst Aks	Alt Aks	yön	d, dmin cm	bo cm	bt cm	g t/m ²	q t/m ²	gx t/m ²	gy t/m ²	qx t/m ²	qy t/m ²
D101	2X	8X	1Y	2Y	X-HURDI	20≥ 8			1.850	0.500	1.850	0.000	0.500	0.000
D102	8X	5X	1Y	2Y	X-HURDI	20≥ 8			1.850	0.500	1.850	0.000	0.500	0.000
D103	5X	7X	1Y	2Y	X-HURDI	20≥ 8			1.850	0.500	1.850	0.000	0.500	0.000
D104	7X	6X	1Y	2Y	X-HURDI	20≥ 8			1.850	0.500	1.850	0.000	0.500	0.000
D105	6X	9X	1Y	3Y	PLAK	20≥ 8			1.850	0.500	0.947	0.903	0.256	0.244
D106	6X	1X	3Y	2Y	PLAK	20≥ 11			1.850	0.500	1.753	0.097	0.474	0.026

Dmin: TS500 minimum yükseklik



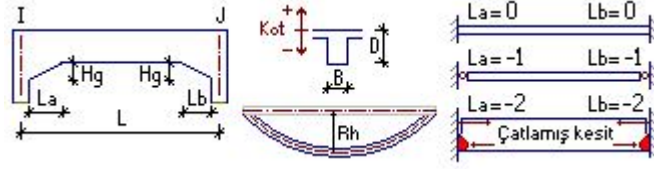
DÖŞEME STATİK HESAP SONUÇLARI

Zamana bağlı sehim : $\delta_t = \delta_i + \delta_{ig} \cdot \lambda$, $\lambda=2$ (5yıl üzeri)

Döşeme no	yön	L m	sol mesnet gGg	mesnet qGq	(tm) gQg	açıklık	sağ mesnet gGg	mesnet qGq	(tm) gQg	sehim < fmax $\delta_t = \delta_i + \delta_{ig} \cdot \lambda$ mm	Wk mm
D101	X	2.70	4.72	3.94	4.44	1.88	-0.25	-0.20	-0.21	0.82 < 7.08 ✓	0.26
E1	Y	8.60	1.11	0.85	1.11	1.08	-1.11	-0.85	-1.12	2.12	0.26
D102	X	2.50	0.25	0.20	0.21	1.43	-0.89	-0.71	-0.84	0.31 < 6.94 ✓	0.26
E1	Y	8.60	1.52	1.49	1.21	1.34	-1.53	-1.50	-1.22	0.79	0.26
D103	X	2.50	0.89	0.71	0.84	1.41	-0.32	-0.29	-0.25	0.32 < 6.94 ✓	0.26
E1	Y	8.60	1.52	1.19	1.50	1.34	-1.52	-1.20	-1.51	0.82	0.26
D104	X	2.70	0.32	0.29	0.25	1.77	-4.18	-3.61	-3.79	0.77 < 7.08 ✓	0.26
E1	Y	8.60	1.72	1.33	1.73	1.02	-1.76	-1.35	-1.77	1.99	0.26
D105	X	1.50	1.00	0.77	0.99	0.53	0.00	0.00	0.00	0.03 < 5.14 ✓	0.26
E1	Y	1.80	0.27	0.23	0.25	0.34	-0.56	-0.52	-0.46	0.09	0.26
D106	X	3.30	4.18	3.61	3.79	1.82	-2.58	-2.61	-1.93	0.34 < 9.17 ✓	0.26
E1	Y	6.80	0.99	0.99	0.75	0.74	-1.41	-1.45	-1.04	0.88	0.26

DÖŞEME BETONARME HESAP SONUÇLARI

Döşeme no	Msol (tm)	As cm ²	Maç (tm)	As cm ²	Msağ (tm)	As cm ²	Donatı
D101 X d=20cm Y	4.72 1.12	7.94 2.36	1.88 1.08	3.40 0.00	0.25 1.11	0.52 2.36	ø10/20 (düz)+ø10/30 (sol ila)+ø12/20 (Mon.) ø10/20 (düz)+ø10/30 (sol ila)+ø10/30 (sağ ila)
D102 X d=20cm Y	0.25 1.53	0.52 3.25	1.43 1.34	3.40 0.00	0.89 1.52	1.87 3.23	ø10/20 (düz)+ø10/30 (Mon.) ø10/20 (düz)+ø10/24 (sol ila)+ø10/24 (sağ ila)
D103 X d=20cm Y	0.89 1.52	1.87 3.24	1.41 1.34	3.40 0.00	0.32 1.52	0.67 3.22	ø10/20 (düz)+ø10/30 (Mon.) ø10/20 (düz)+ø10/24 (sol ila)+ø10/24 (sağ ila)
D104 X d=20cm Y	0.32 1.77	0.67 3.77	1.77 1.02	3.40 0.00	4.18 1.73	6.99 3.68	ø10/20 (düz)+ø10/17 (sağ ila)+ø10/30 (Mon.) ø10/20 (düz)+ø10/20 (sol ila)+ø10/21 (sağ ila)
D105 X d=20cm Y	1.00 0.56	2.11 1.18	0.53 0.34	3.40 3.40	0.00 0.27	0.00 0.57	ø10/20 (düz)+ø10/30 (Mon.) ø10/20 (düz)+ø10/30 (Mon.)
D106 X d=20cm Y	4.18 1.45	6.99 3.08	1.82 0.74	3.40 1.56	2.61 0.99	5.59 2.10	ø10/20 (düz)+ø10/26 (sağ ila)+ø10/30 (Mon.) ø10/20 (düz)+ø10/30 (sol ila)+ø10/30 (Mon.)



KİRİŞ VE PANEL BİLGİLERİ

Kiriş no	aks	sol aks	sağ aks	D cm	B cm	G (t/m)	I/J Nokta	L m	Rh m	Tabla b/d (cm)	sol Hg/Lg (cm)	sağ Hg/Lg (cm)	Mal zeme
K101	3Y	6X	9X	60	40	0.600	25-28	1.65	0.00	36/20	0/0	0/0	E1
K101	3Y	9X	1X	60	40	0.600	28-31	1.65	0.00	18/20	0/0	0/0	E1
K102	8X	1Y	2Y	60	60	0.900	4-6	8.30	0.00	96/20	0/0	0/0	E1
K103	5X	1Y	2Y	60	60	0.900	10-11	8.30	0.00	96/20	0/0	0/0	E1
K104	7X	1Y	2Y	60	60	0.900	14-15	8.30	0.00	96/20	0/0	0/0	E1
K105	9X	1Y	3Y	60	30	0.450	24-28	1.85	0.00	9/20	0/0	0/0	E1
P106	1Y	2X	8X	460	30	3.450	1-4	2.55	0.00	11/20	0/0	0/0	E1
P107	1Y	8X	5X	460	30	3.450	4-10	2.50	0.00	9/20	0/0	0/0	E1
P108	1Y	5X	7X	460	30	3.450	10-14	2.50	0.00	9/20	0/0	0/0	E1
P109	1Y	7X	6X	460	30	3.450	14-18	2.20	0.00	7/20	0/0	0/0	E1
P110	1Y	6X	9X	460	30	3.450	18-24	2.20	0.00	7/20	0/0	0/0	E1
P111	1Y	9X	1X	460	30	3.450	24-30	1.45	0.00	0/0	0/0	0/0	E1
P112	2Y	2X	8X	460	30	3.450	5-6	2.55	0.00	11/20	0/0	0/0	E1
P113	2Y	8X	5X	460	30	3.450	6-11	2.50	0.00	9/20	0/0	0/0	E1
P114	2Y	5X	7X	460	30	3.450	11-15	2.50	0.00	9/20	0/0	0/0	E1
P115	2Y	7X	6X	460	30	3.450	15-19	2.20	0.00	7/20	0/0	0/0	E1
P116	2Y	6X	1X	460	30	3.450	19-26	3.65	0.00	18/20	0/0	0/0	E1
P117	2X	1Y	2Y	460	30	3.450	1-5	7.60	0.00	40/20	0/0	0/0	E1
P118	6X	3Y	2Y	460	30	3.450	25-19	6.15	0.00	66/20	0/0	0/0	E1
P119	6X	1Y	3Y	460	30	3.450	18-25	2.15	0.00	18/20	0/0	0/0	E1
P120	1X	3Y	2Y	460	30	3.450	31-26	5.80	0.00	29/20	0/0	0/0	E1
P121	1X	1Y	3Y	460	30	3.450	30-31	1.80	0.00	0/0	0/0	0/0	E1

KİRİŞ STATİK HESAP SONUÇLARI

ANALİZLERDE, ÇATLAMIŞ KESİT ETKİN KESİT RİJİTLİK ÇARPANI DİKKATE ALINMIŞTIR TBDY2018 4.5.8

K101		GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	3.18	0.77	0.18	0.60	0.50	0.77	0.28	0.04	0.33 (tm)	
SagM	1.67	0.39	0.42	-0.03	-0.01	0.39	0.39	-0.26		
SolV	4.35	1.04	0.53	0.51	0.45	1.03	0.59	-0.15	Xaç (m)	
SagV	2.17	0.52	0.25	0.27	0.22	0.52	0.31	-0.16	1.57	
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z				
SolM	0.00	-0.02	0.09	-0.09	0.00	0.00	2.64			
SagM	-0.04	0.04	0.04	-0.03	0.00	0.00	1.39			
SolV	-0.02	0.01	0.09	-0.09	0.00	0.00	3.61	Z1=	4.60m	
SagV	-0.02	0.01	0.09	-0.08	0.00	0.00	1.80	Z2=	4.60m	
K101		GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	-1.65	-0.38	-0.42	-0.04	0.02	-0.38	-0.39	0.24	1.96 (tm)	
SagM	-0.25	0.01	-0.03	0.03	0.01	0.01	-0.01	-0.86		
SolV	-0.50	-0.08	-0.13	0.05	0.02	-0.08	-0.10	-0.40	Xaç (m)	
SagV	-2.29	-0.46	-0.52	0.05	0.02	-0.46	-0.49	-0.45	0.00	
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z				
SolM	0.03	-0.03	-0.04	0.03	0.00	0.00	-1.37			
SagM	-0.08	0.07	0.07	-0.06	0.00	0.00	-0.21			
SolV	-0.03	0.02	0.02	-0.02	0.00	0.00	-0.41	Z1=	4.60m	
SagV	-0.03	0.03	0.02	-0.02	0.00	0.00	-1.90	Z2=	4.60m	
K102		GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	16.01	3.84	1.94	1.90	3.75	2.01	1.92	0.34	29.63 (tm)	
SagM	-16.05	-3.84	-1.94	-1.90	-3.76	-2.01	-1.92	-0.35		
SolV	16.43	3.93	1.95	1.98	3.75	2.15	1.97	0.04	Xaç (m)	
SagV	-16.41	-3.93	-1.95	-1.98	-3.74	-2.14	-1.97	-0.04	4.15	
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z				
SolM	-0.04	0.04	-0.10	0.08	0.00	0.00	13.29			
SagM	0.04	-0.05	-0.10	0.08	0.00	0.00	-13.32			
SolV	-0.02	0.02	-0.03	0.03	0.00	0.00	13.64	Z1=	4.60m	
SagV	0.02	-0.02	-0.03	0.02	0.00	0.00	-13.62	Z2=	4.60m	
K103		GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	17.52	4.19	1.97	2.22	2.22	4.07	2.09	0.42	35.22 (tm)	
SagM	-17.58	-4.20	-1.98	-2.22	-2.22	-4.08	-2.10	-0.42		
SolV	18.11	4.33	1.99	2.33	2.34	4.15	2.16	0.05	Xaç (m)	
SagV	-18.09	-4.32	-1.99	-2.33	-2.34	-4.14	-2.16	-0.05	4.15	
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z				
SolM	0.00	0.00	-0.08	0.07	0.00	0.00	14.54			
SagM	0.01	-0.01	-0.08	0.07	0.00	0.00	-14.59			
SolV	0.00	-0.01	-0.02	0.02	0.00	0.00	15.04	Z1=	4.60m	
SagV	0.00	0.00	-0.02	0.02	0.00	0.00	-15.02	Z2=	4.60m	
K104		GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	16.39	3.93	0.06	3.88	1.97	3.95	1.94	0.45	28.65 (tm)	
SagM	-16.51	-3.95	-0.06	-3.89	-1.98	-3.97	-1.95	-0.45		
SolV	16.24	3.89	0.15	3.74	1.97	3.87	1.93	0.14	Xaç (m)	
SagV	-16.28	-3.89	-0.14	-3.75	-1.99	-3.88	-1.92	-0.14	4.15	
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z				
SolM	0.01	-0.01	-0.05	0.06	0.00	0.00	13.61			
SagM	0.00	0.00	-0.07	0.07	0.00	0.00	-13.70			
SolV	0.01	-0.01	-0.02	0.02	0.00	0.00	13.48	Z1=	4.60m	
SagV	-0.01	0.01	-0.02	0.02	0.00	0.00	-13.52	Z2=	4.60m	
K105		GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	0.93	0.20	0.25	-0.05	-0.02	0.20	0.22	-0.17	-0.16 (tm)	
SagM	-0.25	-0.09	-0.05	-0.04	-0.03	-0.09	-0.06	-0.15		
SolV	1.21	0.24	0.15	0.08	0.11	0.24	0.12	-0.22	Xaç (m)	
SagV	-0.02	-0.02	0.13	-0.15	-0.12	-0.02	0.10	-0.21	1.85	
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z				
SolM	0.01	-0.01	-0.10	0.10	0.00	0.00	0.77			
SagM	-0.01	0.01	-0.01	0.01	0.00	0.00	-0.20			
SolV	0.00	0.00	-0.09	0.08	0.00	0.00	1.01	Z1=	4.60m	
SagV	0.00	0.01	-0.07	0.07	0.00	0.00	-0.02	Z2=	4.60m	
P106		GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	-6.94	-1.60	-0.47	-1.14	-1.48	-0.62	-1.11	0.00	0.00 (tm)	
SagM	-14.04	-2.74	-1.13	-1.61	-2.02	-2.03	-1.44	11.33		
SolV	-8.23	-1.08	-0.57	-0.50	-0.82	-0.89	-0.45	9.16	Xaç (m)	
SagV	-7.25	-1.83	-0.54	-1.29	-1.56	-0.85	-1.24	14.02	0.00	
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z				
SolM	0.22	-0.29	0.38	-0.52	0.00	0.02	-5.76			
SagM	2.35	-2.56	3.91	-4.75	0.06	0.16	-11.66			
SolV	2.85	-3.09	3.78	-4.60	0.08	0.16	-6.83	Z1=	4.60m	
SagV	0.66	-0.76	0.78	-0.96	0.02	0.03	-6.02	Z2=	4.60m	
P107		GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	13.79	2.81	0.30	2.51	1.82	1.71	2.07	0.00	0.00 (tm)	
SagM	-15.37	-3.28	-0.38	-2.90	-2.01	-2.30	-2.25	11.33		
SolV	17.97	4.86	1.75	3.11	3.21	3.94	2.57	9.16	Xaç (m)	
SagV	-21.91	-6.04	-1.97	-4.06	-3.68	-5.37	-3.03	14.02	0.00	
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z				
SolM	-2.88	3.16	-3.22	4.10	-0.08	-0.13	11.45			
SagM	1.62	-1.98	2.80	-3.71	0.04	0.12	-12.76			
SolV	-1.82	1.96	1.42	-1.65	-0.07	0.05	14.92	Z1=	4.60m	
SagV	-2.29	2.49	-2.55	2.95	-0.05	-0.10	-18.19	Z2=	4.60m	

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P108	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	15.02	3.31	-1.27	-2.04	2.76	-2.34	1.52	0.00	0.00 (tm)
SagM	-8.70	-1.95	-0.81	-1.14	-1.83	-1.49	-0.58	11.33	
SolV	4.91	1.27	0.39	0.88	0.74	0.92	0.88	9.16	Xaç (m)
SagV	-14.22	-3.99	-1.44	-2.56	-2.57	-3.48	-1.93	14.02	0.00
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
SolM	-2.73	2.98	-2.50	2.68	-0.08	-0.10	12.46		
SagM	-0.49	0.07	1.60	-2.03	-0.02	0.07	-7.22		
SolV	-1.89	2.05	-0.12	0.18	-0.06	-0.01	4.07		
SagV	-1.66	1.87	-2.32	2.38	-0.02	-0.09	-11.80	Z1=	4.60m
								Z2=	4.60m
P109	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	6.87	1.62	-0.53	-1.09	0.65	-1.53	-1.06	0.00	0.00 (tm)
SagM	1.99	0.45	0.08	0.37	0.36	0.40	0.13	11.33	
SolV	8.31	2.13	0.52	1.61	1.50	1.97	0.79	9.16	Xaç (m)
SagV	1.54	0.30	0.07	0.23	0.16	0.28	0.16	14.02	0.00
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
SolM	-0.93	1.03	-1.34	1.11	-0.03	-0.06	5.70		
SagM	0.04	-0.05	-0.82	0.80	0.00	-0.03	1.65		
SolV	-2.36	2.62	-0.95	0.83	-0.08	-0.04	6.90		
SagV	0.80	-0.90	-1.35	1.31	0.03	-0.06	1.28	Z1=	4.60m
								Z2=	4.60m
P110	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	-4.02	-2.22	-1.16	-1.06	-1.16	-1.93	-1.33	0.00	0.00 (tm)
SagM	5.49	1.51	0.81	0.70	0.83	1.37	0.81	11.33	
SolV	60.28	-0.69	-0.45	-0.24	1.95	0.45	-3.79	9.16	Xaç (m)
SagV	-3.93	-0.85	-0.39	-0.46	-0.63	-0.78	-0.28	14.02	0.00
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
SolM	5.11	-5.66	-2.55	2.13	0.20	-0.11	-3.33		
SagM	-3.18	3.49	1.26	-0.99	-0.09	0.06	4.56		
SolV	50.31	-56.09	-47.44	44.97	1.94	-1.93	50.04		
SagV	-2.35	2.59	3.05	-2.96	-0.07	0.13	-3.26	Z1=	4.60m
								Z2=	4.60m
P111	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	-4.89	-1.41	-0.77	-0.64	-0.77	-1.28	-0.76	0.00	0.00 (tm)
SagM	1.34	0.62	0.50	0.12	0.15	0.58	0.51	44.42	
SolV	-2.38	-0.64	-0.24	-0.40	-0.47	-0.56	-0.24	-21.02	Xaç (m)
SagV	-11.06	-1.37	-0.26	-1.10	-1.39	-1.21	-0.13	44.20	0.00
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
SolM	0.61	-0.59	-1.33	0.86	0.01	-0.07	-4.05		
SagM	-0.61	0.56	2.42	-1.94	0.00	0.11	1.12		
SolV	0.20	-0.20	-0.29	0.10	0.01	-0.02	-1.98		
SagV	0.96	-1.56	12.60	-10.56	0.03	0.55	-9.18	Z1=	4.60m
								Z2=	4.60m
P112	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	-6.97	-1.61	-0.47	-1.14	-1.48	-0.63	-1.11	0.00	0.00 (tm)
SagM	-14.51	-2.80	-1.18	-1.62	-2.02	-2.09	-1.49	11.33	
SolV	-8.41	-1.10	-0.59	-0.50	-0.82	-0.91	-0.47	9.16	Xaç (m)
SagV	-7.41	-1.84	-0.55	-1.29	-1.57	-0.87	-1.25	14.02	0.00
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
SolM	0.31	-0.24	-0.39	0.52	0.01	-0.02	-5.79		
SagM	2.67	-2.48	-4.00	4.83	0.07	-0.17	-12.04		
SolV	3.14	-2.92	-3.82	4.65	0.08	-0.16	-6.98		
SagV	0.80	-0.70	-0.81	0.98	0.02	-0.03	-6.15	Z1=	4.60m
								Z2=	4.60m
P113	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	14.87	2.96	-0.43	-2.53	1.83	1.87	2.21	0.00	0.00 (tm)
SagM	-16.99	-3.51	-0.59	-2.92	-2.03	-2.53	-2.47	11.33	
SolV	17.86	4.85	1.76	3.09	3.19	3.94	2.58	9.16	Xaç (m)
SagV	-23.12	-6.23	-2.17	-4.07	-3.68	-5.56	-3.22	14.02	0.00
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
SolM	-3.19	3.01	3.73	-3.97	-0.08	0.15	12.34		
SagM	1.88	-1.89	-3.52	3.50	0.05	-0.14	-14.10		
SolV	-1.55	1.45	-1.40	1.61	-0.03	-0.05	14.83		
SagV	-2.78	2.59	2.29	-2.72	-0.07	0.09	-19.19	Z1=	4.60m
								Z2=	4.60m
P114	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	17.13	3.62	1.54	-2.08	2.78	-2.65	1.80	0.00	0.00 (tm)
SagM	-12.09	-2.49	-1.34	-1.15	-1.85	-2.03	-1.11	11.33	
SolV	3.99	1.11	0.22	0.89	0.74	0.76	0.72	9.16	Xaç (m)
SagV	-14.22	-4.06	-1.58	-2.48	-2.54	-3.55	-2.04	14.02	0.00
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
SolM	-3.02	2.78	2.93	-3.07	-0.07	0.12	14.22		
SagM	-0.86	0.50	-2.68	2.28	-0.02	-0.11	-10.03		
SolV	-2.23	2.08	-0.09	0.00	-0.05	0.00	3.31		
SagV	-3.00	2.73	2.25	-2.29	-0.07	0.09	-11.80	Z1=	4.60m
								Z2=	4.60m
P115	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	11.25	2.32	1.24	-1.09	0.67	-2.23	1.75	0.00	0.00 (tm)
SagM	2.24	0.32	-0.04	0.36	0.34	0.27	0.02	11.33	
SolV	9.56	2.26	0.56	1.70	1.54	2.11	0.87	9.16	Xaç (m)
SagV	2.11	0.06	-0.13	0.19	0.12	0.03	-0.03	14.02	0.00
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
SolM	-0.33	0.27	2.31	-1.99	-0.01	0.10	9.34		
SagM	-1.00	0.93	1.08	-0.99	-0.03	0.04	1.86		
SolV	-3.35	3.04	1.10	-0.95	-0.08	0.04	7.94		
SagV	-0.49	0.44	2.05	-1.88	-0.01	0.08	1.75	Z1=	4.60m
								Z2=	4.60m

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P116	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	46.02	7.57	7.09	0.48	0.99	7.75	6.40	0.00	0.00 (tm)
SagM	-46.02	-7.57	-7.09	-0.48	-0.99	-7.75	-6.40	11.33	
SolV	714.20	126.82	113.01	13.81	22.11	127.70	103.82	9.16	Xaç (m)
SagV	-11.88	-2.01	-1.40	-0.61	-0.80	-1.96	-1.26	14.02	0.00
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
SolM	22.04	-4.24	28.32	-1.42	0.55	1.17	38.20		
SagM	-22.04	4.24	-28.32	1.42	-0.55	-1.17	-38.20		
SolV	263.66	-244.46	377.99	-339.72	6.53	15.50	592.78	Z1=	4.60m
SagV	-3.24	3.05	-6.35	5.87	-0.08	-0.26	-9.86	Z2=	4.60m
P117	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	4.12	-0.28	0.15	-0.42	-0.32	0.21	-0.44	0.00	0.00 (tm)
SagM	-4.19	0.27	-0.16	0.43	0.32	-0.22	0.43	11.33	
SolV	5.47	1.28	0.08	1.20	1.28	0.09	1.20	9.16	Xaç (m)
SagV	-5.48	-1.28	-0.08	-1.20	-1.28	-0.09	-1.20	14.02	0.00
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
SolM	-1.70	4.98	-2.85	5.20	-0.04	-0.11	3.42		
SagM	1.66	-4.66	-4.32	3.46	0.05	-0.18	-3.48		
SolV	0.59	-0.63	-0.99	1.19	0.02	-0.04	4.54	Z1=	4.60m
SagV	-0.61	0.58	-0.99	1.18	-0.01	-0.04	-4.55	Z2=	4.60m
P118	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	51.56	14.69	7.14	7.54	6.54	14.76	8.08	0.00	0.00 (tm)
SagM	-51.56	-14.69	-7.14	-7.54	-6.54	-14.76	-8.08	9.26	
SolV	154.29	41.73	19.18	22.55	19.27	41.62	22.57	4.10	Xaç (m)
SagV	-447.70	-120.51	-55.92	-64.59	-55.42	-120.17	-65.43	12.22	0.00
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
SolM	0.95	-0.83	3.76	1.37	0.03	0.20	42.80		
SagM	-0.95	0.83	-3.76	-1.37	-0.03	-0.20	-42.80		
SolV	1.33	-1.08	-3.76	4.17	0.03	-0.27	128.06	Z1=	4.60m
SagV	-2.43	2.16	-8.29	7.75	-0.08	-0.42	-371.59	Z2=	4.60m
P119	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	-13.24	-3.18	-0.53	-2.65	-1.74	-3.06	-1.56	0.00	0.00 (tm)
SagM	3.24	1.03	-0.15	1.18	0.68	0.81	0.57	9.26	
SolV	4.27	0.75	0.52	0.24	0.50	0.74	0.27	4.10	Xaç (m)
SagV	-193.84	-39.12	-16.33	-22.80	-20.58	-40.22	-17.45	12.22	0.00
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
SolM	-0.26	0.31	-0.35	0.35	-0.01	0.00	-10.99		
SagM	-1.22	1.23	4.98	-4.54	-0.03	0.25	2.69		
SolV	-1.25	1.41	-0.88	0.78	-0.04	-0.03	3.54	Z1=	4.60m
SagV	-9.32	8.62	82.14	-75.32	-0.22	3.94	-160.89	Z2=	4.60m
P120	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	2.33	-0.10	-0.23	0.23	0.29	-0.15	-0.23	0.00	0.00 (tm)
SagM	0.37	-0.57	-0.45	-0.12	-0.13	-0.54	-0.46	11.33	
SolV	3.73	1.08	1.11	-0.03	-0.02	1.08	1.10	9.16	Xaç (m)
SagV	0.46	-1.49	-1.22	-0.27	-0.30	-1.43	-1.26	14.02	0.00
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
SolM	3.03	0.08	-0.37	2.13	0.09	-0.01	1.93		
SagM	3.63	-3.32	1.69	-1.38	0.09	0.07	0.31		
SolV	-0.12	0.07	-0.94	0.86	0.00	-0.04	3.10	Z1=	4.60m
SagV	8.85	-8.20	4.93	-4.07	0.22	0.20	0.38	Z2=	4.60m
P121	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Maçıklık
SolM	0.86	0.08	0.03	0.05	0.06	0.07	0.03	0.00	0.00 (tm)
SagM	-2.57	-0.48	-0.28	-0.19	-0.24	-0.44	-0.28	44.42	
SolV	0.43	-0.24	-0.16	-0.08	-0.10	-0.22	-0.15	-21.02	Xaç (m)
SagV	-1.57	-0.49	-0.34	-0.15	-0.18	-0.46	-0.34	44.20	0.00
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
SolM	0.35	-0.23	-2.66	2.18	0.00	-0.10	0.71		
SagM	-2.49	2.41	0.77	-2.07	-0.08	0.04	-2.14		
SolV	-1.86	2.13	-1.48	1.09	-0.06	-0.06	0.36	Z1=	4.60m
SagV	-1.69	1.84	0.26	-0.27	-0.05	0.03	-1.30	Z2=	4.60m

KTIP = 0 | , KTIP = 1 | , KTIP = 2 | , KTIP = 3 | , KTIP = 4 | , KTIP = 5 |

KİRİŞ BETONARME HESAP SONUÇLARI

Kiriş	üstMsol	altMsol	Mac.	üstMsağ	altMsağ	DONATI
K101 Mduz. (tm)	0.00	0.00	(1.57m)	0.00	0.00	4ø16(mon.)+2ø12(göv.)
A4 ✓ max M (tm)	5.74	0.00	0.33	0.00	3.00	4ø16(düz)
D=60 fcd (kg/cm ²)	233.33	0.00	233.33	0.00	233.33	
B=40 As' (cm ²)	0.00	0.00	0.00	0.00	0.00	
As (cm ²)	6.65	3.32	6.65	0.00	1.50	ø10/10(etriye)
Asw (cm ²)	3.23			3.57		Wk=0.24<0,4 ✓
K101 Mduz. (tm)	0.00	0.00	(0.00m)	0.00	0.00	4ø16(mon.)+2ø12(göv.)
A4 ✓ max M (tm)	0.00	-2.98	1.96	-1.76	0.00	4ø16(düz)
D=60 fcd (kg/cm ²)	0.00	233.33	233.33	233.33	0.00	
B=40 As' (cm ²)	0.00	0.00	0.00	0.00	0.00	
As (cm ²)	0.00	1.49	6.65	6.65	3.32	ø10/10(etriye)
Asw (cm ²)	3.06			3.74		Wk=0.24<0,4 ✓
K102 Mduz. (tm)	0.00	0.00	(4.15m)	0.00	0.00	5ø16(mon.)+2ø16(göv.)
A4 ✓ max M (tm)	-29.17	0.00	29.63	29.10	0.00	5ø20(düz)
D=60 fcd (kg/cm ²)	233.33	0.00	233.33	233.33	0.00	2ø20(sol üst ila.)+2ø20(sağ üst ila.)
B=60 As' (cm ²)	0.00	0.00	0.00	0.00	0.00	
As (cm ²)	15.17	7.58	14.99	15.13	7.56	2xø10/20/10(etriye)
Asw (cm ²)	13.60			13.60		Wk=0.31<0,4 ✓
K103 Mduz. (tm)	0.00	0.00	(4.15m)	0.00	0.00	6ø16(mon.)+2ø16(göv.)
A4 ✓ max M (tm)	-32.00	0.00	35.22	31.90	0.00	6ø20(düz)
D=60 fcd (kg/cm ²)	233.33	0.00	233.33	233.33	0.00	2ø20(sol üst ila.)+2ø20(sağ üst ila.)
B=60 As' (cm ²)	0.00	0.00	0.00	0.00	0.00	
As (cm ²)	16.71	8.36	17.88	16.65	8.33	2xø10/20/10(etriye)
Asw (cm ²)	13.60			13.60		Wk=0.29<0,4 ✓
K104 Mduz. (tm)	0.00	0.00	(4.15m)	0.00	0.00	5ø16(mon.)+2ø16(göv.)
A4 ✓ max M (tm)	-30.18	0.00	28.65	29.99	0.00	5ø20(düz)
D=60 fcd (kg/cm ²)	233.33	0.00	233.33	233.33	0.00	2ø20(sol üst ila.)+2ø20(sağ üst ila.)
B=60 As' (cm ²)	0.00	0.00	0.00	0.00	0.00	
As (cm ²)	15.71	7.86	14.49	15.61	7.81	2xø10/20/10(etriye)
Asw (cm ²)	13.60			13.60		Wk=0.31<0,4 ✓
K105 Mduz. (tm)	0.00	0.00	(1.85m)	0.00	0.00	3ø16(mon.)+2ø12(göv.)
A4 ✓ max M (tm)	-0.72	0.00	-0.16	1.69	0.00	3ø16(düz)
D=60 fcd (kg/cm ²)	233.33	0.00	0.00	233.33	0.00	
B=30 As' (cm ²)	0.00	0.00	0.00	0.00	0.00	
As (cm ²)	0.46	0.00	4.99	4.99	2.49	ø10/10(etriye)
Asw (cm ²)	0.00			2.55		Wk=0.24<0,4 ✓

Ck : Kiriş üstüne oturan kolonların Dinamik Etki çarpanı

A4 : (Ba=Bax+0.3*Bay,Ba=0.3*Bax+Bay)

KOLON STATİK HESAP SONUÇLARI

ANALİZLERDE, ÇATLAMIŞ KESİT ETKİN KESİT RİJİTLİK ÇARPANI DİKKATE ALINMIŞTIR TBDY2018 4.5.8

S101	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Material:E1
Üst Mx	0.05	0.01	0.00	0.01	0.01	0.01	0.01	0.13	
Alt Mx	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.14	I = 1
Üst My	-0.96	-0.24	-0.06	-0.18	-0.22	-0.08	-0.17	0.24	J = 0
Alt My	-0.45	-0.11	-0.02	-0.08	-0.10	-0.04	-0.08	0.28	
Tx	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.06	Bx= 30 cm
Ty	-0.31	-0.07	-0.02	-0.06	-0.07	-0.03	-0.05	0.11	By= 100 cm
Nz	8.66	0.51	-0.19	0.70	0.65	-0.35	0.72	-1.59	H = 4.60 m
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
Üst Mx	0.21	-0.24	-0.01	0.03	0.01	0.00	0.04		
Alt Mx	0.22	-0.25	0.00	0.01	0.01	0.00	0.02		
Üst My	-0.09	0.21	1.70	-2.17	-0.01	0.07	-0.79		
Alt My	-0.01	0.12	1.84	-2.33	0.00	0.08	-0.37		
Tx	0.09	-0.11	0.00	0.01	0.00	0.00	0.01		
Ty	-0.02	0.07	0.77	-0.98	0.00	0.03	-0.25		
Nz	-2.61	2.82	-2.93	3.50	-0.07	-0.12	7.19		
S102	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Material:E1
Üst Mx	0.43	0.08	0.01	0.07	0.06	0.04	0.06	1.09	
Alt Mx	0.17	0.04	0.01	0.03	0.02	0.02	0.03	1.17	I = 4
Üst My	-5.67	-1.37	-0.64	-0.73	-1.15	-0.90	-0.68	0.40	J = 0
Alt My	-2.89	-0.70	-0.33	-0.37	-0.59	-0.46	-0.35	0.26	
Tx	0.13	0.03	0.01	0.02	0.02	0.01	0.02	0.49	Bx= 100 cm
Ty	-1.86	-0.45	-0.21	-0.24	-0.38	-0.29	-0.22	0.14	By= 30 cm
Nz	37.38	7.94	3.77	4.17	7.03	4.77	4.07	-1.67	H = 4.60 m
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
Üst Mx	2.07	-2.36	-0.03	0.15	0.06	0.00	0.36		
Alt Mx	2.16	-2.47	0.05	0.06	0.06	0.00	0.14		
Üst My	-0.02	0.02	0.31	-0.38	0.00	0.01	-4.70		
Alt My	-0.01	0.02	0.33	-0.39	0.00	0.01	-2.40		
Tx	0.92	-1.05	0.01	0.05	0.03	0.00	0.11		
Ty	-0.01	0.01	0.14	-0.17	0.00	0.01	-1.54		
Nz	-0.66	0.71	-0.57	0.76	-0.02	-0.02	31.02		
S103	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Material:E1
Üst Mx	-0.03	-0.01	0.01	-0.02	0.00	-0.01	-0.01	0.93	
Alt Mx	-0.03	0.00	0.01	-0.01	0.00	0.00	0.00	0.95	I = 10
Üst My	-6.98	-1.68	-0.68	-1.00	-1.01	-1.50	-0.84	0.46	J = 0
Alt My	-3.56	-0.85	-0.35	-0.51	-0.51	-0.77	-0.43	0.29	
Tx	-0.01	0.00	0.00	-0.01	0.00	0.00	0.00	0.41	Bx= 100 cm
Ty	-2.29	-0.55	-0.22	-0.33	-0.33	-0.49	-0.27	0.16	By= 30 cm
Nz	43.32	9.52	3.96	5.56	5.61	8.67	4.75	-1.23	H = 4.60 m
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
Üst Mx	2.18	-2.48	0.01	0.11	0.07	0.00	-0.02		
Alt Mx	2.22	-2.52	0.02	0.10	0.07	0.00	-0.02		
Üst My	-0.01	0.01	0.38	-0.42	0.00	0.01	-5.79		
Alt My	0.00	0.01	0.39	-0.43	0.00	0.02	-2.95		
Tx	0.96	-1.09	0.01	0.04	0.03	0.00	-0.01		
Ty	0.00	0.00	0.17	-0.19	0.00	0.01	-1.90		
Nz	0.02	-0.02	0.21	-0.23	0.00	0.01	35.95		
S104	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Material:E1
Üst Mx	-0.33	-0.07	-0.02	-0.05	-0.06	-0.05	-0.02	0.77	
Alt Mx	-0.16	-0.03	0.00	-0.03	-0.03	-0.02	-0.01	0.76	I = 14
Üst My	-5.18	-1.24	-0.19	-1.05	-0.66	-1.20	-0.62	0.37	J = 0
Alt My	-2.64	-0.63	-0.10	-0.54	-0.34	-0.61	-0.32	0.24	
Tx	-0.11	-0.02	0.00	-0.02	-0.02	-0.02	-0.01	0.33	Bx= 100 cm
Ty	-1.70	-0.41	-0.06	-0.34	-0.22	-0.39	-0.20	0.13	By= 30 cm
Nz	33.64	7.21	0.83	6.38	3.73	7.14	3.54	-0.93	H = 4.60 m
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
Üst Mx	2.21	-2.51	-0.01	0.13	0.07	0.00	-0.27		
Alt Mx	2.24	-2.54	-0.05	0.17	0.07	0.00	-0.13		
Üst My	0.00	0.00	0.36	-0.36	0.00	0.01	-4.30		
Alt My	0.00	0.00	0.37	-0.37	0.00	0.01	-2.19		
Tx	0.97	-1.10	-0.01	0.07	0.03	0.00	-0.09		
Ty	0.00	0.00	0.16	-0.16	0.00	0.01	-1.41		
Nz	0.10	-0.10	-0.24	0.16	0.00	-0.01	27.92		
S105	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	_QQ_QQ	Q_QQ_Q	Zemin	Material:E1
Üst Mx	-0.30	-0.06	-0.02	-0.04	-0.04	-0.05	-0.03	0.60	
Alt Mx	-0.13	-0.02	0.00	-0.02	-0.02	-0.02	-0.01	0.59	I = 18
Üst My	-0.14	-0.03	-0.01	-0.02	-0.02	-0.03	-0.02	0.07	J = 0
Alt My	-0.07	-0.02	-0.01	-0.01	-0.01	-0.02	-0.01	0.06	
Tx	-0.09	-0.02	0.00	-0.01	-0.01	-0.01	-0.01	0.26	Bx= 100 cm
Ty	-0.04	-0.01	0.00	-0.01	-0.01	-0.01	-0.01	0.03	By= 30 cm
Nz	3.12	-0.17	-0.08	-0.09	-0.05	-0.08	-0.21	0.30	H = 4.60 m
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
Üst Mx	2.18	-2.47	-0.05	0.17	0.07	0.00	-0.25		
Alt Mx	2.23	-2.52	-0.09	0.22	0.07	0.00	-0.11		
Üst My	0.00	-0.01	0.26	-0.25	0.00	0.01	-0.11		
Alt My	0.00	-0.01	0.27	-0.25	0.00	0.01	-0.05		
Tx	0.96	-1.09	-0.03	0.08	0.03	0.00	-0.08		
Ty	0.00	0.00	0.12	-0.11	0.00	0.00	-0.04		
Nz	0.31	-0.33	-1.24	1.12	0.01	-0.05	2.59		

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S106	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin	Material:El
Üst Mx	-0.16	-0.03	0.00	-0.03	-0.02	-0.02	-0.02	0.47	
Alt Mx	-0.07	-0.01	0.00	-0.01	-0.01	0.00	-0.01	0.48	I = 24
Üst My	-0.18	-0.04	-0.03	-0.01	-0.01	-0.04	-0.03	0.17	J = 0
Alt My	-0.09	-0.02	-0.02	0.00	0.00	-0.02	-0.02	0.13	
Tx	-0.05	-0.01	0.00	-0.01	-0.01	0.00	0.00	0.21	Bx= 100 cm
Ty	-0.06	-0.01	-0.01	0.00	0.00	-0.01	-0.01	0.07	By= 30 cm
Nz	5.83	0.40	0.27	0.14	0.21	0.41	0.19	-0.32	H = 4.60 m
Deprem+X	2.12	-2.41	-0.09	0.22	0.07	0.00	-0.14		
Alt Mx	2.19	-2.48	-0.14	0.26	0.07	-0.01	-0.06		
Üst My	0.00	-0.01	0.18	-0.15	0.00	0.01	-0.15		
Alt My	-0.01	0.00	0.20	-0.17	0.00	0.01	-0.07		
Tx	0.94	-1.06	-0.05	0.11	0.03	0.00	-0.04		
Ty	0.00	0.00	0.08	-0.07	0.00	0.00	-0.05		
Nz	0.80	-0.86	-1.72	1.53	0.03	-0.08	4.84		
S107	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin	Material:El
Üst Mx	-0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.06	
Alt Mx	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.06	I = 30
Üst My	-0.27	-0.05	-0.06	0.01	0.01	-0.05	-0.06	0.27	J = 0
Alt My	-0.11	-0.02	-0.02	0.00	0.00	-0.02	-0.02	0.27	
Tx	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.02	Bx= 30 cm
Ty	-0.08	-0.02	-0.02	0.00	0.00	-0.02	-0.02	0.12	By= 100 cm
Nz	5.79	0.30	0.15	0.15	0.18	0.28	0.15	0.57	H = 4.60 m
Deprem+X	0.22	-0.24	0.01	0.01	0.01	0.00	-0.01		
Alt Mx	0.22	-0.25	0.00	0.01	0.01	0.00	0.00		
Üst My	0.08	-0.19	1.53	-1.18	0.01	0.07	-0.23		
Alt My	0.02	-0.13	1.64	-1.27	0.00	0.08	-0.09		
Tx	0.09	-0.11	0.00	0.00	0.00	0.00	0.00		
Ty	0.02	-0.07	0.69	-0.53	0.00	0.03	-0.07		
Nz	1.34	-1.43	-2.24	1.94	0.04	-0.10	4.80		
S108	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin	Material:El
Üst Mx	0.04	0.02	-0.13	0.15	0.12	0.02	-0.10	0.20	
Alt Mx	0.03	0.01	-0.07	0.08	0.06	0.01	-0.05	0.12	I = 25
Üst My	-1.03	-0.24	-0.11	-0.13	-0.11	-0.24	-0.13	0.41	J = 0
Alt My	-0.47	-0.11	-0.05	-0.06	-0.05	-0.11	-0.06	0.38	
Tx	0.02	0.01	-0.04	0.05	0.04	0.01	-0.03	0.07	Bx= 30 cm
Ty	-0.33	-0.08	-0.03	-0.04	-0.04	-0.08	-0.04	0.17	By= 100 cm
Nz	15.67	2.74	0.26	2.47	2.06	2.74	0.67	0.58	H = 4.60 m
Deprem+X	0.31	-0.34	0.00	0.01	0.01	0.00	0.04		
Alt Mx	0.31	-0.33	0.00	0.01	0.01	0.00	0.02		
Üst My	0.02	-0.05	2.39	-2.20	0.00	0.10	-0.86		
Alt My	0.01	-0.04	2.45	-2.25	0.00	0.10	-0.39		
Tx	0.13	-0.14	0.00	0.00	0.00	0.00	0.01		
Ty	0.01	-0.02	1.05	-0.97	0.00	0.04	-0.27		
Nz	0.29	-0.32	-0.86	0.77	0.00	-0.04	13.01		
S109	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin	Material:El
Üst Mx	0.54	0.14	0.16	-0.02	-0.01	0.14	0.15	-0.39	
Alt Mx	0.28	0.07	0.08	-0.01	-0.01	0.07	0.08	-0.24	I = 31
Üst My	-0.28	-0.06	-0.06	0.01	0.01	-0.06	-0.06	0.13	J = 0
Alt My	-0.11	-0.02	-0.03	0.00	0.00	-0.02	-0.03	0.13	
Tx	0.18	0.05	0.05	-0.01	0.00	0.05	0.05	-0.14	Bx= 30 cm
Ty	-0.09	-0.02	-0.02	0.00	0.00	-0.02	-0.02	0.06	By= 100 cm
Nz	12.13	1.72	1.78	-0.06	0.00	1.71	1.73	-1.42	H = 4.60 m
Deprem+X	0.28	-0.30	0.02	0.00	0.01	0.00	0.44		
Alt Mx	0.29	-0.31	0.00	0.01	0.01	0.00	0.23		
Üst My	0.06	-0.16	1.52	-1.17	0.00	0.07	-0.23		
Alt My	0.03	-0.13	1.60	-1.24	0.00	0.07	-0.09		
Tx	0.12	-0.13	0.00	0.00	0.00	0.00	0.15		
Ty	0.02	-0.06	0.68	-0.52	0.00	0.03	-0.07		
Nz	0.48	-0.48	-1.18	0.97	0.02	-0.05	10.07		
S110	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin	Material:El
Üst Mx	0.06	0.01	0.00	0.01	0.01	0.01	0.01	0.12	
Alt Mx	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.13	I = 5
Üst My	0.99	0.24	0.06	0.18	0.22	0.09	0.18	-0.25	J = 0
Alt My	0.48	0.11	0.03	0.08	0.10	0.04	0.08	-0.29	
Tx	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.06	Bx= 30 cm
Ty	0.32	0.08	0.02	0.06	0.07	0.03	0.06	-0.12	By= 100 cm
Nz	8.60	0.50	-0.19	0.70	0.65	-0.36	0.72	-1.55	H = 4.60 m
Deprem+X	0.23	-0.21	0.01	-0.03	0.01	0.00	0.05		
Alt Mx	0.24	-0.22	0.00	-0.01	0.01	0.00	0.02		
Üst My	0.17	-0.04	1.71	-2.17	0.00	0.07	0.82		
Alt My	0.08	0.04	1.84	-2.33	0.00	0.08	0.39		
Tx	0.10	-0.09	0.00	-0.01	0.00	0.00	0.01		
Ty	0.05	0.00	0.77	-0.98	0.00	0.03	0.26		
Nz	-2.76	2.59	2.92	-3.52	-0.07	0.12	7.14		

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S111	GGGGGG	QQQQQQ	Q_Q_Q	-Q_Q_Q	QQ_QQ	-QQ_QQ	Q_QQ_Q	Zemin	Material:El
Üst Mx	0.45	0.09	0.02	0.07	0.06	0.05	0.07	1.05	
Alt Mx	0.19	0.04	0.01	0.03	0.03	0.03	0.03	1.13	I = 6
Üst My	5.67	1.37	0.64	0.73	1.15	0.90	0.68	-0.40	J = 0
Alt My	2.89	0.70	0.33	0.37	0.59	0.46	0.35	-0.26	
Tx	0.14	0.03	0.01	0.02	0.02	0.02	0.02	0.47	Bx= 100 cm
Ty	1.86	0.45	0.21	0.24	0.38	0.29	0.22	-0.14	By= 30 cm
Nz	37.15	7.90	3.74	4.17	7.02	4.74	4.04	-1.64	H = 4.60 m
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
Üst Mx	2.29	-2.02	0.02	-0.14	0.05	0.00	0.37		
Alt Mx	2.39	-2.11	-0.06	-0.04	0.05	0.00	0.16		
Üst My	0.02	-0.01	0.31	-0.38	0.00	0.01	4.70		
Alt My	0.01	0.00	0.33	-0.39	0.00	0.01	2.40		
Tx	1.02	-0.90	-0.01	-0.04	0.02	0.00	0.12		
Ty	0.01	0.00	0.14	-0.17	0.00	0.01	1.54		
Nz	-0.72	0.67	0.53	-0.73	-0.02	0.02	30.83		
S112	GGGGGG	QQQQQQ	Q_Q_Q	-Q_Q_Q	QQ_QQ	-QQ_QQ	Q_QQ_Q	Zemin	Material:El
Üst Mx	-0.05	-0.01	0.01	-0.02	0.00	-0.01	-0.01	0.88	
Alt Mx	-0.02	0.00	0.01	-0.01	0.00	0.00	0.00	0.90	I = 11
Üst My	6.97	1.67	0.68	1.00	1.01	1.50	0.84	-0.46	J = 0
Alt My	3.56	0.85	0.35	0.51	0.51	0.77	0.43	-0.29	
Tx	-0.02	0.00	0.00	-0.01	0.00	0.00	0.00	0.39	Bx= 100 cm
Ty	2.29	0.55	0.22	0.33	0.33	0.49	0.27	-0.16	By= 30 cm
Nz	43.23	9.49	3.92	5.57	5.62	8.65	4.72	-1.19	H = 4.60 m
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
Üst Mx	2.40	-2.12	-0.02	-0.08	0.05	0.00	-0.04		
Alt Mx	2.44	-2.16	-0.03	-0.07	0.06	0.00	-0.02		
Üst My	0.01	0.00	0.38	-0.42	0.00	0.01	5.79		
Alt My	0.00	0.00	0.39	-0.43	0.00	0.02	2.95		
Tx	1.05	-0.93	-0.01	-0.03	0.02	0.00	-0.01		
Ty	0.00	0.00	0.17	-0.19	0.00	0.01	1.90		
Nz	-0.08	0.07	-0.24	0.26	0.00	-0.01	35.88		
S113	GGGGGG	QQQQQQ	Q_Q_Q	-Q_Q_Q	QQ_QQ	-QQ_QQ	Q_QQ_Q	Zemin	Material:El
Üst Mx	-0.48	-0.09	-0.04	-0.05	-0.06	-0.08	-0.04	0.72	
Alt Mx	-0.21	-0.04	-0.01	-0.03	-0.03	-0.03	-0.02	0.70	I = 15
Üst My	5.17	1.24	0.19	1.05	0.67	1.20	0.62	-0.37	J = 0
Alt My	2.64	0.63	0.10	0.54	0.34	0.61	0.32	-0.24	
Tx	-0.15	-0.03	-0.01	-0.02	-0.02	-0.02	-0.01	0.31	Bx= 100 cm
Ty	1.70	0.41	0.06	0.35	0.22	0.39	0.20	-0.13	By= 30 cm
Nz	34.70	7.36	0.92	6.43	3.77	7.29	3.65	-0.91	H = 4.60 m
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
Üst Mx	2.40	-2.13	-0.03	-0.08	0.05	0.00	-0.40		
Alt Mx	2.44	-2.16	0.03	-0.14	0.06	0.00	-0.17		
Üst My	0.00	0.00	0.35	-0.36	0.00	0.01	4.29		
Alt My	0.00	0.00	0.37	-0.37	0.00	0.01	2.19		
Tx	1.05	-0.93	0.00	-0.05	0.02	0.00	-0.12		
Ty	0.00	0.00	0.16	-0.16	0.00	0.01	1.41		
Nz	-0.12	0.10	0.40	-0.29	0.00	0.01	28.80		
S114	GGGGGG	QQQQQQ	Q_Q_Q	-Q_Q_Q	QQ_QQ	-QQ_QQ	Q_QQ_Q	Zemin	Material:El
Üst Mx	-0.53	-0.10	-0.06	-0.04	-0.04	-0.09	-0.07	0.60	
Alt Mx	-0.22	-0.04	-0.02	-0.02	-0.02	-0.03	-0.03	0.57	I = 19
Üst My	0.16	0.04	0.01	0.02	0.02	0.04	0.02	-0.06	J = 0
Alt My	0.08	0.02	0.01	0.01	0.01	0.02	0.01	-0.05	
Tx	-0.16	-0.03	-0.02	-0.01	-0.01	-0.03	-0.02	0.25	Bx= 100 cm
Ty	0.05	0.01	0.00	0.01	0.01	0.01	0.01	-0.02	By= 30 cm
Nz	6.93	0.42	0.42	0.00	0.02	0.51	0.31	0.12	H = 4.60 m
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
Üst Mx	2.30	-2.03	-0.03	-0.08	0.05	0.00	-0.44		
Alt Mx	2.37	-2.10	0.04	-0.15	0.05	0.00	-0.18		
Üst My	-0.01	0.01	0.25	-0.24	0.00	0.01	0.13		
Alt My	-0.01	0.01	0.26	-0.24	0.00	0.01	0.07		
Tx	1.01	-0.90	0.00	-0.05	0.02	0.00	-0.14		
Ty	0.00	0.00	0.11	-0.10	0.00	0.00	0.04		
Nz	0.19	-0.21	1.92	-1.70	0.01	0.08	5.75		
S115	GGGGGG	QQQQQQ	Q_Q_Q	-Q_Q_Q	QQ_QQ	-QQ_QQ	Q_QQ_Q	Zemin	Material:El
Üst Mx	-0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.02	
Alt Mx	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.02	I = 26
Üst My	0.15	0.05	0.06	-0.01	-0.01	0.05	0.06	-0.26	J = 0
Alt My	0.12	0.03	0.03	-0.01	-0.01	0.03	0.03	-0.27	
Tx	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	Bx= 30 cm
Ty	0.06	0.02	0.02	0.00	0.00	0.02	0.02	-0.12	By= 100 cm
Nz	11.94	1.25	1.12	0.13	0.16	1.23	1.11	-0.04	H = 4.60 m
Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y	Deprem Z			
Üst Mx	0.23	-0.21	0.00	-0.02	0.01	0.00	-0.01		
Alt Mx	0.24	-0.22	0.01	-0.02	0.01	0.00	0.00		
Üst My	-0.14	0.04	1.39	-1.06	0.00	0.06	0.12		
Alt My	-0.04	-0.06	1.54	-1.19	0.00	0.07	0.10		
Tx	0.10	-0.09	0.00	-0.01	0.00	0.00	0.00		
Ty	-0.04	0.00	0.64	-0.49	0.00	0.03	0.05		
Nz	2.65	-2.50	3.37	-2.94	0.06	0.14	9.91		

KOLON BETONARME HESAP SONUÇLARI

Kolon			N (t)	minor M	major M	fcd	ρ	As	Donatı
S101	Bx=30	X- (G+Q)	12.951	-1.47	0.31	233.3	0.0020	6.00	2x5ø14+2x5ø14 (govde)
	By=100	X- (G+Q+E)	14.151	-1.40	0.45	233.3	0.0020	6.00	ø10/8 (ettriye)
I:1		Y- (G+Q)	12.951	0.09	-1.72	233.3	0.0020	6.00	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	12.680	0.10	-3.38	233.3	0.0020	6.00	
	$\beta x = 1.000$	X- (G-E)	2.822	-0.17	0.27	233.3	0.0020	6.00	
A4 ✓	$\beta y = 1.000$	Y- (G-E)	2.136	0.06	1.61	233.3	0.0020	6.00	$\Sigma As / Ac = 0.0103$
S102	Bx=100	X- (G+Q)	65.031	-9.72	2.93	233.3	0.0020	6.00	2x5ø14+2x5ø14 (govde)
	By=30	X- (G+Q+E)	55.338	-8.07	4.11	233.3	0.0020	6.00	ø10/8 (ettriye)
I:4		Y- (G+Q)	65.031	0.73	-10.12	233.3	0.0020	6.00	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	46.075	0.77	-7.42	233.3	0.0020	6.00	
	$\beta x = 1.000$	X- (G-E)	23.616	-1.86	2.59	233.3	0.0020	6.00	
A4 ✓	$\beta y = 1.000$	Y- (G-E)	23.572	0.17	-1.48	233.3	0.0020	6.00	$\Sigma As / Ac = 0.0103$
S103	Bx=100	X- (G+Q)	75.877	-5.24	-3.41	233.3	0.0020	6.00	2x5ø14+2x5ø14 (govde)
	By=30	X- (G+Q+E)	63.642	-4.50	3.49	233.3	0.0020	6.00	ø10/8 (ettriye)
I:10		Y- (G+Q)	75.877	-0.05	-12.45	233.3	0.0021	6.41	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	53.064	0.07	-9.08	233.3	0.0020	6.00	
	$\beta x = 1.000$	X- (G-E)	28.182	-4.54	-2.46	233.3	0.0020	6.00	
A4 ✓	$\beta y = 1.000$	Y- (G-E)	27.974	0.08	-2.75	233.3	0.0020	6.00	$\Sigma As / Ac = 0.0103$
S104	Bx=100	X- (G+Q)	58.628	-3.45	-2.64	233.3	0.0020	6.00	2x5ø14+2x5ø14 (govde)
	By=30	X- (G+Q+E)	49.323	-3.05	3.23	233.3	0.0020	6.00	ø10/8 (ettriye)
I:14		Y- (G+Q)	58.628	-0.57	-9.24	233.3	0.0020	6.00	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	41.003	-0.35	-6.78	233.3	0.0020	6.00	
	$\beta x = 1.000$	X- (G-E)	21.801	-1.72	-2.59	233.3	0.0020	6.00	
A4 ✓	$\beta y = 1.000$	Y- (G-E)	21.891	-0.14	-1.70	233.3	0.0020	6.00	$\Sigma As / Ac = 0.0103$
S105	Bx=100	X- (G+Q)	4.847	-0.03	0.76	233.3	0.0020	6.00	2x5ø14+2x5ø14 (govde)
	By=30	X- (G+Q+E)	4.526	-0.02	3.08	233.3	0.0020	6.00	ø10/8 (ettriye)
I:18		Y- (G+Q)	4.847	-0.52	-0.24	233.3	0.0020	6.00	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	4.660	-0.39	-0.43	233.3	0.0020	6.00	
	$\beta x = 1.000$	X- (G-E)	1.705	-0.05	-2.55	233.3	0.0020	6.00	
A4 ✓	$\beta y = 1.000$	Y- (G-E)	0.793	-0.24	0.18	233.3	0.0020	6.00	$\Sigma As / Ac = 0.0103$
S106	Bx=100	X- (G+Q)	8.808	-0.02	0.68	233.3	0.0020	6.00	2x5ø14+2x5ø14 (govde)
	By=30	X- (G+Q+E)	8.544	0.00	3.00	233.3	0.0020	6.00	ø10/8 (ettriye)
I:24		Y- (G+Q)	8.808	-0.27	-0.31	233.3	0.0020	6.00	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	7.954	-0.14	-0.40	233.3	0.0020	6.00	
	$\beta x = 1.000$	X- (G-E)	2.937	-0.13	-2.45	233.3	0.0020	6.00	
A4 ✓	$\beta y = 1.000$	Y- (G-E)	2.075	-0.20	0.07	233.3	0.0020	6.00	$\Sigma As / Ac = 0.0103$
S107	Bx=30	X- (G+Q)	9.500	0.07	-0.23	233.3	0.0020	6.00	2x5ø14+2x5ø14 (govde)
	By=100	X- (G+Q+E)	9.529	0.23	0.31	233.3	0.0020	6.00	ø10/8 (ettriye)
I:30		Y- (G+Q)	9.500	-0.01	-0.48	233.3	0.0020	6.00	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	10.343	0.06	1.83	233.3	0.0020	6.00	
	$\beta x = 1.000$	X- (G-E)	2.339	-0.37	-0.25	233.3	0.0020	6.00	
A4 ✓	$\beta y = 1.000$	Y- (G-E)	1.526	0.00	1.41	233.3	0.0020	6.00	$\Sigma As / Ac = 0.0103$
S108	Bx=30	X- (G+Q)	27.250	-1.26	0.65	233.3	0.0020	6.00	2x5ø14+2x5ø14 (govde)
	By=100	X- (G+Q+E)	23.211	-0.97	0.75	233.3	0.0020	6.00	ø10/8 (ettriye)
I:25		Y- (G+Q)	27.250	0.09	-1.84	233.3	0.0020	6.00	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	19.848	0.07	-3.68	233.3	0.0020	6.00	
	$\beta x = 1.000$	X- (G-E)	9.886	-0.72	-0.31	233.3	0.0020	6.00	
A4 ✓	$\beta y = 1.000$	Y- (G-E)	9.346	0.03	1.74	233.3	0.0020	6.00	$\Sigma As / Ac = 0.0103$
S109	Bx=30	X- (G+Q)	19.736	-0.49	1.00	233.3	0.0020	6.00	2x5ø14+2x5ø14 (govde)
	By=100	X- (G+Q+E)	17.350	-0.25	1.13	233.3	0.0020	6.00	ø10/8 (ettriye)
I:31		Y- (G+Q)	19.736	0.99	-0.89	233.3	0.0020	6.00	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	18.052	0.34	1.53	233.3	0.0020	6.00	
	$\beta x = 1.000$	X- (G-E)	7.420	-0.12	0.08	233.3	0.0020	6.00	
A4 ✓	$\beta y = 1.000$	Y- (G-E)	6.717	0.36	1.38	233.3	0.0020	6.00	$\Sigma As / Ac = 0.0103$
S110	Bx=30	X- (G+Q)	12.846	1.51	0.31	233.3	0.0020	6.00	2x5ø14+2x5ø14 (govde)
	By=100	X- (G+Q+E)	14.006	1.38	0.44	233.3	0.0020	6.00	ø10/8 (ettriye)
I:5		Y- (G+Q)	12.846	0.09	1.76	233.3	0.0020	6.00	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	14.762	0.11	3.69	233.3	0.0020	6.00	
	$\beta x = 1.000$	X- (G-E)	2.836	0.39	0.26	233.3	0.0020	6.00	
A4 ✓	$\beta y = 1.000$	Y- (G-E)	2.080	0.01	-1.47	233.3	0.0020	6.00	$\Sigma As / Ac = 0.0103$
S111	Bx=100	X- (G+Q)	64.653	9.71	2.91	233.3	0.0020	6.00	2x5ø14+2x5ø14 (govde)
	By=30	X- (G+Q+E)	55.018	8.06	4.03	233.3	0.0020	6.00	ø10/8 (ettriye)
I:6		Y- (G+Q)	64.653	0.77	10.12	233.3	0.0020	6.00	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	55.031	0.79	8.83	233.3	0.0020	6.00	
	$\beta x = 1.000$	X- (G-E)	23.469	1.89	2.53	233.3	0.0020	6.00	
A4 ✓	$\beta y = 1.000$	Y- (G-E)	23.456	0.09	1.49	233.3	0.0020	6.00	$\Sigma As / Ac = 0.0103$
S112	Bx=100	X- (G+Q)	75.708	5.24	-3.41	233.3	0.0020	6.00	2x5ø14+2x5ø14 (govde)
	By=30	X- (G+Q+E)	63.561	4.50	3.36	233.3	0.0020	6.00	ø10/8 (ettriye)
I:11		Y- (G+Q)	75.708	-0.08	12.44	233.3	0.0021	6.41	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	63.740	0.01	10.81	233.3	0.0020	6.00	
	$\beta x = 1.000$	X- (G-E)	28.063	4.55	2.39	233.3	0.0020	6.00	
A4 ✓	$\beta y = 1.000$	Y- (G-E)	27.884	-0.09	2.75	233.3	0.0020	6.00	$\Sigma As / Ac = 0.0103$

KOLON BETONARME HESAP SONUÇLARI

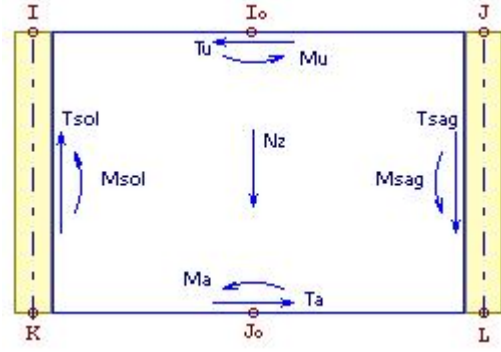
Kolon			N (t)	minor M	major M	fcd	ρ	As	Donatı
S113	Bx=100	X- (G+Q)	60.353	3.45	-2.72	233.3	0.0020	6.00	2×5ø14+2×5ø14 (govde)
	By=30	X- (G+Q+E)	50.818	3.05	3.02	233.3	0.0020	6.00	ø10/8 (ettriye)
I:15		Y- (G+Q)	60.353	-0.82	9.22	233.3	0.0020	6.00	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	50.988	-0.61	8.05	233.3	0.0020	6.00	
	$\beta_x = 1.000$	X- (G-E)	22.473	3.36	2.12	233.3	0.0020	6.00	
A4 ✓	$\beta_y = 1.000$	Y- (G-E)	22.189	-0.10	1.35	233.3	0.0020	6.00	$\Sigma As/Ac=0.0103$
S114	Bx=100	X- (G+Q)	10.576	0.28	-0.90	233.3	0.0020	6.00	2×5ø14+2×5ø14 (govde)
	By=30	X- (G+Q+E)	9.392	0.04	2.82	233.3	0.0020	6.00	ø10/8 (ettriye)
I:19		Y- (G+Q)	10.576	-0.90	0.28	233.3	0.0020	6.00	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	11.120	-0.80	0.49	233.3	0.0020	6.00	
	$\beta_x = 1.000$	X- (G-E)	4.323	0.04	-2.47	233.3	0.0020	6.00	
A4 ✓	$\beta_y = 1.000$	Y- (G-E)	2.595	-0.38	-0.15	233.3	0.0020	6.00	$\Sigma As/Ac=0.0103$
S115	Bx=30	X- (G+Q)	18.708	-0.06	-0.45	233.3	0.0020	6.00	2×5ø14+2×5ø14 (govde)
	By=100	X- (G+Q+E)	18.803	0.14	0.45	233.3	0.0020	6.00	ø10/8 (ettriye)
I:26		Y- (G+Q)	18.708	-0.01	0.84	233.3	0.0020	6.00	Cx:1 Cy:1
J:0	Hk=4.6m	Y- (G+Q+E)	19.527	0.01	1.74	233.3	0.0020	6.00	
	$\beta_x = 1.000$	X- (G-E)	5.124	-0.05	-0.23	233.3	0.0020	6.00	
A4 ✓	$\beta_y = 1.000$	Y- (G-E)	4.400	0.00	-1.25	233.3	0.0020	6.00	$\Sigma As/Ac=0.0103$

 β_x, β_y : Kolon Moment büyütme katsayısı

Cx, Cy : Güçlü kolon Moment büyütme katsayısı

Ck : Kiriş üstüne oturan kolonların Dinamik Etki çarpanı

A4 : (Ba=Bax+0.3*Bay, Ba=0.3*Bax+Bay)

**PANEL STATİK HESAP SONUÇLARI (tm)**

ANALİZLERDE, ÇATLAMIŞ KESİT ETKİN KESİT RİJİTLİK ÇARPANI DİKKATE ALINMIŞTIR TBDY2018 4.5.8

P106	I=1 Üst Mx	J=4 Alt Mx	Io=2 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:El		Nz
GGGGGG	5.90	-1.71	-2.75	-1.50	2.23	0.91	-6.94	-14.04	-8.05	8.39	1.8
QQQQQQ	0.53	-0.49	-0.66	-0.36	0.57	0.22	-1.60	-2.74	-1.95	2.01	-1.1
Q_Q_Q	0.01	-0.14	-0.30	-0.16	0.20	0.10	-0.47	-1.13	-0.87	1.01	-0.6
_Q_Q_Q	0.52	-0.35	-0.36	-0.20	0.38	0.12	-1.14	-1.61	-1.08	1.00	-0.4
QQ_QQ	0.45	-0.36	-0.61	-0.30	0.39	0.19	-1.48	-2.02	-1.66	1.67	-0.5
_QQ_QQ	0.13	-0.33	-0.36	-0.24	0.42	0.13	-0.62	-2.03	-1.21	1.42	-1.4
Q_QQ_Q	0.48	-0.30	-0.35	-0.18	0.34	0.11	-1.11	-1.44	-1.03	0.93	-0.3
Zemin	-0.75	0.27	0.39	0.16	7.10	-0.08	0.00	11.33	0.65	-0.28	-5.8
Deprem+X	-3.47	-1.45	0.00	0.00	12.88	0.00	0.22	2.35	0.00	0.01	-13.3
Deprem-X	4.27	2.01	0.03	0.02	-14.94	-0.02	-0.29	-2.56	-0.01	-0.01	14.5
Deprem+Y	4.26	5.53	0.48	0.34	-1.46	-0.35	0.38	3.91	-0.03	0.00	-8.9
Deprem-Y	-5.64	-7.07	-0.61	-0.42	2.71	0.45	-0.52	-4.75	0.01	0.01	10.5
Deprem Z	4.90	-1.42	-2.28	-1.25	1.85	0.76	-5.76	-11.66	0.00	0.00	1.5
Rüzgar X	-0.12	-0.06	0.00	0.00	0.40	0.00	0.00	0.06	0.00	0.00	-0.3
Rüzgar Y	0.18	0.23	0.02	0.01	-0.06	-0.01	0.02	0.16	0.00	0.00	-0.3
P107	I=4 Üst Mx	J=10 Alt Mx	Io=7 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:El		Nz
GGGGGG	2.22	0.48	-5.79	-2.96	0.44	1.89	13.79	-15.37	3.64	2.91	-4.2
QQQQQQ	0.42	0.14	-1.39	-0.71	0.18	0.46	2.81	-3.28	0.86	0.68	-2.2
Q_Q_Q	0.07	0.06	-0.66	-0.30	0.09	0.20	0.30	-0.38	0.23	0.07	-0.9
_Q_Q_Q	0.35	0.09	-0.74	-0.41	0.10	0.25	2.51	-2.90	0.64	0.61	-1.3
QQ_QQ	0.30	0.09	-1.04	-0.50	0.11	0.33	1.82	-2.01	0.03	-0.13	-1.4
_QQ_QQ	0.25	0.13	-1.06	-0.57	0.14	0.36	1.71	-2.30	1.27	1.10	-2.0
Q_QQ_Q	0.29	0.07	-0.69	-0.35	0.11	0.23	2.07	-2.25	0.43	0.40	-1.1
Zemin	3.00	3.02	0.44	0.28	4.97	-0.15	0.00	11.33	0.07	0.06	-5.6
Deprem+X	4.54	4.99	-0.01	-0.01	11.63	0.00	-2.88	1.62	-0.01	-0.01	-16.8
Deprem-X	-5.23	-5.71	0.01	0.01	-13.27	-0.01	3.16	-1.98	0.01	0.01	19.2
Deprem+Y	0.11	0.44	0.32	0.34	0.05	-0.14	-3.22	2.80	-0.05	-0.05	-0.2
Deprem-Y	0.19	-0.22	-0.38	-0.39	0.63	0.16	4.10	-3.71	0.05	0.05	-0.6
Deprem Z	1.84	0.40	-4.81	-2.46	0.36	1.57	11.45	-12.76	0.00	0.00	-3.5
Rüzgar X	0.13	0.15	0.00	0.00	0.36	0.00	-0.08	0.04	0.00	0.00	-0.5
Rüzgar Y	0.00	0.02	0.01	0.01	0.00	-0.01	-0.13	0.12	0.00	0.00	-0.0
P108	I=10 Üst Mx	J=14 Alt Mx	Io=12 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:El		Nz
GGGGGG	-0.64	0.62	-6.43	-2.65	-1.05	1.81	15.02	-8.70	-1.46	-2.15	-2.6
QQQQQQ	-0.17	0.21	-1.54	-0.64	-0.18	0.44	3.31	-1.95	-0.35	-0.52	-1.7
Q_Q_Q	-0.04	0.10	-0.47	-0.19	-0.02	0.13	1.27	-0.81	-0.69	-0.69	-0.6
_Q_Q_Q	-0.13	0.12	-1.08	-0.45	-0.15	0.30	2.04	-1.14	0.34	0.17	-1.0
QQ_QQ	-0.11	0.14	-0.88	-0.36	-0.15	0.25	2.76	-1.83	-0.36	-0.39	-1.1
_QQ_QQ	-0.14	0.19	-1.43	-0.59	-0.13	0.40	2.34	-1.49	-0.17	-0.35	-1.4
Q_QQ_Q	-0.09	0.10	-0.78	-0.32	-0.07	0.22	1.52	-0.58	-0.17	-0.32	-0.9
Zemin	2.70	2.42	0.48	0.26	3.82	-0.16	0.00	11.33	0.29	0.27	-3.7
Deprem+X	4.81	5.71	0.00	0.00	11.02	0.00	-2.73	-0.49	-0.01	-0.01	-15.3
Deprem-X	-5.51	-6.51	0.00	0.00	-12.54	0.00	2.98	0.07	0.00	0.00	17.4
Deprem+Y	0.37	-0.01	0.36	0.36	-0.22	-0.17	-2.50	1.60	-0.05	-0.04	0.3
Deprem-Y	-0.11	0.33	-0.38	-0.38	0.88	0.18	2.68	-2.03	0.05	0.04	-1.3
Deprem Z	-0.53	0.51	-5.34	-2.20	-0.87	1.50	12.46	-7.22	0.00	0.00	-2.2
Rüzgar X	0.14	0.17	0.00	0.00	0.35	0.00	-0.08	-0.02	0.00	0.00	-0.4
Rüzgar Y	0.01	0.00	0.01	0.01	0.00	-0.01	-0.10	0.07	0.00	0.00	0.0
P109	I=14 Üst Mx	J=18 Alt Mx	Io=16 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:El		Nz
GGGGGG	-0.54	1.23	-2.28	-1.11	-1.83	0.84	6.87	1.99	11.09	-0.02	2.7
QQQQQQ	-0.36	0.26	-0.55	-0.27	-0.40	0.20	1.62	0.45	2.66	-0.01	-0.4
Q_Q_Q	-0.24	0.21	-0.09	-0.04	-0.32	0.04	0.53	0.08	0.41	0.00	-0.0
_Q_Q_Q	-0.12	0.06	-0.46	-0.22	-0.09	0.16	1.09	0.37	2.25	0.00	-0.4
QQ_QQ	-0.19	0.06	-0.29	-0.14	-0.11	0.11	0.65	0.36	1.39	0.00	-0.3
_QQ_QQ	-0.23	0.29	-0.53	-0.26	-0.35	0.19	1.53	0.40	2.56	-0.01	-0.3
Q_QQ_Q	-0.30	0.18	-0.27	-0.13	-0.35	0.10	1.06	0.13	1.37	0.00	-0.2
Zemin	2.83	2.91	0.28	0.16	3.39	-0.13	0.00	11.33	-0.35	0.00	-1.4
Deprem+X	10.83	13.05	0.01	0.00	9.03	0.00	-0.93	0.04	0.01	0.00	-3.4
Deprem-X	-12.24	-14.76	-0.01	0.00	-10.32	0.00	1.03	-0.05	-0.01	0.00	4.0
Deprem+Y	-4.86	-4.97	0.33	0.37	1.67	-0.36	-1.34	-0.82	0.01	0.00	-5.5
Deprem-Y	5.14	5.40	-0.32	-0.36	-0.94	0.34	1.11	0.80	-0.01	0.00	4.8
Deprem Z	-0.45	1.02	-1.90	-0.93	-1.52	0.70	5.70	1.65	0.00	0.00	2.3
Rüzgar X	0.35	0.42	0.00	0.00	0.29	0.00	-0.03	0.00	0.00	0.00	-0.1
Rüzgar Y	-0.20	-0.20	0.01	0.02	0.08	-0.01	-0.06	-0.03	0.00	0.00	-0.2

PANEL STATİK HESAP SONUÇLARI (tm)

P110	I=18 Üst Mx	J=24 Alt Mx	Io=20 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:E1		Nz
GGGGGG	-0.72	-0.48	-0.14	-0.06	0.34	0.10	-4.02	5.49	-0.27	0.17	4.3
QQQQQQ	-0.18	-0.09	-0.03	-0.01	0.14	0.02	-2.22	1.51	-0.06	0.03	0.2
Q_Q_Q	-0.07	-0.03	-0.01	-0.01	-0.05	0.01	-1.16	0.81	-0.10	0.10	-0.0
_Q_Q_Q	-0.11	-0.05	-0.02	-0.01	0.19	0.01	-1.06	0.70	0.05	-0.06	0.3
QQ_QQ	-0.10	-0.05	-0.02	-0.01	0.16	0.01	-1.16	0.83	0.03	-0.04	0.3
_QQ_QQ	-0.16	-0.09	-0.03	-0.01	0.16	0.02	-1.93	1.37	-0.06	0.03	0.3
Q_QQ_Q	-0.10	-0.05	-0.02	-0.01	-0.04	0.01	-1.33	0.81	-0.08	0.07	-0.0
Zemin	0.85	0.65	0.09	0.06	1.41	-0.07	0.00	11.33	0.34	-0.34	-1.3
Deprem+X	1.50	1.64	-0.02	0.00	7.27	0.00	5.11	-3.18	0.08	-0.08	-5.2
Deprem-X	-1.72	-1.88	0.02	0.00	-8.25	0.00	-5.66	3.49	-0.08	0.08	6.0
Deprem+Y	0.96	0.87	0.19	0.19	-2.39	-0.25	-2.55	1.26	-0.15	0.15	-4.4
Deprem-Y	-0.78	-0.69	-0.17	-0.17	2.70	0.23	2.13	-0.99	0.14	-0.14	3.6
Deprem Z	-0.60	-0.40	-0.11	-0.05	0.28	0.09	-3.33	4.56	0.00	0.00	3.6
Rüzgar X	0.05	0.05	0.00	0.00	0.24	0.00	0.20	-0.09	0.00	0.00	-0.1
Rüzgar Y	0.04	0.04	0.01	0.01	-0.09	-0.01	-0.11	0.06	0.00	0.00	-0.1
P111	I=24 Üst Mx	J=30 Alt Mx	Io=27 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:E1		Nz
GGGGGG	0.06	-0.03	-0.04	-0.03	0.56	0.03	-4.89	1.34	0.54	-0.54	3.4
QQQQQQ	0.03	0.02	-0.01	-0.01	0.14	0.01	-1.41	0.62	0.12	-0.12	0.0
Q_Q_Q	0.07	0.04	-0.01	-0.01	0.17	0.01	-0.77	0.50	0.10	-0.10	-0.1
_Q_Q_Q	-0.04	-0.02	0.00	0.00	-0.03	0.00	-0.64	0.12	0.02	-0.02	0.1
QQ_QQ	-0.02	-0.01	0.00	0.00	-0.01	0.00	-0.77	0.15	0.03	-0.03	0.1
_QQ_QQ	0.05	0.03	-0.01	-0.01	0.15	0.01	-1.28	0.58	0.12	-0.12	0.0
Q_QQ_Q	0.03	0.02	-0.01	-0.01	0.13	0.01	-0.76	0.51	0.10	-0.10	-0.1
Zemin	0.95	0.96	0.07	0.05	0.23	-0.04	0.00	44.42	-0.31	0.30	0.1
Deprem+X	5.18	5.09	0.02	0.00	4.70	0.00	0.61	-0.61	-0.04	0.04	-2.9
Deprem-X	-5.83	-5.74	-0.03	-0.01	-5.37	0.01	-0.59	0.56	0.03	-0.03	3.5
Deprem+Y	-1.15	-1.01	0.14	0.15	0.48	-0.14	-1.33	2.42	0.08	-0.08	-3.1
Deprem-Y	1.30	1.18	-0.11	-0.12	-0.02	0.11	0.86	-1.94	-0.08	0.08	2.3
Deprem Z	0.05	-0.02	-0.03	-0.02	0.47	0.02	-4.05	1.12	0.00	0.00	2.8
Rüzgar X	0.17	0.17	0.00	0.00	0.16	0.00	0.01	0.00	0.00	0.00	-0.1
Rüzgar Y	-0.05	-0.04	0.01	0.01	0.03	-0.01	-0.07	0.11	0.00	0.00	-0.1
P112	I=5 Üst Mx	J=6 Alt Mx	Io=8 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:E1		Nz
GGGGGG	5.81	-1.82	2.75	1.50	2.41	-0.92	-6.97	-14.51	8.04	-8.38	1.7
QQQQQQ	0.52	-0.51	0.66	0.36	0.60	-0.22	-1.61	-2.80	1.95	-2.01	-1.1
Q_Q_Q	0.00	-0.16	0.30	0.16	0.22	-0.10	-0.47	-1.18	0.86	-1.01	-0.7
_Q_Q_Q	0.52	-0.35	0.36	0.20	0.38	-0.12	-1.14	-1.62	1.08	-1.00	-0.4
QQ_QQ	0.45	-0.36	0.61	0.30	0.39	-0.19	-1.48	-2.02	1.66	-1.66	-0.5
_QQ_QQ	0.12	-0.34	0.36	0.24	0.45	-0.13	-0.63	-2.09	1.21	-1.42	-1.4
Q_QQ_Q	0.47	-0.31	0.36	0.18	0.37	-0.11	-1.11	-1.49	1.02	-0.93	-0.3
Zemin	-0.66	0.35	-0.40	-0.17	6.82	0.08	0.00	11.33	-0.65	0.28	-5.6
Deprem+X	-4.00	-1.83	0.02	0.01	14.43	-0.01	0.31	2.67	0.00	-0.01	-14.3
Deprem-X	3.24	1.29	0.01	0.00	-12.53	-0.01	-0.24	-2.48	0.00	0.01	13.2
Deprem+Y	-4.24	-5.53	0.48	0.34	1.43	-0.35	-0.39	-4.00	-0.03	0.00	9.0
Deprem-Y	5.60	7.06	-0.61	-0.42	-2.60	0.45	0.52	4.83	0.01	0.01	-10.6
Deprem Z	4.83	-1.51	2.28	1.25	2.00	-0.76	-5.79	-12.04	0.00	0.00	1.4
Rüzgar X	-0.08	-0.03	0.00	0.00	0.33	0.00	0.01	0.07	0.00	0.00	-0.3
Rüzgar Y	-0.18	-0.23	0.02	0.01	0.06	-0.01	-0.02	-0.17	0.00	0.00	0.3
P113	I=6 Üst Mx	J=11 Alt Mx	Io=9 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:E1		Nz
GGGGGG	2.31	0.69	5.79	2.96	0.37	-1.89	14.87	-16.99	-3.63	-2.90	-4.2
QQQQQQ	0.44	0.18	1.39	0.71	0.18	-0.46	2.96	-3.51	-0.86	-0.68	-2.3
Q_Q_Q	0.09	0.08	0.66	0.30	0.08	-0.20	0.43	-0.59	-0.23	-0.07	-0.9
_Q_Q_Q	0.35	0.10	0.74	0.41	0.10	-0.25	2.53	-2.92	-0.64	-0.61	-1.3
QQ_QQ	0.30	0.10	1.04	0.50	0.11	-0.33	1.83	-2.03	-0.03	0.13	-1.4
_QQ_QQ	0.27	0.16	1.06	0.57	0.14	-0.36	1.87	-2.53	-1.27	-1.10	-2.0
Q_QQ_Q	0.31	0.10	0.69	0.35	0.11	-0.23	2.21	-2.47	-0.43	-0.40	-1.1
Zemin	2.92	2.94	-0.44	-0.28	4.71	0.15	0.00	11.33	-0.07	-0.06	-5.2
Deprem+X	5.13	5.54	0.01	0.01	12.83	-0.01	-3.19	1.88	0.01	0.01	-18.6
Deprem-X	-4.49	-4.88	-0.01	0.00	-11.32	0.00	3.01	-1.89	-0.01	-0.01	16.5
Deprem+Y	-0.12	-0.43	0.32	0.34	-0.11	-0.14	3.73	-3.52	-0.05	-0.04	0.3
Deprem-Y	-0.16	0.24	-0.38	-0.39	-0.50	0.16	-3.97	3.50	0.05	0.04	0.4
Deprem Z	1.92	0.57	4.80	2.46	0.31	-1.57	12.34	-14.10	0.00	0.00	-3.5
Rüzgar X	0.12	0.13	0.00	0.00	0.29	0.00	-0.08	0.05	0.00	0.00	-0.4
Rüzgar Y	0.00	-0.02	0.01	0.01	-0.01	-0.01	0.15	-0.14	0.00	0.00	0.0
P114	I=11 Üst Mx	J=15 Alt Mx	Io=13 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:E1		Nz
GGGGGG	-0.72	0.97	6.42	2.65	-1.53	-1.81	17.13	-12.09	1.47	2.16	-1.3
QQQQQQ	-0.18	0.27	1.54	0.64	-0.24	-0.44	3.62	-2.49	0.35	0.52	-1.5
Q_Q_Q	-0.04	0.15	0.46	0.19	-0.09	-0.13	1.54	-1.34	0.69	0.70	-0.5
_Q_Q_Q	-0.14	0.12	1.08	0.45	-0.15	-0.31	2.08	-1.15	-0.34	-0.17	-1.0
QQ_QQ	-0.11	0.14	0.88	0.36	-0.15	-0.25	2.78	-1.85	0.36	0.38	-1.0
_QQ_QQ	-0.14	0.25	1.43	0.59	-0.20	-0.40	2.65	-2.03	0.17	0.35	-1.3
Q_QQ_Q	-0.09	0.15	0.78	0.32	-0.13	-0.22	1.80	-1.11	0.17	0.32	-0.7
Zemin	2.64	2.29	-0.47	-0.26	3.55	0.16	0.00	11.33	-0.29	-0.28	-3.3
Deprem+X	5.44	6.32	0.00	0.00	12.02	0.00	-3.02	-0.86	0.00	0.00	-16.8
Deprem-X	-4.79	-5.59	0.00	0.00	-10.63	0.00	2.78	0.50	0.00	0.00	14.9
Deprem+Y	-0.42	0.05	0.35	0.36	0.07	-0.17	2.93	-2.68	-0.04	-0.03	-0.0
Deprem-Y	0.17	-0.33	-0.38	-0.38	-0.68	0.18	-3.07	2.28	0.04	0.03	1.0
Deprem Z	-0.60	0.80	5.33	2.20	-1.27	-1.50	14.22	-10.03	0.00	0.00	-1.1
Rüzgar X	0.12	0.14	0.00	0.00	0.28	0.00	-0.07	-0.02	0.00	0.00	-0.3
Rüzgar Y	-0.02	0.00	0.01	0.01	0.00	-0.01	0.12	-0.11	0.00	0.00	0.0

PANEL STATİK HESAP SONUÇLARI (tm)

P115	I=15 Üst Mx	J=19 Alt Mx	Io=17 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:E1		Nz
GGGGGG	-3.77	0.52	2.37	1.12	-1.88	-0.84	11.25	2.24	-11.01	0.02	5.2
QQQQQQ	-0.77	0.15	0.57	0.27	-0.41	-0.20	2.32	0.32	-2.64	0.01	-0.1
Q_Q_Q	-0.45	0.12	0.10	0.04	-0.26	-0.04	1.24	-0.04	-0.40	0.00	0.2
Q_Q_Q	-0.32	0.02	0.47	0.22	-0.14	-0.16	1.09	0.36	-2.24	0.01	-0.3
QQ_QQ	-0.37	0.02	0.30	0.14	-0.15	-0.11	0.67	0.34	-1.38	0.00	-0.3
QQ_QQ	-0.65	0.17	0.55	0.26	-0.36	-0.19	2.23	0.27	-2.54	0.01	0.0
Q_QQ_Q	-0.52	0.10	0.28	0.13	-0.31	-0.10	1.75	0.02	-1.35	0.00	0.0
Zemin	2.82	3.35	-0.33	-0.14	2.52	0.09	0.00	11.33	0.37	0.00	-0.3
Deprem+X	11.08	14.01	-0.01	-0.01	9.58	0.01	-0.33	-1.00	-0.02	0.00	-3.9
Deprem-X	-9.84	-12.47	0.01	0.00	-8.41	0.00	0.27	0.93	0.02	0.00	3.3
Deprem+Y	5.79	5.82	0.45	0.40	-2.25	-0.42	2.31	1.08	0.00	0.00	7.2
Deprem-Y	-5.92	-6.08	-0.43	-0.39	1.53	0.40	-1.99	-0.99	0.00	0.00	-6.3
Deprem Z	-3.13	0.43	1.97	0.93	-1.56	-0.69	9.34	1.86	0.00	0.00	4.3
Rüzgar X	0.25	0.32	0.00	0.00	0.22	0.00	-0.01	-0.03	0.00	0.00	-0.0
Rüzgar Y	0.23	0.23	0.02	0.02	-0.09	-0.02	0.10	0.04	0.00	0.00	0.3
P116	I=19 Üst Mx	J=26 Alt Mx	Io=22 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:E1		Nz
GGGGGG	-4.05	-0.90	0.36	0.13	-0.02	-0.17	46.02	-46.02	-0.08	0.92	13.7
QQQQQQ	-0.61	-0.19	0.09	0.03	0.08	-0.03	7.57	-7.57	-0.03	0.24	1.3
Q_Q_Q	-0.48	0.05	0.06	0.02	-0.02	-0.02	7.09	-7.09	-0.07	0.23	1.0
Q_Q_Q	-0.14	-0.23	0.02	0.01	0.11	-0.01	0.48	-0.48	0.04	0.01	0.2
QQ_QQ	-0.13	-0.17	0.02	0.00	0.10	-0.01	0.99	-0.99	0.03	0.01	0.3
QQ_QQ	-0.53	-0.18	0.08	0.03	0.11	-0.03	7.75	-7.75	-0.03	0.24	1.3
Q_QQ_Q	-0.56	-0.02	0.07	0.02	-0.05	-0.03	6.40	-6.40	-0.06	0.23	1.0
Zemin	0.62	1.51	-0.29	-0.08	2.02	0.05	0.00	11.33	0.30	-0.27	0.2
Deprem+X	3.82	15.07	-0.01	-0.01	13.72	0.01	22.04	-22.04	0.02	0.02	1.2
Deprem-X	-3.61	-13.68	-0.01	-0.01	-11.96	0.01	-4.24	4.24	-0.02	-0.02	-1.6
Deprem+Y	-2.24	-0.10	0.49	0.40	1.68	-0.57	28.32	-28.32	-0.01	0.03	13.8
Deprem-Y	2.58	0.05	-0.41	-0.34	-2.62	0.49	-1.42	1.42	0.00	-0.02	-11.8
Deprem Z	-3.36	-0.75	0.30	0.11	-0.02	-0.14	38.20	-38.20	0.00	0.00	11.4
Rüzgar X	0.09	0.36	0.00	0.00	0.31	0.00	0.55	-0.55	0.00	0.00	0.0
Rüzgar Y	-0.08	0.01	0.02	0.02	0.05	-0.02	1.17	-1.17	0.00	0.00	0.5
P117	I=1 Üst Mx	J=5 Alt Mx	Io=3 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:E1		Nz
GGGGGG	-1.78	-1.02	-0.54	-0.50	-0.61	0.23	4.12	-4.19	5.57	0.01	25.2
QQQQQQ	-0.45	-0.26	-0.07	-0.05	-0.15	0.03	-0.28	0.27	1.40	0.00	2.9
Q_Q_Q	-0.11	-0.06	-0.07	-0.08	-0.04	0.03	0.15	-0.16	0.34	0.00	0.1
Q_Q_Q	-0.34	-0.19	0.00	0.03	-0.12	-0.01	-0.42	0.43	1.06	0.00	2.8
QQ_QQ	-0.43	-0.25	0.00	0.02	-0.15	-0.01	-0.32	0.32	1.33	0.00	3.0
QQ_QQ	-0.14	-0.08	-0.07	-0.05	-0.05	0.03	0.21	-0.22	0.42	0.00	0.0
Q_QQ_Q	-0.34	-0.19	-0.07	-0.08	-0.11	0.03	-0.44	0.43	1.05	0.00	2.8
Zemin	0.74	0.79	0.23	0.12	0.33	-0.08	0.00	11.33	-0.66	0.01	-1.0
Deprem+X	0.41	0.66	-1.62	-1.50	0.23	0.68	-1.70	1.66	-0.07	0.00	-4.1
Deprem-X	-0.41	-0.67	-3.11	-3.18	-0.23	1.37	4.98	-4.66	0.06	0.00	4.2
Deprem+Y	0.00	0.00	-42.61	-88.30	0.00	28.46	-2.85	-4.32	0.03	0.00	0.0
Deprem-Y	0.00	0.00	54.99	111.16	0.00	-36.12	5.20	3.46	-0.04	0.00	-0.0
Deprem Z	-1.48	-0.85	-0.45	-0.41	-0.51	0.19	3.42	-3.48	0.00	0.00	20.9
Rüzgar X	0.01	0.02	0.10	0.11	0.01	-0.05	-0.04	0.05	0.00	0.00	-0.1
Rüzgar Y	0.00	0.00	-1.79	-3.67	0.00	1.19	-0.11	-0.18	0.00	0.00	0.0
P118	I=25 Üst Mx	J=19 Alt Mx	Io=23 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:E1		Nz
GGGGGG	0.44	0.24	4.95	-6.08	0.16	1.53	51.56	-51.56	-0.77	-1.12	29.9
QQQQQQ	0.10	0.06	-0.61	-1.17	0.04	0.26	14.69	-14.69	-0.18	-0.25	4.7
Q_Q_Q	-0.23	-0.14	0.20	-0.86	-0.09	0.12	7.14	-7.14	0.24	0.58	2.3
Q_Q_Q	0.33	0.20	-0.81	-0.32	0.13	0.14	7.54	-7.54	-0.43	-0.83	2.3
QQ_QQ	0.26	0.16	-0.62	-0.26	0.10	0.13	6.54	-6.54	-0.32	-0.68	2.0
QQ_QQ	0.10	0.06	-0.49	-1.15	0.04	0.26	14.76	-14.76	-0.18	-0.24	4.7
Q_QQ_Q	-0.16	-0.10	-0.11	-0.93	-0.06	0.13	8.08	-8.08	0.14	0.42	2.5
Zemin	0.28	0.27	1.46	4.22	0.13	1.04	0.00	9.26	0.21	-0.25	3.1
Deprem+X	0.43	0.65	1.14	1.09	0.26	-0.64	0.95	-0.95	0.11	-0.11	0.3
Deprem-X	-0.42	-0.63	-0.81	-0.53	-0.25	0.13	-0.83	0.83	-0.10	0.10	-0.5
Deprem+Y	-0.01	0.00	-19.28	-46.88	0.00	34.86	3.76	-3.76	-0.02	-0.01	13.7
Deprem-Y	0.00	0.00	17.78	42.82	0.00	-31.95	1.37	-1.37	0.02	0.01	-12.5
Deprem Z	0.37	0.20	4.11	-5.05	0.13	1.27	42.80	-42.80	0.00	0.00	24.8
Rüzgar X	0.01	0.01	0.02	0.02	0.01	0.00	0.03	-0.03	0.00	0.00	0.0
Rüzgar Y	0.00	0.00	-0.79	-1.85	0.00	1.42	0.20	-0.20	0.00	0.00	0.5
P119	I=18 Üst Mx	J=25 Alt Mx	Io=21 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:E1		Nz
GGGGGG	0.02	0.01	4.40	1.48	0.01	-1.23	-13.24	3.24	-0.34	-0.26	7.1
QQQQQQ	0.01	0.00	1.01	0.37	0.00	-0.29	-3.18	1.03	-0.11	-0.05	0.8
Q_Q_Q	-0.07	-0.03	0.44	0.15	-0.02	-0.12	-0.53	-0.15	0.50	-0.56	0.3
Q_Q_Q	0.07	0.04	0.57	0.22	0.02	-0.16	-2.65	1.18	-0.61	0.51	0.4
QQ_QQ	0.06	0.03	0.48	0.18	0.02	-0.14	-1.74	0.68	-0.48	0.39	0.4
QQ_QQ	0.01	0.00	0.98	0.36	0.00	-0.28	-3.06	0.81	-0.10	-0.06	0.8
Q_QQ_Q	-0.05	-0.02	0.55	0.20	-0.02	-0.16	-1.56	0.57	0.36	-0.43	0.3
Zemin	0.12	0.08	-1.82	-1.59	0.04	0.72	0.00	9.26	-0.60	0.67	0.0
Deprem+X	0.18	0.17	0.01	0.07	0.08	-0.02	-0.26	-1.22	-0.08	0.08	0.3
Deprem-X	-0.20	-0.19	0.12	0.05	-0.08	-0.04	0.31	1.23	0.10	-0.10	-0.3
Deprem+Y	0.00	0.00	-8.15	-8.20	0.00	3.43	-0.35	4.98	0.00	0.01	-0.9
Deprem-Y	0.00	0.01	7.47	7.52	0.00	-3.14	0.35	-4.54	0.01	-0.01	0.8
Deprem Z	0.01	0.01	3.66	1.23	0.00	-1.02	-10.99	2.69	0.00	0.00	5.9
Rüzgar X	0.01	0.01	0.00	0.00	0.00	0.00	-0.01	-0.03	0.00	0.00	0.0
Rüzgar Y	0.00	0.00	-0.34	-0.34	0.00	0.14	0.00	0.25	0.00	0.00	-0.0

PANEL STATİK HESAP SONUÇLARI (tm)

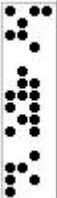
P120	I=31 Üst Mx	J=26 Alt Mx	Io=29 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:E1		Nz
GGGGGG	0.88	0.48	13.28	-2.63	0.30	0.35	2.33	0.37	-1.79	0.00	21.2
QQQQQQ	0.24	0.13	1.24	-0.66	0.08	-0.03	-0.10	-0.57	-0.49	0.00	2.1
Q_Q_Q	0.26	0.14	0.98	-0.79	0.09	-0.02	-0.23	-0.45	-0.51	0.00	1.9
_Q_Q_Q	-0.02	-0.01	0.26	0.13	-0.01	-0.01	0.23	-0.12	0.02	0.00	0.1
QQ_QQ	-0.01	-0.01	0.31	0.13	0.00	0.00	0.29	-0.13	0.02	0.00	0.2
_QQ_QQ	0.24	0.13	1.19	-0.68	0.08	-0.03	-0.15	-0.54	-0.49	0.00	2.1
Q_QQ_Q	0.25	0.14	0.97	-0.77	0.08	-0.02	-0.23	-0.46	-0.51	0.00	1.9
Zemin	-0.51	-0.39	0.26	5.05	-0.21	-0.79	0.00	11.33	0.25	0.00	2.0
Deprem+X	0.36	0.60	4.91	-1.52	0.22	0.09	3.03	3.63	-0.04	0.00	2.9
Deprem-X	-0.35	-0.59	-3.42	3.38	-0.21	-1.72	0.08	-3.32	0.04	0.00	-3.3
Deprem+Y	0.01	0.01	-11.64	-37.40	0.01	22.22	-0.37	1.69	0.04	0.00	9.3
Deprem-Y	-0.01	-0.01	8.33	29.55	-0.01	-17.06	2.13	-1.38	-0.03	0.00	-7.3
Deprem Z	0.73	0.40	11.02	-2.18	0.25	0.29	1.93	0.31	0.00	0.00	17.6
Rüzgar X	0.01	0.01	0.08	-0.09	0.01	0.06	0.09	0.09	0.00	0.00	0.1
Rüzgar Y	0.00	0.00	-0.55	-1.58	0.00	0.98	-0.01	0.07	0.00	0.00	0.4
P121	I=30 Üst Mx	J=31 Alt Mx	Io=32 Üst My	Jo=0 Alt My	K=0 Tx	L=0 Ty	SolM	SagM	Material:E1		Nz
GGGGGG	0.17	0.09	1.03	-0.31	0.06	-0.13	0.86	-2.57	1.16	1.31	4.5
QQQQQQ	0.04	0.02	0.16	0.02	0.01	-0.03	0.08	-0.48	0.30	0.33	0.2
Q_Q_Q	0.05	0.03	0.19	0.04	0.02	-0.04	0.03	-0.28	0.33	0.38	0.2
_Q_Q_Q	-0.01	0.00	-0.03	-0.02	0.00	0.01	0.05	-0.19	-0.04	-0.04	0.0
QQ_QQ	0.00	0.00	-0.04	-0.03	0.00	0.01	0.06	-0.24	-0.02	-0.03	0.1
_QQ_QQ	0.05	0.02	0.17	0.02	0.01	-0.03	0.07	-0.44	0.30	0.34	0.2
Q_QQ_Q	0.05	0.02	0.20	0.05	0.02	-0.04	0.03	-0.28	0.32	0.36	0.2
Zemin	-0.15	-0.09	-0.29	-0.38	-0.05	0.12	0.00	44.42	-0.69	-0.54	0.5
Deprem+X	0.16	0.14	-0.28	-0.23	0.06	0.08	0.35	-2.49	-0.07	0.01	0.8
Deprem-X	-0.18	-0.16	0.58	0.51	-0.07	-0.19	-0.23	2.41	0.07	-0.02	-0.9
Deprem+Y	0.01	0.00	-3.68	-3.54	0.00	1.38	-2.66	0.77	0.04	0.04	-1.1
Deprem-Y	0.00	0.01	2.80	2.69	0.00	-1.05	2.18	-2.07	-0.04	-0.03	1.0
Deprem Z	0.14	0.07	0.85	-0.26	0.05	-0.11	0.71	-2.14	0.00	0.00	3.7
Rüzgar X	0.01	0.00	-0.02	-0.02	0.00	0.01	0.00	-0.08	0.00	0.00	0.0
Rüzgar Y	0.00	0.00	-0.17	-0.16	0.00	0.06	-0.10	0.04	0.00	0.00	-0.0

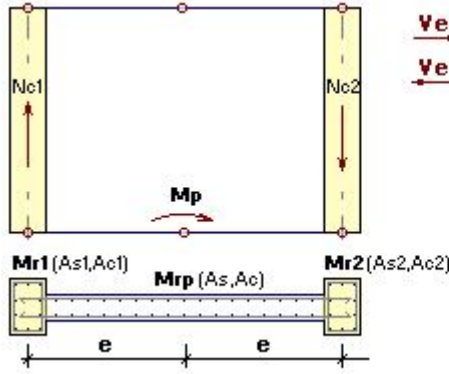
PANEL BETONARME HESAP SONUÇLARI

Panel			N (t)	maxM	fcd	ρ	As	Donatı
P106	Bx=190 By=30 I/J :2/0 Hk = 4.600 m Asw= 7.50 cm ² /m	X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Zemin)	2.609 12.883 2.609 12.418 2.609	9.11 13.54 -4.90 -4.02 0.00	233.3 233.3 233.3 233.3 233.3	0.0010 0.0010 0.0046 0.0013 0.0046	5.70 5.70 26.22 7.13 13.80	2×11ø18 (düşey) ø10/20 (yatay)
P107	Bx=150 By=30 I/J :7/0 Hk = 4.600 m Asw= 7.50 cm ² /m	X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Zemin)	-3.828 13.889 -3.828 -3.626 -3.828	8.59 11.43 -10.34 -7.56 0.00	233.3 233.3 233.3 233.3 233.3	0.0013 0.0010 0.0049 0.0016 0.0045	5.99 4.50 21.96 7.33 13.59	2×9ø18 (düşey) ø10/20 (yatay)
P108	Bx=150 By=30 I/J :12/0 Hk = 4.600 m Asw= 7.50 cm ² /m	X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Zemin)	-2.406 14.073 -2.406 -1.305 -2.406	5.08 9.92 -11.47 -8.36 0.00	233.3 233.3 233.3 233.3 233.3	0.0010 0.0010 0.0048 0.0024 0.0046	4.50 4.50 21.62 10.72 13.76	2×9ø18 (düşey) ø10/20 (yatay)
P109	Bx=120 By=30 I/J :16/0 Hk = 4.600 m Asw= 7.50 cm ² /m	X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Zemin)	3.878 7.469 3.878 8.349 3.878	6.85 19.50 -4.08 -3.17 0.00	233.3 233.3 233.3 233.3 233.3	0.0010 0.0010 0.0039 0.0013 0.0039	3.60 3.60 14.18 4.50 11.81	2×6ø18 (düşey) ø10/20 (yatay)
P110	Bx=120 By=30 I/J :20/0 Hk = 4.600 m Asw= 7.50 cm ² /m	X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Zemin)	6.544 10.639 6.544 9.112 6.544	-1.30 -2.62 -0.24 -0.36 0.00	233.3 233.3 233.3 233.3 233.3	0.0010 0.0010 0.0038 0.0013 0.0038	3.60 3.60 13.72 4.50 11.44	2×6ø18 (düşey) ø10/20 (yatay)
P111	Bx=80 By=30 I/J :27/0 Hk = 4.600 m Asw= 7.50 cm ² /m	X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Zemin)	5.158 8.025 5.158 7.670 5.158	1.73 6.94 -0.12 0.18 0.00	233.3 233.3 233.3 233.3 233.3	0.0010 0.0010 0.0158 0.0013 0.0158	2.40 2.40 37.92 3.00 47.34	2×8ø26 (düşey) ø10/20 (yatay)
P112	Bx=190 By=30 I/J :8/0 Hk = 4.600 m Asw= 7.50 cm ² /m	X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Zemin)	2.403 12.790 2.403 12.790 2.403	8.97 13.38 4.91 4.71 0.00	233.3 233.3 233.3 233.3 233.3	0.0010 0.0010 0.0046 0.0013 0.0046	5.70 5.70 26.26 7.13 13.81	2×11ø18 (düşey) ø10/20 (yatay)
P113	Bx=150 By=30 I/J :9/0 Hk = 4.600 m Asw= 7.50 cm ² /m	X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Zemin)	-3.840 13.305 -3.840 -4.863 -3.840	8.62 11.38 10.33 9.00 0.00	233.3 233.3 233.3 233.3 233.3	0.0013 0.0010 0.0049 0.0020 0.0045	5.99 4.50 21.96 9.22 13.59	2×9ø18 (düşey) ø10/20 (yatay)
P114	Bx=150 By=30 I/J :13/0 Hk = 4.600 m Asw= 7.50 cm ² /m	X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Zemin)	-1.244 15.136 -1.244 -0.721 -1.244	5.45 10.09 11.45 9.94 0.00	233.3 233.3 233.3 233.3 233.3	0.0010 0.0010 0.0047 0.0028 0.0046	4.50 4.50 21.34 12.54 13.89	2×9ø18 (düşey) ø10/20 (yatay)
P115	Bx=120 By=30 I/J :17/0 Hk = 4.600 m Asw= 7.50 cm ² /m	X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Zemin)	7.441 10.548 7.441 13.869 7.441	-6.51 18.18 4.22 3.98 0.00	233.3 233.3 233.3 233.3 233.3	0.0010 0.0010 0.0038 0.0013 0.0038	3.60 3.60 13.60 4.50 11.32	2×7ø16 (düşey) ø10/20 (yatay)
P116	Bx=300 By=30 I/J :22/0 Hk = 4.600 m Asw= 7.50 cm ² /m	X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) Y-(Zemin)	21.855 20.023 21.855 32.647 21.855	-6.65 15.95 0.64 1.02 0.00	233.3 233.3 233.3 233.3 233.3	0.0010 0.0010 0.0043 0.0013 0.0043	9.00 9.00 38.35 11.25 12.78	2×16ø18 (düşey) ø10/20 (yatay)
P117	Bx=30 By=660 I/J :3/0 Hk = 4.600 m Asw= 7.50 cm ² /m	X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) X-(Zemin)	40.050 32.405 40.050 34.490 40.050	-3.22 -2.65 -8.53 110.81 0.00	233.3 233.3 233.3 233.3 233.3	0.0043 0.0013 0.0010 0.0010 0.0043	85.75 24.76 19.81 19.81 12.99	2×43ø16 (düşey) ø10/20 (yatay)
P118	Bx=30 By=550 I/J :23/0 Hk = 4.600 m Asw= 7.50 cm ² /m	X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) X-(Zemin)	54.496 45.645 54.496 51.559 54.496	1.60 1.60 -10.39 -54.13 0.00	233.3 233.3 233.3 233.3 233.3	0.0033 0.0013 0.0010 0.0010 0.0033	53.66 20.63 16.51 16.51 9.75	2×35ø14 (düşey) ø10/20 (yatay)
P119	Bx=30 By=150 I/J :21/0 Hk = 4.600 m Asw= 7.50 cm ² /m	X-(G+Q) X-(G+Q+E) Y-(G+Q) Y-(G+Q+E) X-(Zemin)	11.462 10.152 11.462 10.793 11.462	0.33 0.41 7.77 14.65 0.00	233.3 233.3 233.3 233.3 233.3	0.0029 0.0013 0.0010 0.0010 0.0029	13.25 5.62 4.50 4.50 8.84	2×7ø16 (düşey) ø10/20 (yatay)

PANEL BETONARME HESAP SONUÇLARI

Panel			N (t)	maxM	fcd	ρ	As	Donatı
P120	Bx=30 By=480	X- (G+Q)	36.427	1.65	233.3	0.0042	61.13	2×31ø16 (düşey)
	I/J :29/0	X- (G+Q+E)	33.638	1.72	233.3	0.0013	18.01	ø10/20 (yatay)
	Hk = 4.600 m	Y- (G+Q)	36.427	20.98	233.3	0.0010	14.41	
	Asw= 7.50 cm ² /m	Y- (G+Q+E)	40.027	40.61	233.3	0.0010	14.41	
		X- (Zemin)	36.427	0.00	233.3	0.0042	12.73	
P121	Bx=30 By=80	X- (G+Q)	7.696	0.32	233.3	0.0156	37.46	2×8ø26 (düşey)
	I/J :32/0	X- (G+Q+E)	7.413	0.44	233.3	0.0013	3.00	ø10/20 (yatay)
	Hk = 4.600 m	Y- (G+Q)	7.696	1.75	233.3	0.0010	2.40	
	Asw= 7.50 cm ² /m	Y- (G+Q+E)	7.693	5.16	233.3	0.0010	2.40	
		X- (Zemin)	7.696	0.00	233.3	0.0156	46.82	





$$\overrightarrow{V_e} \quad Mr1=As1 f_{yd} e, \quad Mr2=0.85 A_{c2} f_{cd} + As2 f_{yd} e$$

$$\overleftarrow{V_e} \quad Mr1=0.85 A_{c1} f_{cd} + As1 f_{yd} e, \quad Mr2=As2 f_{yd} e$$

$$M_d = (M_{c1} + N_{c1} \cdot e) + (M_{c2} + N_{c2} \cdot e) + M_p$$

$$M_r = M_{rp} + M_{r1} + M_{r2} > M_d$$

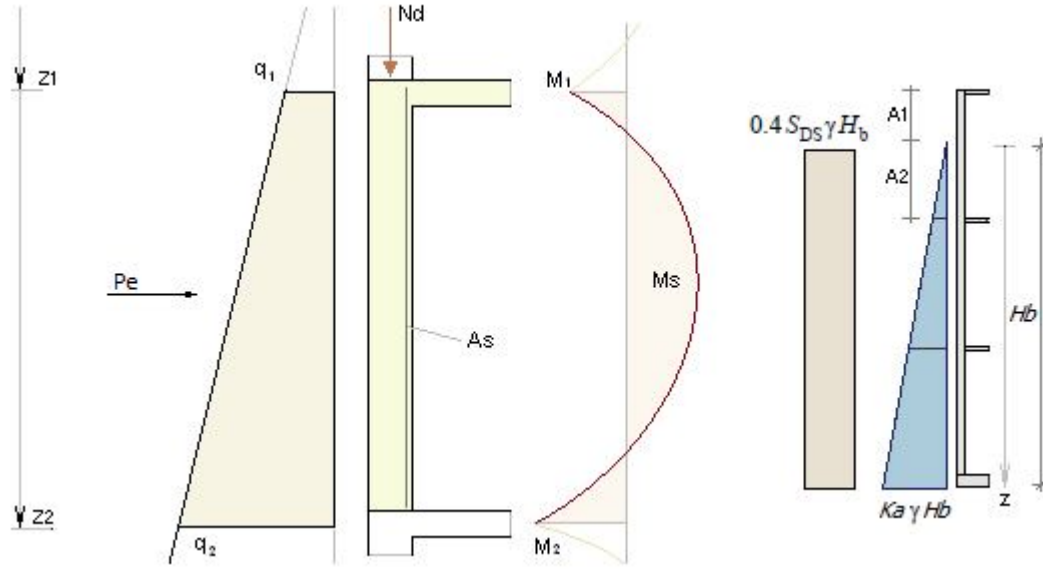
$$g_{sh} = \frac{2 \cdot A_{s_{sws}}}{A_{ch}} \cdot \frac{L_w}{s} \quad V_r = 0.22 A_{ch} f_{cd} > V_d$$

$$V_r = 0.65 f_{ctd} A_c + g_{sh} A_{ch} f_{yd} > V_d$$

PANEL MOMENT ve KESME KAPASİTE KONTROLÜ (tm)

Panel	Kom.	Mp	Mc1	Mc2	Mrp	Mr1	Mr2	ΣMd	ΣMr	Vd	Vr	✓, ×
P106	12	12.07	3.85	-1.10	287.54	777.77	163.01	14.82	1228.32	24.84	177.85	✓
P107	10	7.88	0.89	0.02	236.61	884.23	140.48	8.79	1261.32	18.86	194.49	✓
P108	10	7.34	-0.02	0.12	242.72	884.23	140.48	7.44	1267.43	15.13	194.49	✓
P109	10	16.26	-0.11	0.36	169.42	778.48	123.57	16.51	1071.46	-12.55	177.85	✓
P110	10	-2.62	0.36	-0.94	187.37	123.68	777.77	3.20	1088.81	10.18	177.79	✓
P111	10	-5.75	0.77	-0.78	282.29	101.20	388.71	5.76	772.20	6.33	116.72	✓
P112	11	10.57	3.21	-0.77	289.32	777.77	163.01	13.01	1230.11	24.26	177.85	✓
P113	9	7.88	0.89	-0.10	237.42	140.48	884.23	8.68	1262.13	18.09	194.49	✓
P114	9	7.56	0.10	-0.15	245.87	140.48	884.23	7.51	1270.58	13.80	194.49	✓
P115	9	-15.62	-0.13	-0.21	171.75	778.48	123.57	15.96	1073.80	-11.87	177.85	✓
P116	10	-14.76	0.42	-4.12	604.47	224.88	1166.48	18.46	1995.83	15.83	238.94	✓
P117	12	-111.71	13.31	13.37	2538.50	2688.06	427.06	85.03	5653.62	36.38	477.94	✓
P118	11	-54.13	2.79	5.56	1364.06	365.25	2051.42	45.79	3780.72	37.70	377.92	✓
P119	11	13.56	-1.12	1.07	149.20	635.94	140.59	13.51	925.73	-4.95	155.59	✓
P120	11	-40.69	3.42	9.77	1495.47	325.92	2051.42	27.50	3872.80	-22.69	377.92	✓
P121	11	4.88	-2.01	1.06	388.73	635.94	101.26	3.92	1125.93	-1.55	155.59	✓

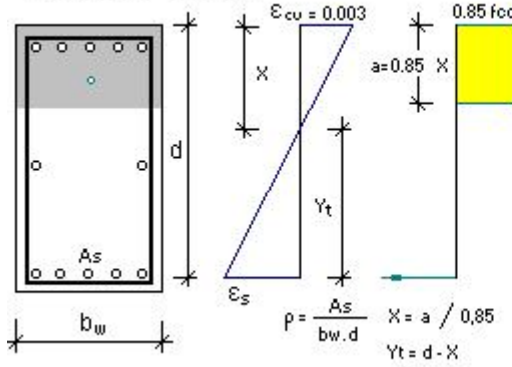
PANELLER ZEMİN YÜKÜ ANALİZİ



ZEMİN YÜKÜ = $Ka \cdot (\gamma \cdot Hb + q)$
 ZEMİN BİRİM HACİM AĞIRLIĞI = 1.8
 ZEMİN İÇSEL SÜRTÜNME ACISI = 30.0
 Kas=0.333 Birimler: (t,m)

Panel	KOMBİN	Z1/Z2	q1	q2	V1	V2	M1	M2	Ms	maxM/As	Donatı
P106 Hb=4.6	1.6 S S + E	0.00 4.60	3.15 4.12	3.15 4.12	9.16 6.82	14.02 11.62	0.00 0.00	11.33 10.90	8.79 5.99	11.33 13.80	ø18/17 (As=14.72 cm ² /m) Zemin yuku
P107 Hb=4.6	1.6 S S + E	0.00 4.60	3.15 4.12	3.15 4.12	9.16 6.82	14.02 11.62	0.00 0.00	11.33 10.90	8.79 5.99	11.33 13.59	ø18/17 (As=15.26 cm ² /m) Zemin yuku
P108 Hb=4.6	1.6 S S + E	0.00 4.60	3.15 4.12	3.15 4.12	9.16 6.82	14.02 11.62	0.00 0.00	11.33 10.90	8.79 5.99	11.33 13.76	ø18/17 (As=15.26 cm ² /m) Zemin yuku
P109 Hb=4.6	1.6 S S + E	0.00 4.60	3.15 4.12	3.15 4.12	9.16 6.82	14.02 11.62	0.00 0.00	11.33 10.90	8.79 5.99	11.33 11.81	ø18/20 (As=12.71 cm ² /m) Zemin yuku
P110 Hb=4.6	1.6 S S + E	0.00 4.60	3.15 4.12	3.15 4.12	9.16 6.82	14.02 11.62	0.00 0.00	11.33 10.90	8.79 5.99	11.33 11.44	ø18/20 (As=12.73 cm ² /m) Zemin yuku
P111 Hb=4.6	1.6 S S + E	0.00 4.60	3.15 4.12	3.15 4.12	-21.02 -20.65	44.20 37.56	0.00 0.00	44.42 42.75	0.00 0.00	44.42 47.34	ø26/10 (As=53.0 cm ² /m) Zemin yuku
P112 Hb=4.6	1.6 S S + E	0.00 4.60	3.15 4.12	3.15 4.12	9.16 6.82	14.02 11.62	0.00 0.00	11.33 10.90	8.79 5.99	11.33 13.81	ø18/17 (As=14.72 cm ² /m) Zemin yuku
P113 Hb=4.6	1.6 S S + E	0.00 4.60	3.15 4.12	3.15 4.12	9.16 6.82	14.02 11.62	0.00 0.00	11.33 10.90	8.79 5.99	11.33 13.59	ø18/17 (As=15.26 cm ² /m) Zemin yuku
P114 Hb=4.6	1.6 S S + E	0.00 4.60	3.15 4.12	3.15 4.12	9.16 6.82	14.02 11.62	0.00 0.00	11.33 10.90	8.79 5.99	11.33 13.89	ø18/17 (As=15.26 cm ² /m) Zemin yuku
P115 Hb=4.6	1.6 S S + E	0.00 4.60	3.15 4.12	3.15 4.12	9.16 6.82	14.02 11.62	0.00 0.00	11.33 10.90	8.79 5.99	11.33 11.32	ø16/17 (As=11.71 cm ² /m) Zemin yuku
P116 Hb=4.6	1.6 S S + E	0.00 4.60	3.15 4.12	3.15 4.12	9.16 6.82	14.02 11.62	0.00 0.00	11.33 10.90	8.79 5.99	11.33 12.78	ø18/19 (As=13.56 cm ² /m) Zemin yuku
P117 Hb=4.6	1.6 S S + E	0.00 4.60	3.15 4.12	3.15 4.12	9.16 6.82	14.02 11.62	0.00 0.00	11.33 10.90	8.79 5.99	11.33 12.99	ø16/15 (As=13.09 cm ² /m) Zemin yuku
P118 Hb=3.4	1.6 S S + E	0.00 3.40	3.00 3.05	3.00 3.05	4.10 2.79	12.22 10.49	0.00 0.00	9.26 9.15	6.86 4.67	9.26 9.75	ø14/16 (As=9.79 cm ² /m) Zemin yuku
P119 Hb=3.4	1.6 S S + E	0.00 3.40	3.00 3.05	3.00 3.05	4.10 2.79	12.22 10.49	0.00 0.00	9.26 9.15	6.86 4.67	9.26 8.84	ø16/21 (As=9.38 cm ² /m) Zemin yuku
P120 Hb=3.4	1.6 S S + E	0.00 4.60	3.15 4.12	3.15 4.12	9.16 6.82	14.02 11.62	0.00 0.00	11.33 10.90	8.79 5.99	11.33 12.73	ø16/15 (As=12.97 cm ² /m) Zemin yuku
P121 Hb=3.4	1.6 S S + E	0.00 4.60	3.15 4.12	3.15 4.12	-21.02 -20.65	44.20 37.56	0.00 0.00	44.42 42.75	0.00 0.00	44.42 46.82	ø26/10 (As=53.07 cm ² /m) Zemin yuku

ANİ SEHİM HESABI



$$\rho_b = \frac{0.85 \cdot 0.85 \cdot f_{cd}}{f_{yd}} \cdot \frac{6000}{6000 + f_{yd}} \quad X = \frac{6000}{6000 + f_{yd}} d$$

$$\rho < \rho_b \quad \text{Çekme kırılması}$$

$$a = \frac{A_s \cdot f_{yd}}{0.85 \cdot f_{cd} \cdot b_w}$$

$$\rho > \rho_b \quad \text{Baskın kırılması}$$

$$(0.85 \cdot f_{cd} \cdot b_w) \cdot a^2 + (6000 \cdot A_s) \cdot a - (6000 \cdot A_s \cdot 0.85 \cdot d) = 0$$

$$a = \frac{6000 \cdot A_s \cdot [\sqrt{1 + f_{cd} \cdot b_w \cdot d / (2076 \cdot A_s)} - 1]}{1.7 \cdot f_{cd} \cdot b_w}$$

Çatlamış kesit atalet momenti

$$M_{cr} = 2.5 \cdot f_{ctd} \cdot I_c / y \quad I_c = b_w \cdot d^3 / 12$$

$$I_{cr} = b_w \cdot X^3 / 3 + E_s / E_c \cdot A_s \cdot (d' - X)^2$$

$$I_{ef} = \left[\frac{M_{cr}}{M_{max}} \right]^3 \cdot I_c + \left[1 - \left(\frac{M_{cr}}{M_{max}} \right)^3 \right] \cdot I_{cr}$$

 δ_i = Ani sehım δ_t = Zamana bağılı sehım

$$\lambda = \frac{2}{1 + 50 \cdot \rho'}$$

$$\delta_t = \delta_i + \delta_{ig} \cdot \lambda$$

KİRİŞ SEHİM ve ÇATLAK KONTROLÜ

(TS500-13.2.4)

Kiriş no	sol T (t)	sağ T (t)	sol M (tm)	sağ M (tm)	M ac. (tm)	Wk mm	fmax mm	Elastik Sehım mm	Ani (δ_i) Sehım mm	$\delta_i + \delta_{ig} \cdot \lambda$ Sehım mm	✓ ✗
K101	5.92	-5.00	4.08	-3.74	2.78	0.23	L/360= 8.33	0.119	0.119	0.291	✓
K102	23.74	-23.75	34.00	-34.03	17.04	0.30	L/360= 22.23	5.771	5.771	13.655	✓
K103	23.50	-23.51	33.66	-33.70	16.87	0.28	L/360= 22.23	6.884	6.884	16.048	✓
K104	23.74	-23.75	34.00	-34.03	17.04	0.30	L/360= 22.23	5.497	5.497	13.007	✓
K105	1.20	-0.54	0.53	0.00	0.31	0.23	L/360= 4.72	0.032	0.032	0.074	✓

w : Kiriş üzerinde kat yüksekliğinde tuğla duvar

KAT BURKULMA HESABI (t) (TS500-7.6)

$\theta = 1.5 \sum (\Delta i \text{ Ndi} / L) / Vfi$ $\theta \leq 0.05$ Kat yanal deplasmanı önlenmiş, $\theta > 0.05$ Kat yanal deplasmanı önlenmemiş
 $\beta s = 1 / (1 - 1.3 * \sum Ng / \sum Nd) \geq 1$ Kat burkulması
 $\sum Nd \leq 0.45 \sum Nkr$ ✓ , $\sum Nd > 0.45 \sum Nkr$ ✗ (Kat kolonları büyütülecektir.)

Kat	$\sum (\Delta i \text{ Ndi} / L)$	Vfi	θ	$\sum Ng$	$\sum Nkr$	βs	$\sum Nd \leq 0.45 \sum Nkr$
1 X	0.064491	129.513	0.000747	677.5	9914929.0	1.0000	✓
1 Y	0.021926	123.151	0.000267	677.5	26639100.0	1.0000	✓

KOLON BURKULMA HESAP SONUÇLARI

X Yönü	Y Yönü
Kat :1 (I/L)b=0.4680333 Hk= 4.600 $\alpha u = 0.001$ Ix=0.00225 $\alpha a = 0$ S101 (I/L)c=0.00048913 Ac=0.3 k($\alpha u, \alpha a$)=0.047 Lkr=0.206 Kat : (I/L)b=0 Cmx=0.454 Rm=Ng/Nd=0.936 yanal deplasman onlenmis EI=0.4 EcIc / (1 + Rm)=1543.066 Nd=12.951 Nkr=π^2 EI/Lkr²=3146.515 $\beta x = Cm / (1 - 1.3 \text{ Nd} / \text{Nkr}) = 0.456$ $\lambda x = Lkr / ix = 2.4 < 100$ ✓ (Lk/i) < 35 / $\sqrt{(Nd / fck \text{ Ac})} >> \beta = \beta x$	Kat :1 (I/L)b=0.1482432 Hk= 4.600 $\alpha u = 0.026$ Iy=0.025 $\alpha a = 0$ S101 (I/L)c=0.00543478 Ac=0.3 k($\alpha u, \alpha a$)=0.058 Lkr=0.256 Kat : (I/L)b=0 Cmy=0.425 Rm=Ng/Nd=0.936 yanal deplasman onlenmis EI=0.4 EcIc / (1 + Rm)=17145.18 Nd=12.951 Nkr=π^2 EI/Lkr²=34074.75 $\beta y = Cm / (1 - 1.3 \text{ Nd} / \text{Nkr}) = 0.425$ $\lambda y = Lkr / iy = 0.9 < 100$ ✓ (Lk/i) < 35 / $\sqrt{(Nd / fck \text{ Ac})} >> \beta = \beta y$
Kat :1 (I/L)b=1.055907 Hk= 4.600 $\alpha u = 0.004$ Ix=0.025 $\alpha a = 0$ S102 (I/L)c=0.00543478 Ac=0.3 k($\alpha u, \alpha a$)=0.143 Lkr=0.629 Kat : (I/L)b=0 Cmx=0.44 Rm=Ng/Nd=0.805 yanal deplasman onlenmis EI=0.4 EcIc / (1 + Rm)=18397.28 Nd=65.031 Nkr=π^2 EI/Lkr²=37505.5 $\beta x = Cm / (1 - 1.3 \text{ Nd} / \text{Nkr}) = 0.441$ $\lambda x = Lkr / ix = 2.2 < 100$ ✓ (Lk/i) < 35 / $\sqrt{(Nd / fck \text{ Ac})} >> \beta = \beta x$	Kat :1 (I/L)b=0.00071949 Hk= 4.600 $\alpha u = 0.476$ Iy=0.00225 $\alpha a = 0$ S102 (I/L)c=0.00048913 Ac=0.3 k($\alpha u, \alpha a$)=0.5 Lkr=2 Kat : (I/L)b=0 Cmy=0.4 Rm=Ng/Nd=0.805 yanal deplasman onlenmis EI=0.4 EcIc / (1 + Rm)=1655.755 Nd=65.031 Nkr=π^2 EI/Lkr²=2972.997 $\beta y = Cm / (1 - 1.3 \text{ Nd} / \text{Nkr}) = 0.412$ $\lambda y = Lkr / iy = 23.1 < 100$ ✓ (Lk/i) < 35 / $\sqrt{(Nd / fck \text{ Ac})} >> \beta = \beta y$
Kat :1 (I/L)b=1.175747 Hk= 4.600 $\alpha u = 0.003$ Ix=0.025 $\alpha a = 0$ S103 (I/L)c=0.00543478 Ac=0.3 k($\alpha u, \alpha a$)=0.143 Lkr=0.629 Kat : (I/L)b=0 Cmx=0.4 Rm=Ng/Nd=0.799 yanal deplasman onlenmis EI=0.4 EcIc / (1 + Rm)=18452.066 Nd=75.877 Nkr=π^2 EI/Lkr²=37618.35 $\beta x = Cm / (1 - 1.3 \text{ Nd} / \text{Nkr}) = 0.401$ $\lambda x = Lkr / ix = 2.2 < 100$ ✓ (Lk/i) < 35 / $\sqrt{(Nd / fck \text{ Ac})} >> \beta = \beta x$	Kat :1 (I/L)b=0.00071949 Hk= 4.600 $\alpha u = 0.476$ Iy=0.00225 $\alpha a = 0$ S103 (I/L)c=0.00048913 Ac=0.3 k($\alpha u, \alpha a$)=0.5 Lkr=2 Kat : (I/L)b=0 Cmy=0.4 Rm=Ng/Nd=0.799 yanal deplasman onlenmis EI=0.4 EcIc / (1 + Rm)=1660.686 Nd=75.877 Nkr=π^2 EI/Lkr²=2981.85 $\beta y = Cm / (1 - 1.3 \text{ Nd} / \text{Nkr}) = 0.414$ $\lambda y = Lkr / iy = 23.1 < 100$ ✓ (Lk/i) < 35 / $\sqrt{(Nd / fck \text{ Ac})} >> \beta = \beta y$
Kat :1 (I/L)b=1.317156 Hk= 4.600 $\alpha u = 0.003$ Ix=0.025 $\alpha a = 0$ S104 (I/L)c=0.00543478 Ac=0.3 k($\alpha u, \alpha a$)=0.156 Lkr=0.687 Kat : (I/L)b=0 Cmx=0.416 Rm=Ng/Nd=0.803 yanal deplasman onlenmis EI=0.4 EcIc / (1 + Rm)=18410.535 Nd=58.628 Nkr=π^2 EI/Lkr²=37534.77 $\beta x = Cm / (1 - 1.3 \text{ Nd} / \text{Nkr}) = 0.417$ $\lambda x = Lkr / ix = 2.4 < 100$ ✓ (Lk/i) < 35 / $\sqrt{(Nd / fck \text{ Ac})} >> \beta = \beta x$	Kat :1 (I/L)b=0.00071949 Hk= 4.600 $\alpha u = 0.476$ Iy=0.00225 $\alpha a = 0$ S104 (I/L)c=0.00048913 Ac=0.3 k($\alpha u, \alpha a$)=0.5 Lkr=2 Kat : (I/L)b=0 Cmy=0.4 Rm=Ng/Nd=0.803 yanal deplasman onlenmis EI=0.4 EcIc / (1 + Rm)=1656.948 Nd=58.628 Nkr=π^2 EI/Lkr²=2975.139 $\beta y = Cm / (1 - 1.3 \text{ Nd} / \text{Nkr}) = 0.411$ $\lambda y = Lkr / iy = 23.1 < 100$ ✓ (Lk/i) < 35 / $\sqrt{(Nd / fck \text{ Ac})} >> \beta = \beta y$
Kat :1 (I/L)b=1.459749 Hk= 4.600 $\alpha u = 0.003$ Ix=0.025 $\alpha a = 0$ S105 (I/L)c=0.00543478 Ac=0.3 k($\alpha u, \alpha a$)=0.156 Lkr=0.688 Kat : (I/L)b=0 Cmx=0.424 Rm=Ng/Nd=1.067 yanal deplasman onlenmis EI=0.4 EcIc / (1 + Rm)=16064.649 Nd=4.1 Nkr=π^2 EI/Lkr²=32752.82 $\beta x = Cm / (1 - 1.3 \text{ Nd} / \text{Nkr}) = 0.424$ $\lambda x = Lkr / ix = 2.4 < 100$ ✓ (Lk/i) < 35 / $\sqrt{(Nd / fck \text{ Ac})} >> \beta = \beta x$	Kat :1 (I/L)b=0.6074438 Hk= 4.600 $\alpha u = 0.001$ Iy=0.00225 $\alpha a = 0$ S105 (I/L)c=0.00048913 Ac=0.3 k($\alpha u, \alpha a$)=0.054 Lkr=0.236 Kat : (I/L)b=0 Cmy=0.404 Rm=Ng/Nd=1.067 yanal deplasman onlenmis EI=0.4 EcIc / (1 + Rm)=1445.818 Nd=4.1 Nkr=π^2 EI/Lkr²=2948.256 $\beta y = Cm / (1 - 1.3 \text{ Nd} / \text{Nkr}) = 0.405$ $\lambda y = Lkr / iy = 2.7 < 100$ ✓ (Lk/i) < 35 / $\sqrt{(Nd / fck \text{ Ac})} >> \beta = \beta y$
Kat :1 (I/L)b=1.793749 Hk= 4.600 $\alpha u = 0.002$ Ix=0.025 $\alpha a = 0$ S106 (I/L)c=0.00543478 Ac=0.3 k($\alpha u, \alpha a$)=0.238 Lkr=1.047 Kat : (I/L)b=0 Cmx=0.432 Rm=Ng/Nd=0.927 yanal deplasman onlenmis EI=0.4 EcIc / (1 + Rm)=17232.726 Nd=8.808 Nkr=π^2 EI/Lkr²=35135.73 $\beta x = Cm / (1 - 1.3 \text{ Nd} / \text{Nkr}) = 0.432$ $\lambda x = Lkr / ix = 3.6 < 100$ ✓ (Lk/i) < 35 / $\sqrt{(Nd / fck \text{ Ac})} >> \beta = \beta x$	Kat :1 (I/L)b=0.00142588 Hk= 4.600 $\alpha u = 0.24$ Iy=0.00225 $\alpha a = 0$ S106 (I/L)c=0.00048913 Ac=0.3 k($\alpha u, \alpha a$)=0.5 Lkr=2 Kat : (I/L)b=0 Cmy=0.405 Rm=Ng/Nd=0.927 yanal deplasman onlenmis EI=0.4 EcIc / (1 + Rm)=1550.945 Nd=8.808 Nkr=π^2 EI/Lkr²=3131.269 $\beta y = Cm / (1 - 1.3 \text{ Nd} / \text{Nkr}) = 0.406$ $\lambda y = Lkr / iy = 23.1 < 100$ ✓ (Lk/i) < 35 / $\sqrt{(Nd / fck \text{ Ac})} >> \beta = \beta y$

X Yönü				Y Yönü			
Kat :1	(I/L)b=1.063283	Hk= 4.600		Kat :1	(I/L)b=1.064613	Hk= 4.600	
$\alpha u=0$	$\downarrow$	Ix=0.00225		$\alpha u=0.004$	$\downarrow$	Iy=0.025	
	S107 (I/L)c=0.00048913	Ac=0.3			S107 (I/L)c=0.00543478	Ac=0.3	
$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.5		$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.179	
Kat :	(I/L)b=0	Lkr=2.3		Kat :	(I/L)b=0	Lkr=0.821	
		Cmx=0.448				Cmy=0.447	
		Rm=Ng/Nd=0.944				Rm=Ng/Nd=0.944	
yanal deplasman onlenmis				yanal deplasman onlenmis			
EI=0.4 EcIc / (1 + Rm)=1537.157 Nd=8.583				EI=0.4 EcIc / (1 + Rm)=17079.522 Nd=8.583			
Nkr= π^2 EI/Lkr ² =2867.927 βx =Cm/ (1-1.3 Nd/Nkr)=0.45				Nkr= π^2 EI/Lkr ² =31857.22 βy =Cm/ (1-1.3 Nd/Nkr)=0.447			
λx =Lkr/ix=26.6<100 ✓ (Lk/i)<35/√(Nd/fck Ac)>> β = βx				λy =Lkr/iy=2.8<100 ✓ (Lk/i)<35/√(Nd/fck Ac)>> β = βy			
Kat :1	(I/L)b=0.00112646	Hk= 4.600		Kat :1	(I/L)b=0.7993737	Hk= 4.600	
$\alpha u=0.304$	$\downarrow$	Ix=0.00225		$\alpha u=0.005$	$\downarrow$	Iy=0.025	
	S108 (I/L)c=0.00048913	Ac=0.3			S108 (I/L)c=0.00543478	Ac=0.3	
$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.5		$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.074	
Kat :	(I/L)b=0	Lkr=2		Kat :	(I/L)b=0	Lkr=0.323	
		Cmx=0.4				Cmy=0.419	
		Rm=Ng/Nd=0.834				Rm=Ng/Nd=0.834	
yanal deplasman onlenmis				yanal deplasman onlenmis			
EI=0.4 EcIc / (1 + Rm)=1629.522 Nd=26.321				EI=0.4 EcIc / (1 + Rm)=18105.802 Nd=26.321			
Nkr= π^2 EI/Lkr ² =3167.164 βx =Cm/ (1-1.3 Nd/Nkr)=0.404				Nkr= π^2 EI/Lkr ² =36746.91 βy =Cm/ (1-1.3 Nd/Nkr)=0.419			
λx =Lkr/ix=23.1<100 ✓ (Lk/i)<35/√(Nd/fck Ac)>> β = βx				λy =Lkr/iy=1.1<100 ✓ (Lk/i)<35/√(Nd/fck Ac)>> β = βy			
Kat :1	(I/L)b=0.00100009	Hk= 4.600		Kat :1	(I/L)b=1.261502	Hk= 4.600	
$\alpha u=0.342$	$\downarrow$	Ix=0.00225		$\alpha u=0.003$	$\downarrow$	Iy=0.025	
	S109 (I/L)c=0.00048913	Ac=0.3			S109 (I/L)c=0.00543478	Ac=0.3	
$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.5		$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.074	
Kat :	(I/L)b=0	Lkr=2		Kat :	(I/L)b=0	Lkr=0.323	
		Cmx=0.4				Cmy=0.438	
		Rm=Ng/Nd=0.861				Rm=Ng/Nd=0.861	
yanal deplasman onlenmis				yanal deplasman onlenmis			
EI=0.4 EcIc / (1 + Rm)=1606.007 Nd=19.736				EI=0.4 EcIc / (1 + Rm)=17844.518 Nd=19.736			
Nkr= π^2 EI/Lkr ² =3058.574 βx =Cm/ (1-1.3 Nd/Nkr)=0.403				Nkr= π^2 EI/Lkr ² =36380.4 βy =Cm/ (1-1.3 Nd/Nkr)=0.438			
λx =Lkr/ix=23.1<100 ✓ (Lk/i)<35/√(Nd/fck Ac)>> β = βx				λy =Lkr/iy=1.1<100 ✓ (Lk/i)<35/√(Nd/fck Ac)>> β = βy			
Kat :1	(I/L)b=0.4680333	Hk= 4.600		Kat :1	(I/L)b=0.1482432	Hk= 4.600	
$\alpha u=0.001$	$\downarrow$	Ix=0.00225		$\alpha u=0.026$	$\downarrow$	Iy=0.025	
	S110 (I/L)c=0.00048913	Ac=0.3			S110 (I/L)c=0.00543478	Ac=0.3	
$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.047		$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.506	
Kat :	(I/L)b=0	Lkr=0.206		Kat :	(I/L)b=0	Lkr=2.229	
		Cmx=0.449				Cmy=0.409	
		Rm=Ng/Nd=0.937				Rm=Ng/Nd=0.937	
yanal deplasman onlenmis				yanal deplasman onlenmis			
EI=0.4 EcIc / (1 + Rm)=1542.479 Nd=12.846				EI=0.4 EcIc / (1 + Rm)=17138.652 Nd=12.846			
Nkr= π^2 EI/Lkr ² =3145.317 βx =Cm/ (1-1.3 Nd/Nkr)=0.451				Nkr= π^2 EI/Lkr ² =34061.77 βy =Cm/ (1-1.3 Nd/Nkr)=0.409			
λx =Lkr/ix=2.4<100 ✓ (Lk/i)<35/√(Nd/fck Ac)>> β = βx				λy =Lkr/iy=7.7<100 ✓ (Lk/i)<35/√(Nd/fck Ac)>> β = βy			
Kat :1	(I/L)b=1.055907	Hk= 4.600		Kat :1	(I/L)b=0.00071949	Hk= 4.600	
$\alpha u=0.004$	$\downarrow$	Ix=0.025		$\alpha u=0.476$	$\downarrow$	Iy=0.00225	
	S111 (I/L)c=0.00543478	Ac=0.3			S111 (I/L)c=0.00048913	Ac=0.3	
$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.143		$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.5	
Kat :	(I/L)b=0	Lkr=0.629		Kat :	(I/L)b=0	Lkr=2	
		Cmx=0.438				Cmy=0.4	
		Rm=Ng/Nd=0.804				Rm=Ng/Nd=0.804	
yanal deplasman onlenmis				yanal deplasman onlenmis			
EI=0.4 EcIc / (1 + Rm)=18398.883 Nd=64.653				EI=0.4 EcIc / (1 + Rm)=1655.899 Nd=64.653			
Nkr= π^2 EI/Lkr ² =37508.77 βx =Cm/ (1-1.3 Nd/Nkr)=0.439				Nkr= π^2 EI/Lkr ² =2973.256 βy =Cm/ (1-1.3 Nd/Nkr)=0.412			
λx =Lkr/ix=2.2<100 ✓ (Lk/i)<35/√(Nd/fck Ac)>> β = βx				λy =Lkr/iy=23.1<100 ✓ (Lk/i)<35/√(Nd/fck Ac)>> β = βy			
Kat :1	(I/L)b=1.175747	Hk= 4.600		Kat :1	(I/L)b=0.00071949	Hk= 4.600	
$\alpha u=0.003$	$\downarrow$	Ix=0.025		$\alpha u=0.476$	$\downarrow$	Iy=0.00225	
	S112 (I/L)c=0.00543478	Ac=0.3			S112 (I/L)c=0.00048913	Ac=0.3	
$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.143		$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.5	
Kat :	(I/L)b=0	Lkr=0.629		Kat :	(I/L)b=0	Lkr=2	
		Cmx=0.437				Cmy=0.4	
		Rm=Ng/Nd=0.799				Rm=Ng/Nd=0.799	
yanal deplasman onlenmis				yanal deplasman onlenmis			
EI=0.4 EcIc / (1 + Rm)=18451.217 Nd=75.708				EI=0.4 EcIc / (1 + Rm)=1660.609 Nd=75.708			
Nkr= π^2 EI/Lkr ² =37616.62 βx =Cm/ (1-1.3 Nd/Nkr)=0.438				Nkr= π^2 EI/Lkr ² =2981.713 βy =Cm/ (1-1.3 Nd/Nkr)=0.414			
λx =Lkr/ix=2.2<100 ✓ (Lk/i)<35/√(Nd/fck Ac)>> β = βx				λy =Lkr/iy=23.1<100 ✓ (Lk/i)<35/√(Nd/fck Ac)>> β = βy			
Kat :1	(I/L)b=1.317156	Hk= 4.600		Kat :1	(I/L)b=0.00071949	Hk= 4.600	
$\alpha u=0.003$	$\downarrow$	Ix=0.025		$\alpha u=0.476$	$\downarrow$	Iy=0.00225	
	S113 (I/L)c=0.00543478	Ac=0.3			S113 (I/L)c=0.00048913	Ac=0.3	
$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.156		$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.5	
Kat :	(I/L)b=0	Lkr=0.687		Kat :	(I/L)b=0	Lkr=2	
		Cmx=0.43				Cmy=0.4	
		Rm=Ng/Nd=0.805				Rm=Ng/Nd=0.805	
yanal deplasman onlenmis				yanal deplasman onlenmis			
EI=0.4 EcIc / (1 + Rm)=18393.356 Nd=60.353				EI=0.4 EcIc / (1 + Rm)=1655.402 Nd=60.353			
Nkr= π^2 EI/Lkr ² =37499.74 βx =Cm/ (1-1.3 Nd/Nkr)=0.431				Nkr= π^2 EI/Lkr ² =2972.363 βy =Cm/ (1-1.3 Nd/Nkr)=0.411			
λx =Lkr/ix=2.4<100 ✓ (Lk/i)<35/√(Nd/fck Ac)>> β = βx				λy =Lkr/iy=23.1<100 ✓ (Lk/i)<35/√(Nd/fck Ac)>> β = βy			

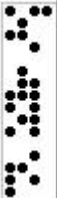
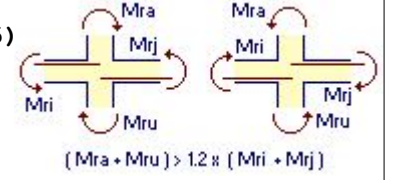
X Yönü			Y Yönü		
Kat :1	(I/L)b=1.033005	Hk= 4.600	Kat :1	(I/L)b=0.1919299	Hk= 4.600
$\alpha u=0.004$	$\downarrow$	Ix=0.025	$\alpha u=0.002$	$\downarrow$	Iy=0.00225
S114	(I/L)c=0.00543478	Ac=0.3	S114	(I/L)c=0.00048913	Ac=0.3
$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.116	$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.5
Kat :	(I/L)b=0	Lkr=0.512	Kat :	(I/L)b=0	Lkr=2.2
		Cmx=0.436			Cmy=0.4
		Rm=Ng/Nd=0.935			Rm=Ng/Nd=0.935
yanal deplasman onlenmis			yanal deplasman onlenmis		
EI=0.4 EcIc / (1 + Rm)=17155.973 Nd=10.378			EI=0.4 EcIc / (1 + Rm)=1544.037 Nd=10.378		
Nkr= π^2 EI/Lkr ² =34974.69 $\beta x=Cm/(1-1.3 Nd/Nkr)=0.437$			Nkr= π^2 EI/Lkr ² =3148.22 $\beta y=Cm/(1-1.3 Nd/Nkr)=0.402$		
$\lambda x=Lkr/ix=1.8<100 \checkmark (Lk/i)<35/\sqrt{(Nd/fck Ac)}>>\beta=\beta x$			$\lambda y=Lkr/iy=25.4<100 \checkmark (Lk/i)<35/\sqrt{(Nd/fck Ac)}>>\beta=\beta y$		
Kat :1	(I/L)b=0.3037218	Hk= 4.600	Kat :1	(I/L)b=0.1968887	Hk= 4.600
$\alpha u=0.001$	$\downarrow$	Ix=0.00225	$\alpha u=0.019$	$\downarrow$	Iy=0.025
S115	(I/L)c=0.00048913	Ac=0.3	S115	(I/L)c=0.00543478	Ac=0.3
$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.5	$\alpha a=0$	$\downarrow$	k($\alpha u, \alpha a$)=0.505
Kat :	(I/L)b=0	Lkr=2.2	Kat :	(I/L)b=0	Lkr=2.221
		Cmx=0.991			Cmy=0.4
		Rm=Ng/Nd=0.893			Rm=Ng/Nd=0.893
yanal deplasman onlenmis			yanal deplasman onlenmis		
EI=0.4 EcIc / (1 + Rm)=1578.296 Nd=18.708			EI=0.4 EcIc / (1 + Rm)=17536.623 Nd=18.708		
Nkr= π^2 EI/Lkr ² =3218.248 $\beta x=Cm/(1-1.3 Nd/Nkr)=0.999$			Nkr= π^2 EI/Lkr ² =35075.39 $\beta y=Cm/(1-1.3 Nd/Nkr)=0.4$		
$\lambda x=Lkr/ix=25.4<100 \checkmark (Lk/i)<35/\sqrt{(Nd/fck Ac)}>>\beta=\beta x$			$\lambda y=Lkr/iy=7.7<100 \checkmark (Lk/i)<35/\sqrt{(Nd/fck Ac)}>>\beta=\beta y$		

GÜÇLÜ KOLONLARIN, KAT KESME GÜVENLİĞİ (t)

(TBDY2018-7.3.5)

Kat	Dyf	Vsx	Vkx	α_x	Vsy	Vky	α_y
1	1	129.47	129.47	1.00	93.13	93.13	1.00

$V_s/V_k > .70$ KOŞULU SAĞLANMAKTADIR. GÜÇLÜ KOLONLAR, $(1/\alpha)$ ile ÇARPILMIŞTIR.
Tek katlı binalarda ve çok katlı binaların en üst katında bu kontrol yapılmaz

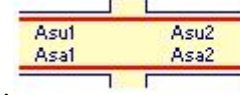


KOLON-KİRİŞ BİRLEŞİM KESME GÜVENLİK KONTROLU

TBDY 2018-7.5'e göre yapılmıştır.

 $V_e = 1.25 f_{yk} (A_{s1} + A_{s2}) - V_{kol} < V_{max} = (1.7 \div 1.0) b_j h_c \sqrt{f_{ck}}$

Konsol kirişler, Kolon-kiriş birleşim kontrolunda dikkate alınmamıştır.

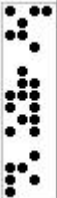
 $B_j \text{ genişlik opsiyonu : } b_j = \min(B_{w1}, B_{w2}, B_c, (B_{w1} + 2.X_1), (B_{w2} + 2.X_2))$  $A_{st} > A_{s1} + A_{s2}$

Bodrum katlar; sınırlı sünek kat olup, kolon-kiriş birleşim kesme kontrolu yeterliliği aranmaz.

Perdelerde kolon-kiriş birleşim kontrolu yapılmaz. Sadece kolonlarda yapılır.

Kolon-kiriş birleşim kesme kontrolu yapılacak kolon bulunmamıştır.

Kolon	Bx/By	bw1	bw2	b _j	Asu1	Asa1	Asu2	Asa2	A _{st}	V _{kol}	V _e	V _{max}	AÇIKLAMA



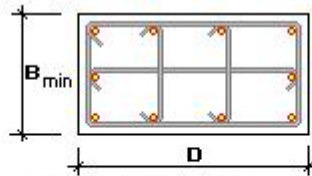
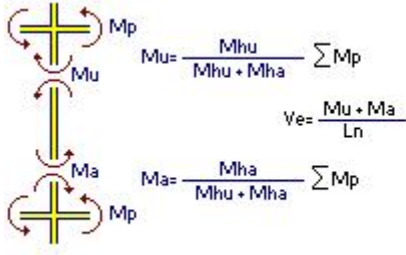
KOLONLARIN KESME DAYANIM KONTROLU

$$V_w = (A_{sw}/s) \cdot f_{ywd} \cdot d, \quad V_{cr} = 0.65 \cdot f_{ctd} \cdot A_c, \quad V_r = 0.8 \cdot V_{cr} + V_w, \quad 0.85 \cdot A_c \cdot v_{fck} \geq V_d \quad (t, cm^2) \quad TBDY2018-7.3.7$$

$$V_{fr} = (f_{ctd} \cdot A_c + \mu \cdot A_s \cdot f_{yd}) = \quad \text{İş Derzi Sürtünme Kesme Dayanımı} \quad TBDY2018-7.6.7.1$$

$$\mu = 1 \quad (\text{pürüzlendirilmiş yüzey} \geq 5mm) \quad f_{ctd} = 13.79 (kg/cm^2)$$

Kolon		Ac	As	A _{sw} /s	V _w	V _{cr}	V _d	V _r =0.8 V _{cr} + V _w	V _{fr}
S101	x	3000	15.40	0.4906	53.755	26.899	0.182	80.654 ✓	56.231 ✓
S101	y	3000	15.40	0.1963	71.674	26.899	1.358	98.573 ✓	56.231 ✓
S102	x	3000	15.40	0.1963	71.674	26.899	1.697	98.573 ✓	56.231 ✓
S102	y	3000	15.40	0.4906	53.755	26.899	3.079	80.654 ✓	56.231 ✓
S103	x	3000	15.40	0.1963	71.674	26.899	1.514	98.573 ✓	56.231 ✓
S103	y	3000	15.40	0.4906	53.755	26.899	3.547	80.654 ✓	56.231 ✓
S104	x	3000	15.40	0.1963	71.674	26.899	1.557	98.573 ✓	56.231 ✓
S104	y	3000	15.40	0.4906	53.755	26.899	2.952	80.654 ✓	56.231 ✓
S105	x	3000	15.40	0.1963	71.674	26.899	1.458	98.573 ✓	56.231 ✓
S105	y	3000	15.40	0.4906	53.755	26.899	1.175	80.654 ✓	56.231 ✓
S106	x	3000	15.40	0.1963	71.674	26.899	1.330	98.573 ✓	56.231 ✓
S106	y	3000	15.40	0.4906	53.755	26.899	1.196	80.654 ✓	56.231 ✓
S107	x	3000	15.40	0.4906	53.755	26.899	0.136	80.654 ✓	56.231 ✓
S107	y	3000	15.40	0.1963	71.674	26.899	0.789	98.573 ✓	56.231 ✓
S108	x	3000	15.40	0.4906	53.755	26.899	0.280	80.654 ✓	56.231 ✓
S108	y	3000	15.40	0.1963	71.674	26.899	1.457	98.573 ✓	56.231 ✓
S109	x	3000	15.40	0.4906	53.755	26.899	0.551	80.654 ✓	56.231 ✓
S109	y	3000	15.40	0.1963	71.674	26.899	0.782	98.573 ✓	56.231 ✓
S110	x	3000	15.40	0.4906	53.755	26.899	0.179	80.654 ✓	56.231 ✓
S110	y	3000	15.40	0.1963	71.674	26.899	1.371	98.573 ✓	56.231 ✓
S111	x	3000	15.40	0.1963	71.674	26.899	1.659	98.573 ✓	56.231 ✓
S111	y	3000	15.40	0.4906	53.755	26.899	3.050	80.654 ✓	56.231 ✓
S112	x	3000	15.40	0.1963	71.674	26.899	1.463	98.573 ✓	56.231 ✓
S112	y	3000	15.40	0.4906	53.755	26.899	3.510	80.654 ✓	56.231 ✓
S113	x	3000	15.40	0.1963	71.674	26.899	1.537	98.573 ✓	56.231 ✓
S113	y	3000	15.40	0.4906	53.755	26.899	2.909	80.654 ✓	56.231 ✓
S114	x	3000	15.40	0.1963	71.674	26.899	1.462	98.573 ✓	56.231 ✓
S114	y	3000	15.40	0.4906	53.755	26.899	1.121	80.654 ✓	56.231 ✓
S115	x	3000	15.40	0.4906	53.755	26.899	0.114	80.654 ✓	56.231 ✓
S115	y	3000	15.40	0.1963	71.674	26.899	0.712	98.573 ✓	56.231 ✓



Ln : Kolon kirişler arası serbest yüksekliği

Hk : Kolon kat yüksekliği

Fk : Kolon boyunca etriye alan toplamı

Letr : hesap doğrultusundaki etriye boylarının toplamı

$$\rho = \frac{F_k \cdot L_{etr}}{A_c \cdot H_k} \geq 0,0025$$

$$V_r = 0,65 \cdot A_c \cdot f_{ctd} + \rho \cdot A_c \cdot f_{yd} > V_e$$

$$\text{Dikdörtgen kolonlarda } L_{etr} \cong D \quad A_c = B \cdot D$$

$$\rho = \frac{F_k \cdot D}{B \cdot D \cdot H_k} = \frac{F_k}{B \cdot H_k}$$

$$V_r = 0,65 \cdot B \cdot D \cdot f_{ctd} + F_k \cdot D \cdot f_{yd} / H_k > V_e$$

$$V_e > V_d(G+Q+D.E, B_{ax}+0.3 \times B_{ay}) \Rightarrow V_e = V_d(G+Q+D.E, B_{ax}+0.3 \times B_{ay})$$

Bodrum katlar; sınırlı sünek kat olup, kesme güvenlik yeterliliği aranmaz.

10cm'den geniş tuğla duvarlar, kesme güvenliğinde dikkate alınmıştır.

TBDY2018-7.3.7

KOLONLARIN KESME GÜVENLİK KONTROLÜ

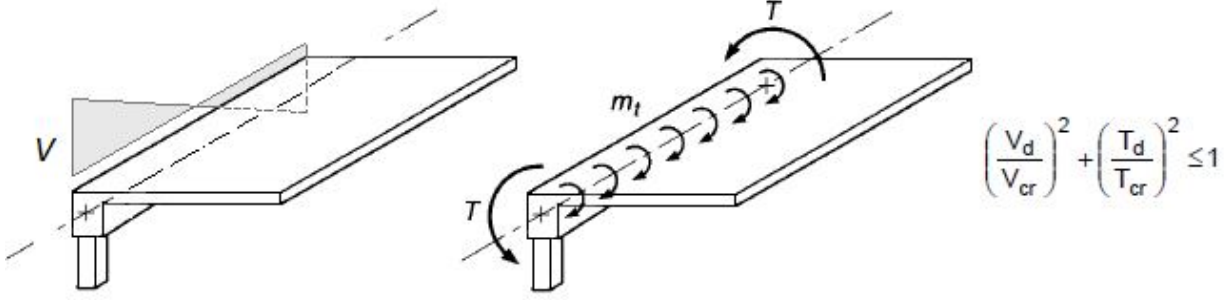
Kolon	+X			-X			+Y			-Y		
	Mp	Mc	Mr	Mp	Mc	Mr	Mp	Mc	Mr	Mp	Mc	Mr

Kısa kolon bulunmamıştır.

Kısa kolonlar; kolon kenarındaki dolgu duvarlarında pencere boşluğu nedeni ile oluşabilirler.

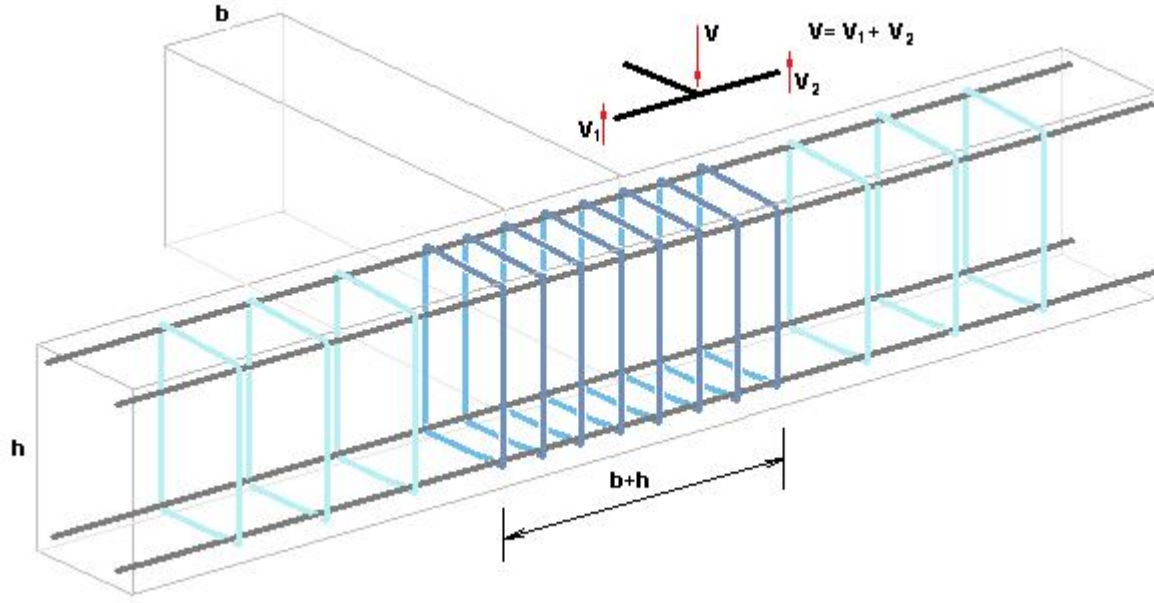
Kısa kolon olması durumunda, kesme güvenlik hesabı kısa kolon yüksekliğine göre yapılmaktadır.

$V_{cr}=0.65 \cdot f_{ctd} \cdot b_w \cdot d$, $V_c=0.80 \cdot V_{cr}$, $V_w=A_{sw}/s \cdot f_{ywd} \cdot d$, $V_r=V_c+V_w > V_d$, $f_{ctd}=13.79 \text{ (kg/cm}^2\text{)}$
 $T_{cr} = 1.35 \cdot f_{ctd} \cdot S_x$, $T_r=(V_d/V_{cr})^2 + (T_d/T_{cr})^2 \leq 1$ (Eğik çatlama sınırı), $n \cdot A_{sw}/s \geq 0.3 \cdot f_{ctd}/f_{ywd} \cdot b_w$
 $A_{ov}/s = (V_d - V_c)/(2 \cdot d \cdot f_{ywd})$, $A_{ot}/s = T_d/(2 \cdot A_e \cdot f_{ywd})$, $A_o/s = A_{ov}/s + A_{ot}/s \leq A_{sw}/s$, $A_{sl} = A_{ot}/s$ Ue f_{ywd}/f_{yd}
 $V_d: V(\min\{a+D, a+L_n/3\})$

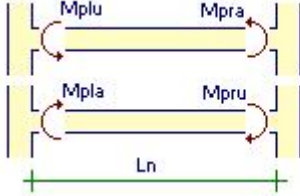


KİRİŞLERİN KESME ve BURULMA KONTROLÜ (tm) (TS500-8.2)

Kiriş	Vcr	Vw	Vr	Vd	Td	Tcr	Tr	Aov/s + Aot/s = Ao/s			Asw/s	✓, ✗
K101	19.73	31.56	47.34	5.02	0.7031	6.7636	0.0756	0.0000	0.0098	0.0098	0.1571	✓
K102	29.59	63.12	86.79	24.17	5.4903	15.7922	0.7884	0.0006	0.0301	0.0307	0.3142	✓
K103	29.59	63.12	86.79	26.64	0.2915	15.7922	0.8108	0.0037	0.0016	0.0053	0.3142	✓
K104	29.59	63.12	86.79	23.95	5.9315	15.7922	0.7965	0.0003	0.0328	0.0330	0.3142	✓
K105	14.79	31.56	43.39	1.18	0.0045	3.5310	0.0063	0.0000	0.0020	0.0020	0.1571	✓


KİRİŞ ASKI DONATISI KESME KONTROLÜ (tm) (TS500-8.1.2)

Kiriş	Tali Kiriş	Askı Donatısı	Asw	Bw/H	Vc	Vw	Vr	Vd	✓, ✗
K101	K105	Ø10/9	1.57	40/60	15.78	35.06	50.85	0.06	✓



$$V_e = \frac{M_{plu} + M_{pra}}{L_n}$$

$$V_e = \frac{M_{pla} + M_{pru}}{L_n}$$

$$V_e > V_d(G+Q+D.E, Bax+0.3 \times Bay) \Rightarrow V_e = V_d(G+Q+D.E, Bax+0.3 \times Bay) *$$

$$V_w = (A_{sw}/s) \cdot f_{ywd} \cdot d, \quad V_{cr} = 0.65 \cdot f_{ctd} \cdot A_c, \quad V_r = 0.8 \cdot V_{cr} + V_w, \quad 0.85 \cdot A_c \cdot \sqrt{f_{ck}} \geq V_d \quad \text{TBDY2018-7.4.5.2}$$

KİRİŞLERİN KESME GÜVENLİK KONTROLU (tm) TBDY2018-7.4.5

Kiriş	L_n	M_{plu}	M_{pla}	M_{pru}	M_{pra}	$V_{dl} + V_{pl} = V_{el} < V_{rl}$	$V_{dr} + V_{pr} = V_{er} < V_{rr}$	✓, ✗

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S101	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	8.66	0.51	(azaltma	Nq=	0.51×1.000	=	0.51)	-1.59
Alt Mx	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.14
Alt My	-0.45	-0.11	-0.02	-0.08	-0.10	-0.04	-0.08	0.28
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-2.61	2.82	-2.93	3.50	-0.07	-0.12	-0.12	
Alt Mx	0.22	-0.25	0.00	0.01	0.01	0.00	0.00	
Alt My	-0.01	0.12	1.84	-2.33	0.00	0.08	0.08	
S102	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	37.38	7.94	(azaltma	Nq=	7.94×1.000	=	7.94)	-1.67
Alt Mx	0.17	0.04	0.01	0.03	0.02	0.02	0.03	1.17
Alt My	-2.89	-0.70	-0.33	-0.37	-0.59	-0.46	-0.35	0.26
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-0.66	0.71	-0.57	0.76	-0.02	-0.02	-0.02	
Alt Mx	2.16	-2.47	0.05	0.06	0.06	0.00	0.00	
Alt My	-0.01	0.02	0.33	-0.39	0.00	0.01	0.01	
S103	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	43.32	9.52	(azaltma	Nq=	9.52×1.000	=	9.52)	-1.23
Alt Mx	-0.03	0.00	0.01	-0.01	0.00	0.00	0.00	0.95
Alt My	-3.56	-0.85	-0.35	-0.51	-0.51	-0.77	-0.43	0.29
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.02	-0.02	0.21	-0.23	0.00	0.01	0.01	
Alt Mx	2.22	-2.52	0.02	0.10	0.07	0.00	0.00	
Alt My	0.00	0.01	0.39	-0.43	0.00	0.02	0.02	
S104	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	33.64	7.21	(azaltma	Nq=	7.21×1.000	=	7.21)	-0.93
Alt Mx	-0.16	-0.03	0.00	-0.03	-0.03	-0.02	-0.01	0.76
Alt My	-2.64	-0.63	-0.10	-0.54	-0.34	-0.61	-0.32	0.24
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.10	-0.10	-0.24	0.16	0.00	-0.01	-0.01	
Alt Mx	2.24	-2.54	-0.05	0.17	0.07	0.00	0.00	
Alt My	0.00	0.00	0.37	-0.37	0.00	0.01	0.01	
S105	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	3.12	-0.17	(azaltma	Nq=	-0.17×1.000	=	-0.17)	0.30
Alt Mx	-0.13	-0.02	0.00	-0.02	-0.02	-0.02	-0.01	0.59
Alt My	-0.07	-0.02	-0.01	-0.01	-0.01	-0.02	-0.01	0.06
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.31	-0.33	-1.24	1.12	0.01	-0.05	-0.05	
Alt Mx	2.23	-2.52	-0.09	0.22	0.07	0.00	0.00	
Alt My	0.00	-0.01	0.27	-0.25	0.00	0.01	0.01	
S106	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	5.83	0.40	(azaltma	Nq=	0.40×1.000	=	0.40)	-0.32
Alt Mx	-0.07	-0.01	0.00	-0.01	-0.01	0.00	-0.01	0.48
Alt My	-0.09	-0.02	-0.02	0.00	0.00	-0.02	-0.02	0.13
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.80	-0.86	-1.72	1.53	0.03	-0.08	-0.08	
Alt Mx	2.19	-2.48	-0.14	0.26	0.07	-0.01	-0.01	
Alt My	-0.01	0.00	0.20	-0.17	0.00	0.01	0.01	
S107	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	5.79	0.30	(azaltma	Nq=	0.30×1.000	=	0.30)	0.57
Alt Mx	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.06
Alt My	-0.11	-0.02	-0.02	0.00	0.00	-0.02	-0.02	0.27
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	1.34	-1.43	-2.24	1.94	0.04	-0.10	-0.10	
Alt Mx	0.22	-0.25	0.00	0.01	0.01	0.00	0.00	
Alt My	0.02	-0.13	1.64	-1.27	0.00	0.08	0.08	
S108	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	15.67	2.74	(azaltma	Nq=	2.74×1.000	=	2.74)	0.58
Alt Mx	0.03	0.01	-0.07	0.08	0.06	0.01	-0.05	0.12
Alt My	-0.47	-0.11	-0.05	-0.06	-0.05	-0.11	-0.06	0.38
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.29	-0.32	-0.86	0.77	0.00	-0.04	-0.04	
Alt Mx	0.31	-0.33	0.00	0.01	0.01	0.00	0.00	
Alt My	0.01	-0.04	2.45	-2.25	0.00	0.10	0.10	
S109	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	12.13	1.72	(azaltma	Nq=	1.72×1.000	=	1.72)	-1.42
Alt Mx	0.28	0.07	0.08	-0.01	0.07	0.08	0.08	-0.24
Alt My	-0.11	-0.02	-0.03	0.00	0.00	-0.02	-0.03	0.13
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.48	-0.48	-1.18	0.97	0.02	-0.05	-0.05	
Alt Mx	0.29	-0.31	0.00	0.01	0.01	0.00	0.00	
Alt My	0.03	-0.13	1.60	-1.24	0.00	0.07	0.07	

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S110	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	8.60	0.50	(azaltma)	Nq=	0.50×1.000	=	0.50)	-1.55
Alt Mx	0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.13
Alt My	0.48	0.11	0.03	0.08	0.10	0.04	0.08	-0.29
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-2.76	2.59	2.92	-3.52	-0.07	0.12	0.12	
Alt Mx	0.24	-0.22	0.00	-0.01	0.01	0.00	0.00	
Alt My	0.08	0.04	1.84	-2.33	0.00	0.08	0.08	
S111	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	37.15	7.90	(azaltma)	Nq=	7.90×1.000	=	7.90)	-1.64
Alt Mx	0.19	0.04	0.01	0.03	0.03	0.03	0.03	1.13
Alt My	2.89	0.70	0.33	0.37	0.59	0.46	0.35	-0.26
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-0.72	0.67	0.53	-0.73	-0.02	0.02	0.02	
Alt Mx	2.39	-2.11	-0.06	-0.04	0.05	0.00	0.00	
Alt My	0.01	0.00	0.33	-0.39	0.00	0.01	0.01	
S112	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	43.23	9.49	(azaltma)	Nq=	9.49×1.000	=	9.49)	-1.19
Alt Mx	-0.02	0.00	0.01	-0.01	0.00	0.00	0.00	0.90
Alt My	3.56	0.85	0.35	0.51	0.51	0.77	0.43	-0.29
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-0.08	0.07	-0.24	0.26	0.00	-0.01	-0.01	
Alt Mx	2.44	-2.16	-0.03	-0.07	0.06	0.00	0.00	
Alt My	0.00	0.00	0.39	-0.43	0.00	0.02	0.02	
S113	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	34.70	7.36	(azaltma)	Nq=	7.36×1.000	=	7.36)	-0.91
Alt Mx	-0.21	-0.04	-0.01	-0.03	-0.03	-0.03	-0.02	0.70
Alt My	2.64	0.63	0.10	0.54	0.34	0.61	0.32	-0.24
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-0.12	0.10	0.40	-0.29	0.00	0.01	0.01	
Alt Mx	2.44	-2.16	0.03	-0.14	0.06	0.00	0.00	
Alt My	0.00	0.00	0.37	-0.37	0.00	0.01	0.01	
S114	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	6.93	0.42	(azaltma)	Nq=	0.42×1.000	=	0.42)	0.12
Alt Mx	-0.22	-0.04	-0.02	-0.02	-0.02	-0.03	-0.03	0.57
Alt My	0.08	0.02	0.01	0.01	0.01	0.02	0.01	-0.05
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.19	-0.21	1.92	-1.70	0.01	0.08	0.08	
Alt Mx	2.37	-2.10	0.04	-0.15	0.05	0.00	0.00	
Alt My	-0.01	0.01	0.26	-0.24	0.00	0.01	0.01	
S115	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	11.94	1.25	(azaltma)	Nq=	1.25×1.000	=	1.25)	-0.04
Alt Mx	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.02
Alt My	0.12	0.03	0.03	-0.01	-0.01	0.03	0.03	-0.27
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	2.65	-2.50	3.37	-2.94	0.06	0.14	0.14	
Alt Mx	0.24	-0.22	0.01	-0.02	0.01	0.00	0.00	
Alt My	-0.04	-0.06	1.54	-1.19	0.00	0.07	0.07	
P106-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	0.93	-0.57	(azaltma)	Nq=	-0.57×1.000	=	-0.57)	-2.93
Alt Mx	-0.86	-0.25	-0.07	-0.18	-0.18	-0.16	-0.15	0.14
Alt My	-0.75	-0.18	-0.08	-0.10	-0.15	-0.12	-0.09	0.08
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-6.66	7.29	-4.49	5.28	-0.19	-0.19	-0.19	
Alt Mx	-0.72	1.00	2.77	-3.54	-0.03	0.11	0.11	
Alt My	0.00	0.01	0.17	-0.21	0.00	0.01	0.01	
P106-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	0.93	-0.57	(azaltma)	Nq=	-0.57×1.000	=	-0.57)	-2.93
Alt Mx	-0.86	-0.25	-0.07	-0.18	-0.18	-0.16	-0.15	0.14
Alt My	-0.75	-0.18	-0.08	-0.10	-0.15	-0.12	-0.09	0.08
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-6.66	7.29	-4.49	5.28	-0.19	-0.19	-0.19	
Alt Mx	-0.72	1.00	2.77	-3.54	-0.03	0.11	0.11	
Alt My	0.00	0.01	0.17	-0.21	0.00	0.01	0.01	
P107-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	-2.13	-1.15	(azaltma)	Nq=	-1.15×1.000	=	-1.15)	-2.83
Alt Mx	0.24	0.07	0.03	0.04	0.05	0.06	0.03	1.51
Alt My	-1.48	-0.36	-0.15	-0.20	-0.25	-0.28	-0.18	0.14
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-8.44	9.60	-0.14	-0.31	-0.26	-0.01	-0.01	
Alt Mx	2.50	-2.86	0.22	-0.11	0.07	0.01	0.01	
Alt My	0.00	0.01	0.17	-0.19	0.00	0.01	0.01	

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P107-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	-2.13	-1.15	(azaltma)	Nq=	-1.15×1.000	=	-1.15)	-2.83
Alt Mx	0.24	0.07	0.03	0.04	0.05	0.06	0.03	1.51
Alt My	-1.48	-0.36	-0.15	-0.20	-0.25	-0.28	-0.18	0.14
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-8.44	9.60	-0.14	-0.31	-0.26	-0.01	-0.01	
Alt Mx	2.50	-2.86	0.22	-0.11	0.07	0.01	0.01	
Alt My	0.00	0.01	0.17	-0.19	0.00	0.01	0.01	
P108-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	-1.34	-0.88	(azaltma)	Nq=	-0.88×1.000	=	-0.88)	-1.88
Alt Mx	0.31	0.11	0.05	0.06	0.07	0.10	0.05	1.21
Alt My	-1.33	-0.32	-0.09	-0.22	-0.18	-0.30	-0.16	0.13
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-7.65	8.71	0.19	-0.68	-0.25	0.00	0.00	
Alt Mx	2.85	-3.26	-0.01	0.16	0.09	0.00	0.00	
Alt My	0.00	0.00	0.18	-0.19	0.00	0.01	0.01	
P108-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	-1.34	-0.88	(azaltma)	Nq=	-0.88×1.000	=	-0.88)	-1.88
Alt Mx	0.31	0.11	0.05	0.06	0.07	0.10	0.05	1.21
Alt My	-1.33	-0.32	-0.09	-0.22	-0.18	-0.30	-0.16	0.13
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-7.65	8.71	0.19	-0.68	-0.25	0.00	0.00	
Alt Mx	2.85	-3.26	-0.01	0.16	0.09	0.00	0.00	
Alt My	0.00	0.00	0.18	-0.19	0.00	0.01	0.01	
P109-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	1.39	-0.23	(azaltma)	Nq=	-0.23×1.000	=	-0.23)	-0.71
Alt Mx	0.62	0.13	0.10	0.03	0.03	0.15	0.09	1.46
Alt My	-0.56	-0.13	-0.02	-0.11	-0.07	-0.13	-0.07	0.08
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-1.71	2.00	-2.79	2.42	-0.06	-0.12	-0.12	
Alt Mx	6.53	-7.38	-2.48	2.70	0.21	-0.10	-0.10	
Alt My	0.00	0.00	0.19	-0.18	0.00	0.01	0.01	
P109-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	1.39	-0.23	(azaltma)	Nq=	-0.23×1.000	=	-0.23)	-0.71
Alt Mx	0.62	0.13	0.10	0.03	0.03	0.15	0.09	1.46
Alt My	-0.56	-0.13	-0.02	-0.11	-0.07	-0.13	-0.07	0.08
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-1.71	2.00	-2.79	2.42	-0.06	-0.12	-0.12	
Alt Mx	6.53	-7.38	-2.48	2.70	0.21	-0.10	-0.10	
Alt My	0.00	0.00	0.19	-0.18	0.00	0.01	0.01	
P110-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	2.17	0.15	(azaltma)	Nq=	0.15×1.000	=	0.15)	-0.68
Alt Mx	-0.24	-0.04	-0.02	-0.03	-0.02	-0.04	-0.02	0.32
Alt My	-0.03	-0.01	0.00	0.00	0.00	-0.01	0.00	0.03
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-2.60	3.00	-2.24	1.84	-0.09	-0.10	-0.10	
Alt Mx	0.82	-0.94	0.43	-0.34	0.03	0.02	0.02	
Alt My	0.00	0.00	0.10	-0.09	0.00	0.00	0.00	
P110-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	2.17	0.15	(azaltma)	Nq=	0.15×1.000	=	0.15)	-0.68
Alt Mx	-0.24	-0.04	-0.02	-0.03	-0.02	-0.04	-0.02	0.32
Alt My	-0.03	-0.01	0.00	0.00	0.00	-0.01	0.00	0.03
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-2.60	3.00	-2.24	1.84	-0.09	-0.10	-0.10	
Alt Mx	0.82	-0.94	0.43	-0.34	0.03	0.02	0.02	
Alt My	0.00	0.00	0.10	-0.09	0.00	0.00	0.00	
P111-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	1.71	0.01	(azaltma)	Nq=	0.01×1.000	=	0.01)	0.09
Alt Mx	-0.01	0.01	0.02	-0.01	0.00	0.02	0.01	0.48
Alt My	-0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.03
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-1.48	1.76	-1.58	1.17	-0.05	-0.07	-0.07	
Alt Mx	2.55	-2.87	-0.51	0.59	0.09	-0.02	-0.02	
Alt My	0.00	0.00	0.07	-0.06	0.00	0.00	0.00	
P111-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	1.71	0.01	(azaltma)	Nq=	0.01×1.000	=	0.01)	0.09
Alt Mx	-0.01	0.01	0.02	-0.01	0.00	0.02	0.01	0.48
Alt My	-0.01	0.00	0.00	0.00	0.00	0.00	0.00	0.03
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-1.48	1.76	-1.58	1.17	-0.05	-0.07	-0.07	
Alt Mx	2.55	-2.87	-0.51	0.59	0.09	-0.02	-0.02	
Alt My	0.00	0.00	0.07	-0.06	0.00	0.00	0.00	

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P112-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	0.86	-0.59	(azaltma	Nq=	-0.59×1.000	=	-0.59)	-2.81
Alt Mx	-0.91	-0.25	-0.08	-0.17	-0.18	-0.17	-0.16	0.17
Alt My	0.75	0.18	0.08	0.10	0.15	0.12	0.09	-0.08
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-7.15	6.60	4.50	-5.32	-0.17	0.19	0.19	
Alt Mx	-0.92	0.64	-2.77	3.53	-0.02	-0.11	-0.11	
Alt My	0.01	0.00	0.17	-0.21	0.00	0.01	0.01	
P112-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	0.86	-0.59	(azaltma	Nq=	-0.59×1.000	=	-0.59)	-2.81
Alt Mx	-0.91	-0.25	-0.08	-0.17	-0.18	-0.17	-0.16	0.17
Alt My	0.75	0.18	0.08	0.10	0.15	0.12	0.09	-0.08
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-7.15	6.60	4.50	-5.32	-0.17	0.19	0.19	
Alt Mx	-0.92	0.64	-2.77	3.53	-0.02	-0.11	-0.11	
Alt My	0.01	0.00	0.17	-0.21	0.00	0.01	0.01	
P113-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	-2.13	-1.15	(azaltma	Nq=	-1.15×1.000	=	-1.15)	-2.61
Alt Mx	0.34	0.09	0.04	0.05	0.05	0.08	0.05	1.47
Alt My	1.48	0.36	0.15	0.20	0.25	0.28	0.18	-0.14
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-9.32	8.25	0.17	0.23	-0.21	0.01	0.01	
Alt Mx	2.77	-2.44	-0.21	0.12	0.06	-0.01	-0.01	
Alt My	0.00	0.00	0.17	-0.19	0.00	0.01	0.01	
P113-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	-2.13	-1.15	(azaltma	Nq=	-1.15×1.000	=	-1.15)	-2.61
Alt Mx	0.34	0.09	0.04	0.05	0.05	0.08	0.05	1.47
Alt My	1.48	0.36	0.15	0.20	0.25	0.28	0.18	-0.14
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-9.32	8.25	0.17	0.23	-0.21	0.01	0.01	
Alt Mx	2.77	-2.44	-0.21	0.12	0.06	-0.01	-0.01	
Alt My	0.00	0.00	0.17	-0.19	0.00	0.01	0.01	
P114-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	-0.69	-0.79	(azaltma	Nq=	-0.79×1.000	=	-0.79)	-1.66
Alt Mx	0.48	0.14	0.07	0.06	0.07	0.12	0.07	1.14
Alt My	1.33	0.32	0.09	0.22	0.18	0.30	0.16	-0.13
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-8.43	7.46	-0.04	0.50	-0.19	0.00	0.00	
Alt Mx	3.16	-2.79	0.03	-0.16	0.07	0.00	0.00	
Alt My	0.00	0.00	0.18	-0.19	0.00	0.01	0.01	
P114-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	-0.69	-0.79	(azaltma	Nq=	-0.79×1.000	=	-0.79)	-1.66
Alt Mx	0.48	0.14	0.07	0.06	0.07	0.12	0.07	1.14
Alt My	1.33	0.32	0.09	0.22	0.18	0.30	0.16	-0.13
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-8.43	7.46	-0.04	0.50	-0.19	0.00	0.00	
Alt Mx	3.16	-2.79	0.03	-0.16	0.07	0.00	0.00	
Alt My	0.00	0.00	0.18	-0.19	0.00	0.01	0.01	
P115-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	2.60	-0.06	(azaltma	Nq=	-0.06×1.000	=	-0.06)	-0.16
Alt Mx	0.26	0.07	0.06	0.01	0.01	0.09	0.05	1.68
Alt My	0.56	0.13	0.02	0.11	0.07	0.13	0.07	-0.07
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-1.98	1.69	3.64	-3.19	-0.04	0.15	0.15	
Alt Mx	7.00	-6.24	2.91	-3.04	0.16	0.11	0.11	
Alt My	0.00	0.00	0.20	-0.19	0.00	0.01	0.01	
P115-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	2.60	-0.06	(azaltma	Nq=	-0.06×1.000	=	-0.06)	-0.16
Alt Mx	0.26	0.07	0.06	0.01	0.01	0.09	0.05	1.68
Alt My	0.56	0.13	0.02	0.11	0.07	0.13	0.07	-0.07
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-1.98	1.69	3.64	-3.19	-0.04	0.15	0.15	
Alt Mx	7.00	-6.24	2.91	-3.04	0.16	0.11	0.11	
Alt My	0.00	0.00	0.20	-0.19	0.00	0.01	0.01	
P116-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	6.90	0.68	(azaltma	Nq=	0.68×1.000	=	0.68)	0.11
Alt Mx	-0.45	-0.09	0.02	-0.12	-0.09	-0.09	-0.01	0.75
Alt My	0.07	0.01	0.01	0.00	0.00	0.01	0.01	-0.04
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.60	-0.80	6.91	-5.91	0.02	0.29	0.29	
Alt Mx	7.54	-6.84	-0.05	0.03	0.18	0.00	0.00	
Alt My	0.00	0.00	0.20	-0.17	0.00	0.01	0.01	

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P116-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	6.90	0.68	(azaltma)	Nq=	0.68×1.000	=	0.68)	0.11
Alt Mx	-0.45	-0.09	0.02	-0.12	-0.09	-0.09	-0.01	0.75
Alt My	0.07	0.01	0.01	0.00	0.00	0.01	0.01	-0.04
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.60	-0.80	6.91	-5.91	0.02	0.29	0.29	
Alt Mx	7.54	-6.84	-0.05	0.03	0.18	0.00	0.00	
Alt My	0.00	0.00	0.20	-0.17	0.00	0.01	0.01	
P117-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	12.63	1.46	(azaltma)	Nq=	1.46×1.000	=	1.46)	-0.50
Alt Mx	-0.51	-0.13	-0.03	-0.10	-0.12	-0.04	-0.10	0.39
Alt My	-0.25	-0.03	-0.04	0.01	0.01	-0.02	-0.04	0.06
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-2.10	2.11	0.00	0.00	-0.06	0.00	0.00	
Alt Mx	0.33	-0.33	0.00	0.00	0.01	0.00	0.00	
Alt My	-0.75	-1.59	-44.15	55.58	0.06	-1.83	-1.83	
P117-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	12.63	1.46	(azaltma)	Nq=	1.46×1.000	=	1.46)	-0.50
Alt Mx	-0.51	-0.13	-0.03	-0.10	-0.12	-0.04	-0.10	0.39
Alt My	-0.25	-0.03	-0.04	0.01	0.01	-0.02	-0.04	0.06
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	-2.10	2.11	0.00	0.00	-0.06	0.00	0.00	
Alt Mx	0.33	-0.33	0.00	0.00	0.01	0.00	0.00	
Alt My	-0.75	-1.59	-44.15	55.58	0.06	-1.83	-1.83	
P118-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	14.97	2.35	(azaltma)	Nq=	2.35×1.000	=	2.35)	1.58
Alt Mx	0.12	0.03	-0.07	0.10	0.08	0.03	-0.05	0.13
Alt My	-3.04	-0.59	-0.43	-0.16	-0.13	-0.58	-0.47	2.11
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.19	-0.29	6.88	-6.28	0.01	0.29	0.29	
Alt Mx	0.32	-0.32	0.00	0.00	0.01	0.00	0.00	
Alt My	0.55	-0.27	-23.44	21.41	0.01	-0.93	-0.93	
P118-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	14.97	2.35	(azaltma)	Nq=	2.35×1.000	=	2.35)	1.58
Alt Mx	0.12	0.03	-0.07	0.10	0.08	0.03	-0.05	0.13
Alt My	-3.04	-0.59	-0.43	-0.16	-0.13	-0.58	-0.47	2.11
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.19	-0.29	6.88	-6.28	0.01	0.29	0.29	
Alt Mx	0.32	-0.32	0.00	0.00	0.01	0.00	0.00	
Alt My	0.55	-0.27	-23.44	21.41	0.01	-0.93	-0.93	
P119-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	3.56	0.42	(azaltma)	Nq=	0.42×1.000	=	0.42)	0.05
Alt Mx	0.00	0.00	-0.02	0.02	0.01	0.00	-0.01	0.04
Alt My	0.74	0.19	0.08	0.11	0.09	0.18	0.10	-0.80
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.15	-0.16	-0.48	0.44	0.00	-0.02	-0.02	
Alt Mx	0.09	-0.09	0.00	0.00	0.00	0.00	0.00	
Alt My	0.04	0.03	-4.10	3.76	0.00	-0.17	-0.17	
P119-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	3.56	0.42	(azaltma)	Nq=	0.42×1.000	=	0.42)	0.05
Alt Mx	0.00	0.00	-0.02	0.02	0.01	0.00	-0.01	0.04
Alt My	0.74	0.19	0.08	0.11	0.09	0.18	0.10	-0.80
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.15	-0.16	-0.48	0.44	0.00	-0.02	-0.02	
Alt Mx	0.09	-0.09	0.00	0.00	0.00	0.00	0.00	
Alt My	0.04	0.03	-4.10	3.76	0.00	-0.17	-0.17	
P120-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	10.61	1.08	(azaltma)	Nq=	1.08×1.000	=	1.08)	1.02
Alt Mx	0.24	0.06	0.07	-0.01	0.00	0.07	0.07	-0.20
Alt My	-1.32	-0.33	-0.39	0.07	0.06	-0.34	-0.38	2.53
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	1.47	-1.68	4.66	-3.68	0.05	0.21	0.21	
Alt Mx	0.30	-0.29	0.00	-0.01	0.01	0.00	0.00	
Alt My	-0.76	1.69	-18.70	14.78	-0.05	-0.79	-0.79	
P120-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	10.61	1.08	(azaltma)	Nq=	1.08×1.000	=	1.08)	1.02
Alt Mx	0.24	0.06	0.07	-0.01	0.00	0.07	0.07	-0.20
Alt My	-1.32	-0.33	-0.39	0.07	0.06	-0.34	-0.38	2.53
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	1.47	-1.68	4.66	-3.68	0.05	0.21	0.21	
Alt Mx	0.30	-0.29	0.00	-0.01	0.01	0.00	0.00	
Alt My	-0.76	1.69	-18.70	14.78	-0.05	-0.79	-0.79	

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P121-Sol	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	2.26	0.14	(azaltma	Nq=	0.14×1.000	=	0.14)	0.28
Alt Mx	0.04	0.01	0.01	0.00	0.00	0.01	0.01	-0.04
Alt My	-0.15	0.01	0.02	-0.01	-0.02	0.01	0.02	-0.19
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.42	-0.45	-0.59	0.52	0.01	-0.02	-0.02	
Alt Mx	0.07	-0.08	0.00	0.00	0.00	0.00	0.00	
Alt My	-0.11	0.25	-1.77	1.35	-0.01	-0.08	-0.08	

P121-Sag	GGGGGG	QQQQQQ	Q_Q_Q	Q_Q_Q	QQ_QQ	QQ_QQ	Q_QQ_Q	Zemin
N	2.26	0.14	(azaltma	Nq=	0.14×1.000	=	0.14)	0.28
Alt Mx	0.04	0.01	0.01	0.00	0.00	0.01	0.01	-0.04
Alt My	-0.15	0.01	0.02	-0.01	-0.02	0.01	0.02	-0.19
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar X	Rüzgar Y		
N	0.42	-0.45	-0.59	0.52	0.01	-0.02	-0.02	
Alt Mx	0.07	-0.08	0.00	0.00	0.00	0.00	0.00	
Alt My	-0.11	0.25	-1.77	1.35	-0.01	-0.08	-0.08	

TOPLAM $\Sigma N_g = 416.69$ $\Sigma N_q = 58.85$ $\Sigma N_{qf} = 58.85$

Temellerin kayma kontrolü TBDY2018-16.8.4 (t,m)

$\Phi = 30.0^\circ$ $\theta = 0, \beta = 0, \varphi = 90^\circ$ $K_p = \sin^2(90 + \Phi) / (1 - \sin \Phi)^2 = 3.0$

Kat	Hi	Lx	Ly	RpkX = Hi·Kpd·Ly	RpkY = Hi·Kpd·Lx
TEMEL	0.50	13.70	8.60	12.90	20.55
1	4.60	13.70	8.60	118.68	189.06

$RpX = 131.58/1.4 = 93.98$, $RpY = 209.60/1.4 = 149.72$
 $W_g = 416.69(\text{Yapı}) + 206.19(\text{Temel}) = 622.87$
 $W_q = 622.87, W_{qf} = 58.85$
 $W_{qf} = W_g + C_q \cdot W_q = 681.72$

$V_{beX} = 88.8$, $V_{beY} = 90.26$ deprem, $V_{bsX} = 43.99$, $V_{bsY} = 1.21$ zemin

$V_{eX} = 88.8 + 43.99 = 132.79 < W_{ge} \cdot \tan \delta + 0.3 \cdot R_{pX} = 681.72 \cdot 0.5 + 0.3 \cdot 93.98 = 369.06$ ✓
 $V_{eY} = 90.26 + 1.21 = 91.47 < W_{ge} \cdot \tan \delta + 0.3 \cdot R_{pY} = 681.72 \cdot 0.5 + 0.3 \cdot 149.72 = 385.78$ ✓
 Temellerin kayma kontrolü yeterlidir

TEMELLERE KOLONLARDAN GELEN SÜNEK TASARIM DEPREM MOMENTLERİ (tm)

Kolon ve Perdelerde $Nez = Dalt \times Ne$, (Dalt=1.5) TBDY2018-4.10.3.2 Bodrumlu yapı

KOLON	Kolon/Perde koşulu	Mex1 (9)	Mex2 (10)	Mpx	Mey1 (11)	Mey2 (12)	Mpy
S101	Kolon Me=Dalt×Me	0.33	-0.37		2.76	-3.50	
S102	Kolon Me=Dalt×Me	3.24	-3.70		0.49	-0.59	
S103	Kolon Me=Dalt×Me	3.33	-3.79		0.59	-0.65	
S104	Kolon Me=Dalt×Me	3.36	-3.82		0.55	-0.56	
S105	Kolon Me=Dalt×Me	3.34	-3.79		0.40	-0.37	
S106	Kolon Me=Dalt×Me	3.28	-3.72		0.30	-0.25	
S107	Kolon Me=Dalt×Me	0.33	-0.38		2.46	-1.91	
S108	Kolon Me=Dalt×Me	0.46	-0.49		3.68	-3.38	
S109	Kolon Me=Dalt×Me	0.44	-0.47		2.41	-1.86	
S110	Kolon Me=Dalt×Me	0.36	-0.32		2.77	-3.50	
S111	Kolon Me=Dalt×Me	3.59	-3.17		0.49	-0.59	
S112	Kolon Me=Dalt×Me	3.66	-3.24		0.59	-0.65	
S113	Kolon Me=Dalt×Me	3.65	-3.24		0.55	-0.56	
S114	Kolon Me=Dalt×Me	3.56	-3.15		0.39	-0.36	
S115	Kolon Me=Dalt×Me	0.37	-0.33		2.32	-1.79	
P106	Perde Me=Dalt×Me ≤ Mp	-2.17	3.01	1228.32	0.51	-0.63	0.00
P107	Perde Me=Dalt×Me ≤ Mp	7.49	-8.57	1261.32	0.51	-0.58	0.00
P108	Perde Me=Dalt×Me ≤ Mp	8.56	-9.77	1267.43	0.54	-0.57	0.00
P109	Perde Me=Dalt×Me ≤ Mp	19.58	-22.14	1071.46	0.56	-0.54	0.00
P110	Perde Me=Dalt×Me ≤ Mp	2.47	-2.82	1088.82	0.29	-0.26	0.00
P111	Perde Me=Dalt×Me ≤ Mp	7.64	-8.61	772.20	0.22	-0.18	0.00
P112	Perde Me=Dalt×Me ≤ Mp	-2.75	1.93	1230.11	0.51	-0.63	0.00
P113	Perde Me=Dalt×Me ≤ Mp	8.31	-7.33	1262.13	0.51	-0.58	0.00
P114	Perde Me=Dalt×Me ≤ Mp	9.49	-8.38	1270.58	0.54	-0.58	0.00
P115	Perde Me=Dalt×Me ≤ Mp	21.01	-18.71	1073.80	0.60	-0.58	0.00
P116	Perde Me=Dalt×Me ≤ Mp	22.61	-20.52	1995.83	0.61	-0.52	0.00
P117	Perde Me=Dalt×Me ≤ Mp	0.99	-1.00	0.00	-132.45	166.74	5653.62
P118	Perde Me=Dalt×Me ≤ Mp	0.97	-0.95	0.00	-70.31	64.23	3780.72
P119	Perde Me=Dalt×Me ≤ Mp	0.26	-0.28	0.00	-12.30	11.28	925.73
P120	Perde Me=Dalt×Me ≤ Mp	0.90	-0.88	0.00	-56.10	44.33	3872.80
P121	Perde Me=Dalt×Me ≤ Mp	0.21	-0.24	0.00	-5.31	4.04	1125.93

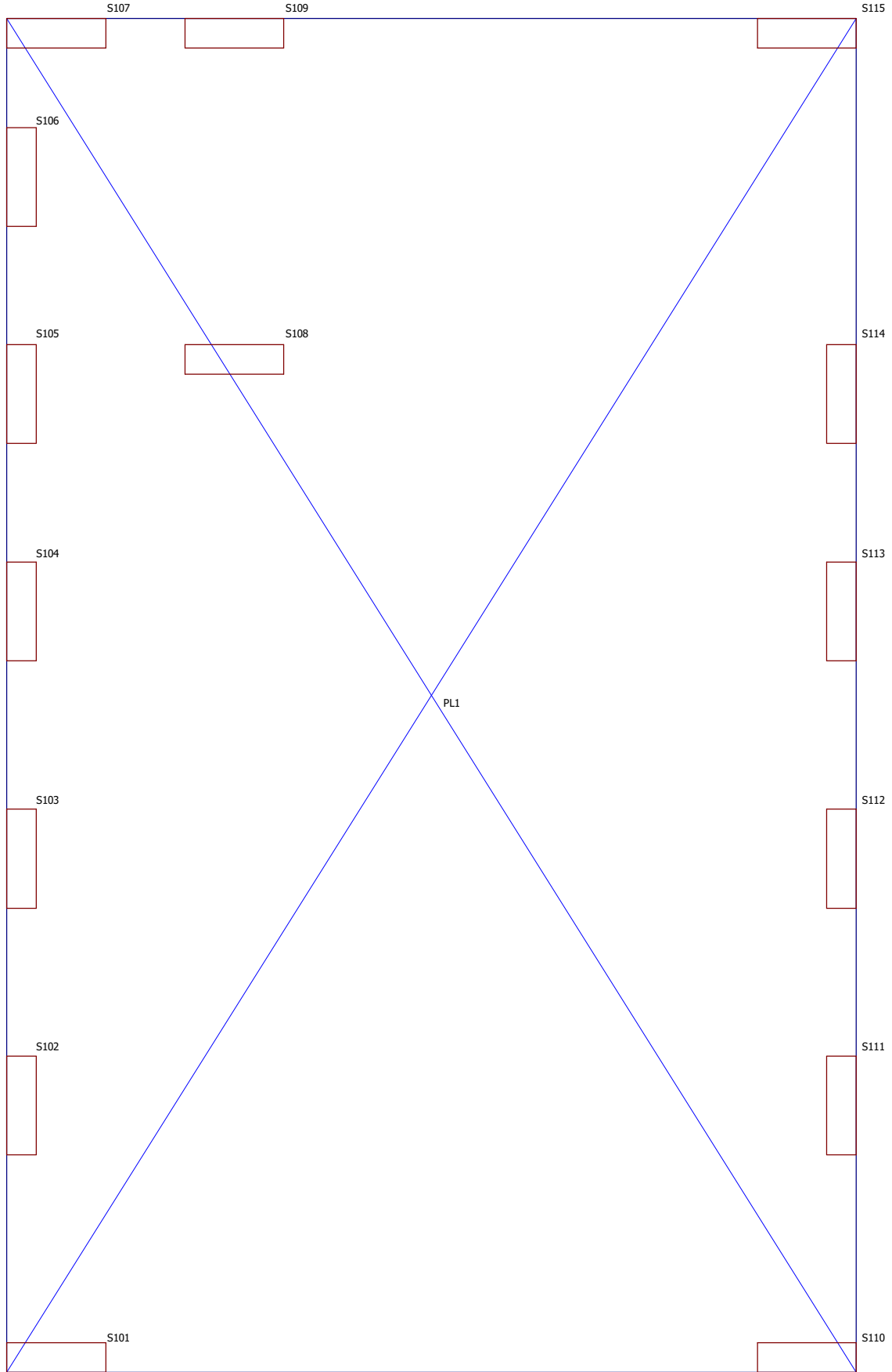
PANEL+BAŞLIK TOPLAM REAKSIYONLARI

P106	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	24.88	3.08	(azaltma)	Nq=	3.08×1.000	=	3.08)	-7.50
Alt Mx	20.73	5.00	2.70	2.30	4.39	3.34	2.28	0.58
Alt My	1.80	-0.04	-0.10	0.07	0.05	-0.21	0.09	-0.09
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	-14.95	16.34	-10.73	12.69	-0.43	-0.45	0.00	0.00
Alt Mx	0.70	-0.38	6.75	-8.41	0.00	0.28	0.00	0.00
Alt My	-0.71	0.84	0.65	-0.85	-0.02	0.03	0.00	0.00
P107	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	36.09	6.44	(azaltma)	Nq=	6.44×1.000	=	6.44)	-7.12
Alt Mx	4.27	1.15	0.18	0.97	-0.78	2.58	0.50	4.36
Alt My	-0.13	-0.18	-0.06	-0.12	-0.10	-0.17	-0.08	0.34
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	-17.19	19.55	-0.45	-0.36	-0.53	-0.02	0.00	0.00
Alt Mx	7.61	-8.66	0.96	-0.75	0.22	0.04	0.00	0.00
Alt My	-0.06	0.07	0.67	-0.76	0.00	0.03	0.00	0.00
P108	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	35.81	6.61	(azaltma)	Nq=	6.61×1.000	=	6.61)	-4.84
Alt Mx	-5.52	-1.25	-1.85	0.61	-1.05	-0.78	-0.66	3.46
Alt My	0.02	-0.13	-0.05	-0.08	-0.09	-0.09	-0.07	0.37
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	-15.25	17.35	0.36	-1.40	-0.49	0.01	0.00	0.00
Alt Mx	7.98	-9.09	-0.31	0.70	0.24	-0.01	0.00	0.00
Alt My	0.01	-0.01	0.74	-0.79	0.00	0.03	0.00	0.00
P109	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	20.63	3.09	(azaltma)	Nq=	3.09×1.000	=	3.09)	-1.78
Alt Mx	-16.25	-3.79	-0.28	-3.51	-2.04	-3.68	-1.86	4.11
Alt My	0.22	-0.06	-0.04	-0.02	-0.04	-0.04	-0.04	0.25
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	-3.27	3.85	-6.11	5.28	-0.12	-0.26	0.00	0.00
Alt Mx	14.97	-16.94	-5.35	5.88	0.48	-0.21	0.00	0.00
Alt My	0.03	-0.03	0.56	-0.56	0.00	0.02	0.00	0.00
P110	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	8.29	0.44	(azaltma)	Nq=	0.44×1.000	=	0.44)	-1.43
Alt Mx	1.50	0.18	0.14	0.04	0.08	0.16	0.13	0.80
Alt My	0.46	-0.01	0.00	0.00	0.00	0.00	-0.02	0.14
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	-4.70	5.47	-5.75	4.81	-0.16	-0.25	0.00	0.00
Alt Mx	3.80	-4.32	0.28	-0.05	0.13	0.01	0.00	0.00
Alt My	0.07	-0.09	0.19	-0.17	0.00	0.01	0.00	0.00
P111	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	9.22	0.37	(azaltma)	Nq=	0.37×1.000	=	0.37)	0.31
Alt Mx	-1.10	-0.08	-0.03	-0.05	-0.06	-0.08	-0.03	1.53
Alt My	1.75	0.08	0.03	0.05	0.06	0.07	0.03	0.37
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	-1.89	2.38	-5.15	4.08	-0.07	-0.23	0.00	0.00
Alt Mx	6.31	-7.11	-0.92	1.16	0.21	-0.04	0.00	0.00
Alt My	0.40	-0.49	0.38	-0.24	0.01	0.02	0.00	0.00
P112	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	24.59	3.02	(azaltma)	Nq=	3.02×1.000	=	3.02)	-7.21
Alt Mx	20.50	4.97	2.66	2.30	4.39	3.31	2.24	0.64
Alt My	-1.75	0.05	0.11	-0.06	-0.05	0.22	-0.08	0.07
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	-16.04	14.83	10.72	-12.77	-0.39	0.45	0.00	0.00
Alt Mx	0.48	-0.82	-6.78	8.44	0.02	-0.28	0.00	0.00
Alt My	0.80	-0.68	0.66	-0.85	0.02	0.03	0.00	0.00
P113	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	35.92	6.39	(azaltma)	Nq=	6.39×1.000	=	6.39)	-6.64
Alt Mx	4.57	1.19	0.21	0.98	-0.77	2.62	0.54	4.24
Alt My	0.15	0.18	0.07	0.12	0.10	0.18	0.09	-0.34
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	-19.03	16.87	0.48	0.23	-0.44	0.02	0.00	0.00
Alt Mx	8.35	-7.39	-0.96	0.79	0.19	-0.04	0.00	0.00
Alt My	0.07	-0.06	0.68	-0.76	0.00	0.03	0.00	0.00
P114	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	37.58	6.84	(azaltma)	Nq=	6.84×1.000	=	6.84)	-4.37
Alt Mx	-4.47	-1.09	-1.73	0.64	-1.02	-0.62	-0.53	3.27
Alt My	-0.09	0.12	0.05	0.07	0.09	0.09	0.06	-0.37
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	-16.96	15.00	0.00	0.99	-0.39	0.01	0.00	0.00
Alt Mx	8.74	-7.73	0.46	-0.77	0.20	0.02	0.00	0.00
Alt My	0.01	-0.01	0.73	-0.78	0.00	0.03	0.00	0.00

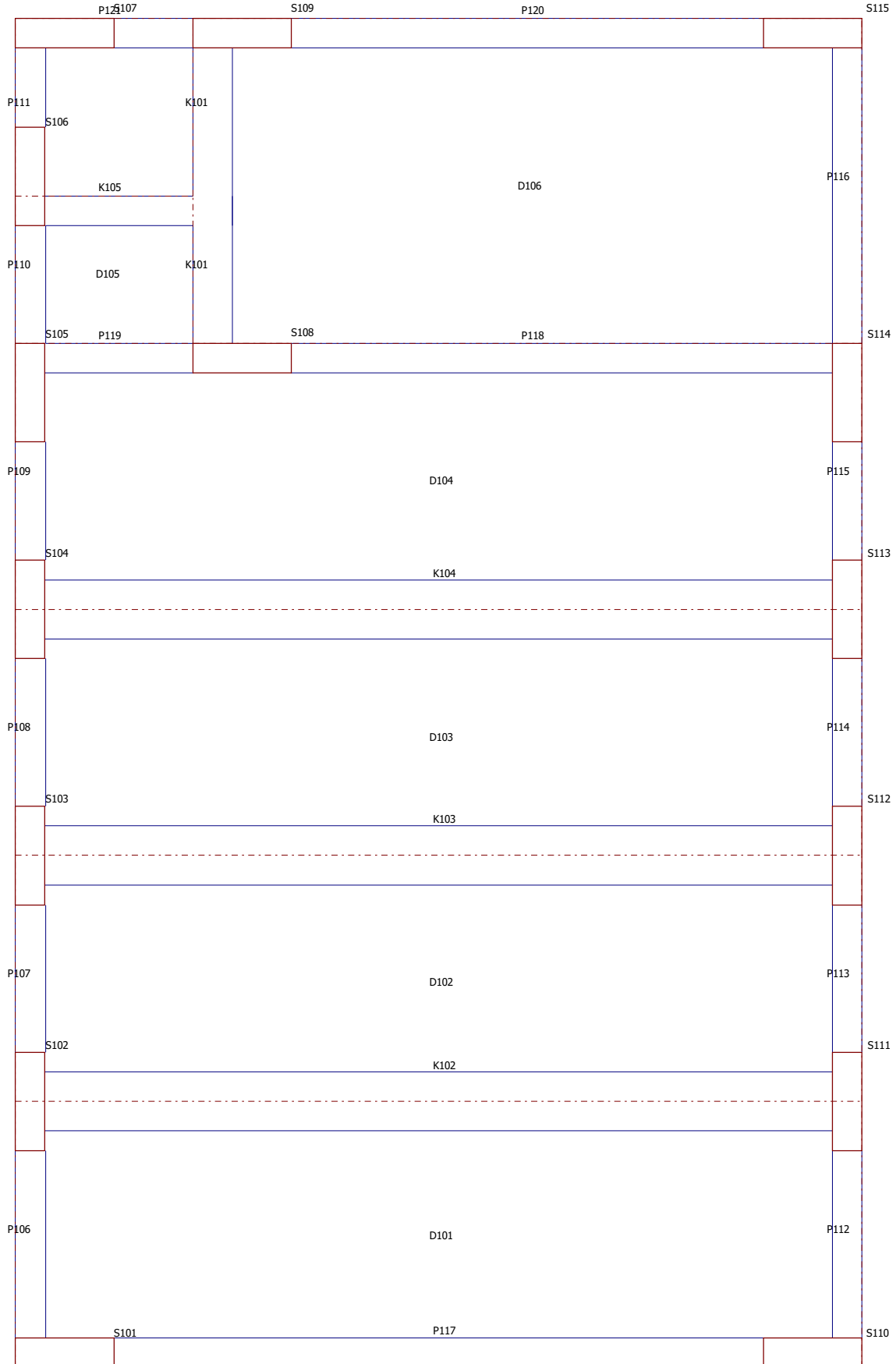
PANEL+BAŞLIK TOPLAM REAKSIYONLARI

P115	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	24.86	3.69	(azaltma	Nq=	3.69×1.000	=	3.69)	-0.74
Alt Mx	-16.21	-3.78	-0.24	-3.53	-2.06	-3.68	-1.81	4.44
Alt My	-0.48	0.02	0.00	0.01	0.03	0.00	0.00	-0.22
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	-3.95	3.35	8.11	-7.08	-0.09	0.33	0.00	0.00
Alt Mx	16.15	-14.38	6.33	-6.67	0.37	0.25	0.00	0.00
Alt My	-0.01	0.01	0.54	-0.55	0.00	0.02	0.00	0.00
P116	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	22.07	2.13	(azaltma	Nq=	2.13×1.000	=	2.13)	0.25
Alt Mx	4.24	0.55	0.69	-0.13	-0.06	0.49	0.68	1.59
Alt My	-3.11	-0.28	-0.26	-0.03	-0.04	-0.28	-0.25	-0.23
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	2.59	-2.91	16.15	-13.86	0.08	0.67	0.00	0.00
Alt Mx	18.04	-16.41	1.42	-1.30	0.43	0.07	0.00	0.00
Alt My	-0.70	0.60	0.32	-0.20	-0.02	0.01	0.00	0.00
P117	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	33.90	3.43	(azaltma	Nq=	3.43×1.000	=	3.43)	-2.57
Alt Mx	0.30	-0.18	-0.09	-0.09	-0.15	-0.13	-0.08	0.69
Alt My	-0.60	-0.07	-0.09	0.02	0.02	-0.07	-0.09	0.19
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	-6.88	6.92	-0.01	-0.02	-0.18	0.00	0.00	0.00
Alt Mx	0.49	-0.49	0.00	0.00	0.01	0.00	0.00	0.00
Alt My	-1.74	-3.53	-75.34	95.49	0.12	-3.13	0.00	0.00
P118	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	40.09	6.21	(azaltma	Nq=	6.21×1.000	=	6.21)	3.49
Alt Mx	-2.15	-0.22	-0.27	0.04	0.02	-0.24	-0.23	0.46
Alt My	-25.06	-5.26	-0.90	-4.36	-3.62	-5.16	-1.75	3.57
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	0.59	-0.81	13.97	-12.74	0.02	0.59	0.00	0.00
Alt Mx	1.54	-1.44	-0.25	0.18	0.04	-0.01	0.00	0.00
Alt My	0.80	-0.23	-42.32	38.72	0.01	-1.66	0.00	0.00
P119	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	16.00	2.15	(azaltma	Nq=	2.15×1.000	=	2.15)	0.48
Alt Mx	-1.72	-0.18	-0.07	-0.10	-0.09	-0.19	-0.07	0.24
Alt My	10.09	2.07	0.31	1.76	1.46	2.04	0.65	-1.11
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	0.56	-0.59	-1.81	1.63	0.01	-0.08	0.00	0.00
Alt Mx	0.99	-1.12	0.23	-0.16	0.03	0.01	0.00	0.00
Alt My	0.17	-0.07	-7.05	6.46	0.00	-0.30	0.00	0.00
P120	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	33.25	3.65	(azaltma	Nq=	3.65×1.000	=	3.65)	1.30
Alt Mx	-1.18	-0.06	-0.04	-0.02	-0.02	-0.05	-0.04	-0.39
Alt My	-2.91	-1.34	-1.74	0.40	0.37	-1.38	-1.67	6.99
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	4.50	-4.85	10.42	-8.34	0.14	0.47	0.00	0.00
Alt Mx	0.63	-0.63	-0.15	0.13	0.02	-0.01	0.00	0.00
Alt My	1.62	0.36	-29.23	22.66	-0.02	-1.23	0.00	0.00
P121	GGGGGG	QQQQQQ	Q_Q_Q	_Q_Q_Q	QQ_QQ	=_QQ_QQ	Q_QQ_Q	Zemin
N	13.49	1.30	(azaltma	Nq=	1.30×1.000	=	1.30)	0.13
Alt Mx	-1.12	-0.09	-0.08	-0.02	-0.02	-0.09	-0.08	-0.12
Alt My	2.44	0.64	0.75	-0.11	-0.11	0.65	0.73	-1.08
	Deprem+X	Deprem-X	Deprem+Y	Deprem-Y	Rüzgar+X	Rüzgar-X	Rüzgar+Y	Rüzgar-Y
N	1.75	-1.86	-2.90	2.51	0.05	-0.13	0.00	0.00
Alt Mx	0.26	-0.30	0.26	-0.20	0.01	0.01	0.00	0.00
Alt My	-0.59	0.80	-1.44	1.00	-0.02	-0.07	0.00	0.00

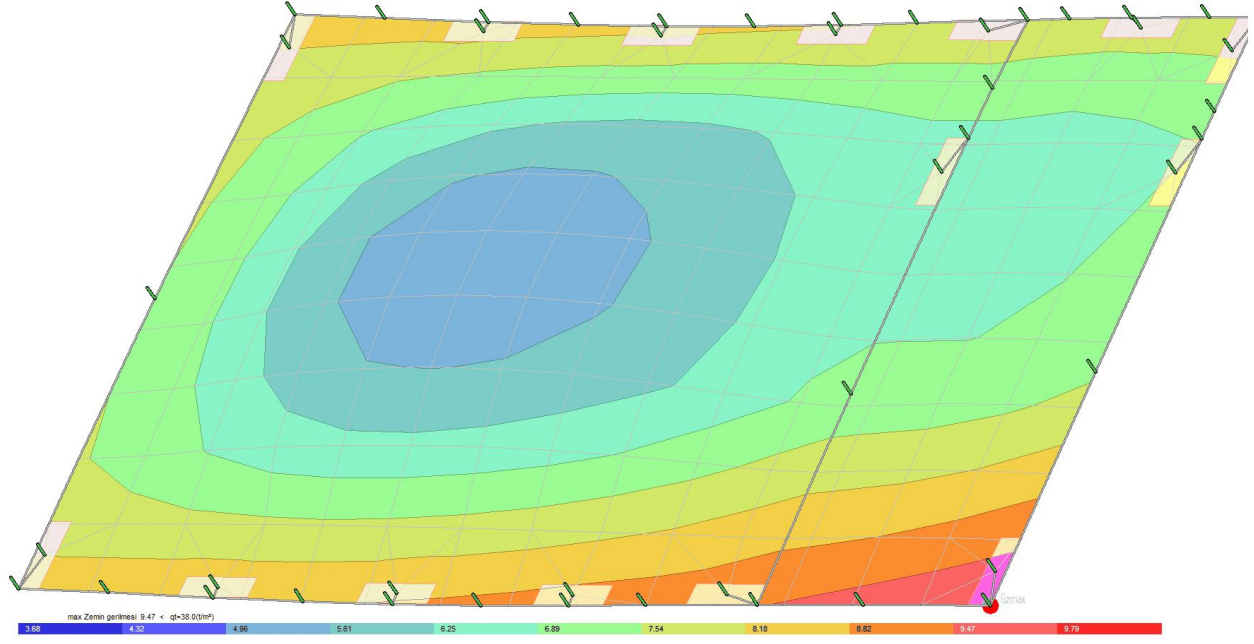
TEMEL APLİKASYON PLANI



1. NORMAL KAT KALIP APLIKASYON PLANI

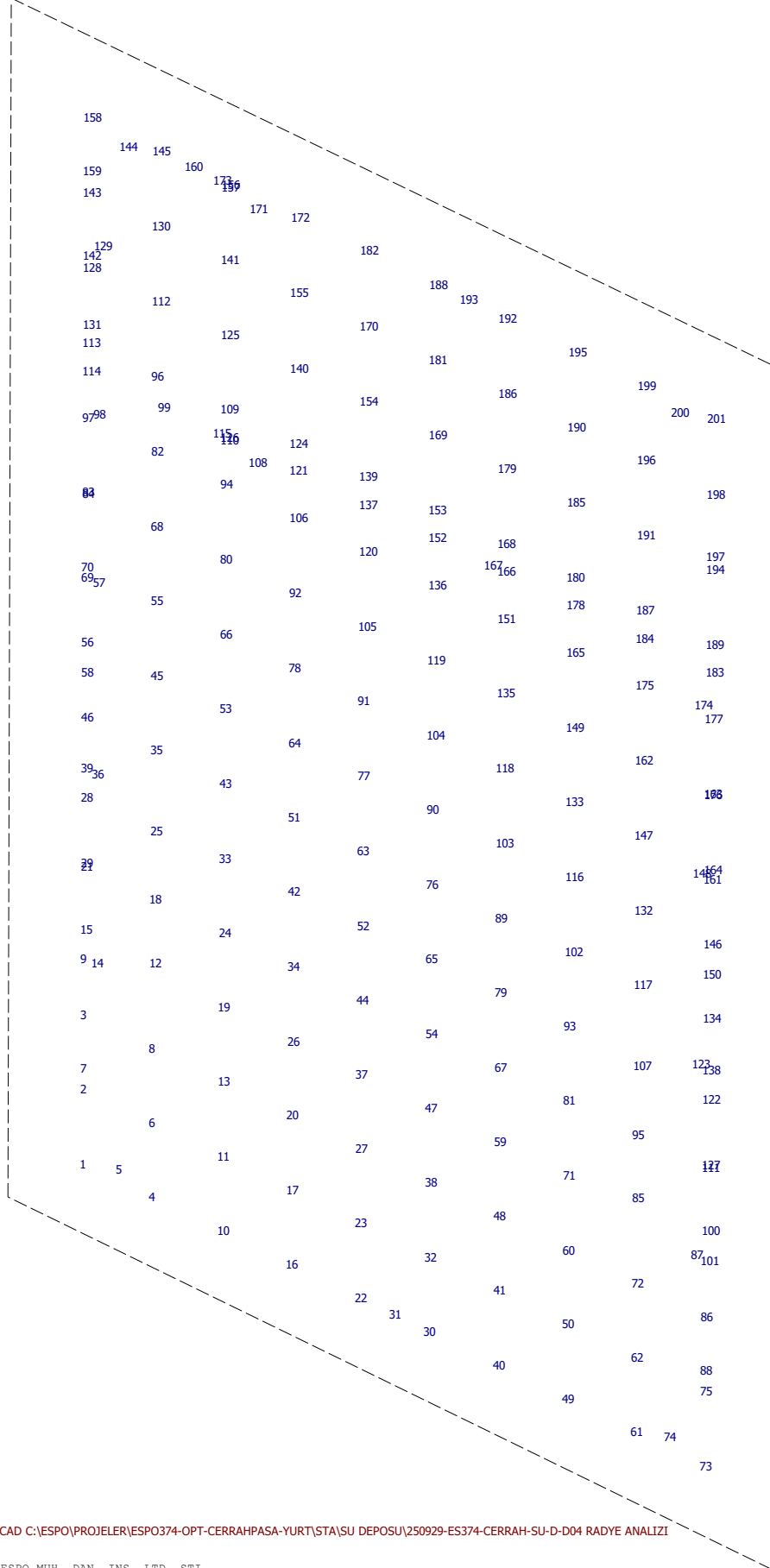


TEMEL 3D GÖRÜNÜŞÜ



Mx

Kenar Bolge : -----
 Kenar Bolgesiz :



STA4-CAD Ver.14.1 RADYE PROGRAMI**RADYE MAT TEMELLERİN SONLU ELEMANLARLA ANALİZİ**ZEMİN YATAK KATSAYISI (t/m³) : 2000.0ZEMİN TAŞIMA GÜCÜ TAS. GER. (t/m²): 38.0

BETONARME HESAP YÖNTEMİ:TAŞIMA GÜCÜ YÖNTEMİ TS500-2000

BETON ve ÇELİK MALZEME BİLGİLERİ

Beton dayanım gerilmesi (kg/cm²):350Çelik akma gerilmesi (kg/cm²):4200

Minimum çekme bölgesi pirsantajı :0.001

Minimum toplam kesit pirsantajı :0.004

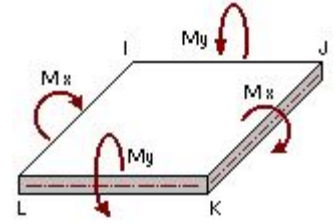
Winkler Yayları Opsiyonu:Ks=1,5 Ko (İki bolgeli zemin)

Nokta Tasarım Momenti Opsiyonu ...:Bağlı düğüm noktalarının tasarım momentlerinin ortalaması göre hesaplama

BETONARME HESAP YÜK KOMBİNASYON PARAMETRESİ

Ölü yük Cg	Hareketli yük Cq	Zemin Cs	Deprem ± Ce	Rüzgar ± Cw	Isı Ct
1.40	1.60	0.00	0.00	0.00	0.00
1.40	1.60	1.60	0.00	0.00	0.00
1.00	1.20	0.00	0.00	0.00	1.20
1.00	1.00	0.00	1.00	0.00	0.00
1.00	1.00	1.00	1.00	0.00	0.00
0.90	0.00	0.00	1.00	0.00	0.00
1.00	1.30	0.00	0.00	1.30	0.00
1.00	1.30	1.00	0.00	1.30	0.00
0.90	0.00	0.00	0.00	1.30	0.00
0.90	0.00	0.90	0.00	1.30	0.00

CODE:TS500T.COD

**ZEMİN GERİLMESİ YÜK KOMBİNASYONU $q_o < q_t$**

Ölü yük Cg	Hareketli yük Cq	Zemin Cs	Deprem ± Ce	Rüzgar ± Cw	Isı Ct
1.40	1.60	0.00	0.00	0.00	0.00
1.40	1.60	1.60	0.00	0.00	0.00
1.00	1.20	0.00	0.00	0.00	1.20
1.00	1.00	0.00	1.00	0.00	0.00
1.00	1.00	1.00	1.00	0.00	0.00
0.90	0.00	0.00	1.00	0.00	0.00
1.00	1.30	0.00	0.00	1.30	0.00
1.00	1.30	1.00	0.00	1.30	0.00
0.90	0.00	0.00	0.00	1.30	0.00
0.90	0.00	0.90	0.00	1.30	0.00

STATİK ANALİZ YÜK KOMBİNASYON NOTASYONLARI:

1. G+G+G+G+G	GENEL ÖLÜ YÜK
2. Q+Q+Q+Q+Q	1. GENEL HAREKETLİ YÜK
3. Q+o+Q+o+Q	2. HAREKETLİ YÜK
4. o+Q+o+Q+o	3. HAREKETLİ YÜK
5. Q+Q+o+Q+Q	4. HAREKETLİ YÜK
6. o+Q+Q+o+Q	5. HAREKETLİ YÜK
7. Q+o+Q+Q+o	6. HAREKETLİ YÜK
8. Gz	Yatay zemin itkisi
9. Ex + %5 x ey	X yönü deprem + %5 eksantrisine
10. Ex - %5 x ey	X yönü deprem - %5 eksantrisine
11. Ey + %5 x ex	Y yönü deprem + %5 eksantrisine
12. Ey - %5 x ex	Y yönü deprem - %5 eksantrisine
13. Wx	X yönü rüzgar
14. Wy	Y yönü rüzgar
15. T	Isı etkisi
17. Ez	Z deprem

Ed(H) = Edx ± 0.3 × Edy, Ed(H) = Edy ± 0.3 × Edx

Ed = Ed(H) ± 0.3 × Edz

FİRMA : ESPO MUH. DAN. INS. LTD. STI.

30-09-2025

SAYFA: 60

PROJE : CERRAHPAŞA YURT SU DEPOSU

(250929-ES374-CERRAH-SU-D-D04.ST4)

PLAK BİLGİLERİ

Plak no	D cm	mesh x y	Ko t/m ³	g t/m ²	p t/m ²	X1	Y1	Z1	X2	Y2	Z2	X3	Y3	Z3	X4	Y4	Z4
PL1	50	14 9	2000	1.250	0.500	-19.2	7.60	0.00	-5.50	7.60	0.00	-5.50	16.20	0.00	-19.2	16.20	0.00

MESH BİLGİLERİ

Mesh no	d cm	I	J	K	L	Mesh no	d cm	I	J	K	L	Mesh no	d cm	I	J	K	L
1	50	2	3	8	6	2	50	3	9	14	8	3	50	15	21	18	12
4	50	21	28	25	18	5	50	39	36	28	6	50	46	56	45	35	
7	50	56	69	57	45	8	50	70	83	68	57	9	50	83	97	82	68
10	50	97	98	82		11	50	113	128	112	96	12	50	128	142	129	112
13	50	143	158	144	130	14	50	4	6	11	10	15	50	6	8	13	11
16	50	8	12	19	13	17	50	12	18	24	19	18	50	18	25	33	24
19	50	25	35	43	33	20	50	35	45	53	43	21	50	45	55	66	53
22	50	55	68	80	66	23	50	68	82	94	80	24	50	82	96	109	94
25	50	96	112	125	109	26	50	112	130	141	125	27	50	130	145	156	141
28	50	10	11	17	16	29	50	11	13	20	17	30	50	13	19	26	20
31	50	19	24	34	26	32	50	24	33	42	34	33	50	33	43	51	42
34	50	43	53	64	51	35	50	53	66	78	64	36	50	66	80	92	78
37	50	80	94	106	92	38	50	110	108	94	39	50	109	125	140	124	
40	50	125	141	155	140	41	50	141	157	171	155	42	50	16	17	23	22
43	50	17	20	27	23	44	50	20	26	37	27	45	50	26	34	44	37
46	50	34	42	52	44	47	50	42	51	63	52	48	50	51	64	77	63
49	50	64	78	91	77	50	50	78	92	105	91	51	50	92	106	120	105
52	50	106	121	137	120	53	50	124	140	154	139	54	50	140	155	170	154
55	50	155	172	182	170	56	50	22	23	32	30	57	50	23	27	38	32
58	50	27	37	47	38	59	50	37	44	54	47	60	50	44	52	65	54
61	50	52	63	76	65	62	50	63	77	90	76	63	50	77	91	104	90
64	50	91	105	119	104	65	50	105	120	136	119	66	50	120	137	152	136
67	50	139	154	169	153	68	50	154	170	181	169	69	50	170	182	188	181
70	50	30	32	41	40	71	50	32	38	48	41	72	50	38	47	59	48
73	50	47	54	67	59	74	50	54	65	79	67	75	50	65	76	89	79
76	50	76	90	103	89	77	50	90	104	118	103	78	50	104	119	135	118
79	50	119	136	151	135	80	50	152	153	168	166	81	50	153	169	179	168
82	50	169	181	186	179	83	50	181	188	192	186	84	50	40	41	50	49
85	50	41	48	60	50	86	50	48	59	71	60	87	50	59	67	81	71
88	50	67	79	93	81	89	50	79	89	102	93	90	50	89	103	116	102
91	50	103	118	133	116	92	50	118	135	149	133	93	50	135	151	165	149
94	50	151	166	178	165	95	50	168	179	185	180	96	50	179	186	190	185
97	50	186	192	195	190	98	50	49	50	62	61	99	50	50	60	72	62
100	50	60	71	85	72	101	50	71	81	95	85	102	50	81	93	107	95
103	50	93	102	117	107	104	50	102	116	132	117	105	50	116	133	147	132
106	50	133	149	162	147	107	50	149	165	175	162	108	50	165	178	184	175
109	50	180	185	191	187	110	50	185	190	196	191	111	50	190	195	199	196
112	50	74	73	61	113	50	62	72	86	75	114	50	72	87	101	86	
115	50	85	95	111	100	116	50	95	107	122	111	117	50	107	123	122	
118	50	117	132	146	134	119	50	132	148	161	146	120	50	147	162	163	148
121	50	162	174	177	163	122	50	175	184	183	174	123	50	187	191	194	189
124	50	191	196	198	194	125	50	200	199	201	126	50	126	109	124	121	
127	50	121	124	139	137	128	50	137	139	153	152	129	50	166	168	180	178
130	50	178	180	187	184	131	50	184	187	189	183	132	50	114	113	96	99
133	50	1	2	6	5	134	50	5	6	4	135	50	1	5	4		
136	50	12	14	15		137	50	14	12	8	138	50	14	9	15		
139	50	39	46	35	36	140	50	36	35	25	141	50	36	25	28		
142	50	55	57	68		143	50	57	55	45	144	50	57	69	70		
145	50	98	99	82		146	50	114	99	98	147	50	130	129	143		
148	50	129	130	112		149	50	129	142	143	150	50	144	145	130		
151	50	158	145	144		152	50	110	126	121	108	153	50	108	121	106	
154	50	108	106	94		155	50	157	156	172	171	156	50	171	172	155	
157	50	136	152	166	151	158	50	74	62	75	73	159	50	61	62	74	
160	50	101	87	100		161	50	72	85	87	162	50	87	85	100		
163	50	123	117	134	138	164	50	107	117	123	165	50	123	138	122		
166	50	161	148	164		167	50	132	147	148	168	50	148	163	164		
169	50	174	183	177		170	50	175	174	162	171	50	200	201	198		
172	50	196	200	198		173	50	97	114	98	174	50	200	196	199		

FİRMA : ESPO MUH. DAN. INS. LTD. STI.

30-09-2025

SAYFA: 61

PROJE : CERRAHPAŞA YURT SU DEPOSU

(250929-ES374-CERRAH-SU-D-D04.ST4)

RADYE NOKTA YÜKLERİ (t) - (m)

Nokta no	1 g	2 q	3 q	4 q	5 q	6 q	7 q	8 s	9 e	10 e	11 e	12 e	13 w	14 w	17 Ez
5 Pz	8.66	0.51	-0.19	0.51	0.51	-0.35	0.51	-1.59	-3.92	4.23	-4.39	5.25	-0.07	-0.12	7.19
5 Mx	-0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.14	-0.33	0.37	0.00	-0.02	-0.01	0.00	-0.02
5 My	0.45	0.11	0.02	0.08	0.10	0.04	0.08	0.28	0.01	-0.19	-2.76	3.50	0.00	-0.08	0.37
7 Pz	1.86	-1.15	-0.68	-0.47	-0.57	-1.41	-0.32	-5.87	-19.97	21.86	-13.48	15.83	-0.38	-0.38	1.55
7 Mx	1.71	0.49	0.14	0.35	0.36	0.33	0.30	0.27	2.17	-3.01	-8.30	10.61	0.06	-0.23	1.42
7 My	1.50	0.36	0.16	0.20	0.30	0.24	0.18	0.16	0.00	0.00	0.00	0.00	0.00	-0.01	1.25
14 Pz	37.38	7.94	3.77	4.17	7.03	4.77	4.07	-1.67	-0.99	1.07	-0.86	1.14	-0.02	-0.02	31.02
14 Mx	-0.17	-0.04	-0.01	-0.03	-0.02	-0.02	-0.03	1.17	-3.24	3.70	-0.08	-0.09	-0.06	0.00	-0.14
14 My	2.89	0.70	0.33	0.37	0.59	0.46	0.35	0.26	0.01	-0.02	-0.49	0.59	0.00	-0.01	2.40
29 Pz	-4.25	-2.29	-0.90	-1.39	-1.44	-2.01	-1.13	-5.66	-25.31	28.80	-0.41	-0.94	-0.52	-0.02	-3.53
29 Mx	-0.48	-0.14	-0.06	-0.09	-0.09	-0.13	-0.07	3.02	-7.49	8.57	-0.66	0.32	-0.15	-0.02	-0.40
29 My	2.96	0.71	0.30	0.41	0.50	0.57	0.35	0.28	0.00	0.00	0.00	0.00	0.00	-0.01	2.46
31 Pz	25.27	2.92	0.11	2.82	2.92	0.02	2.82	-1.00	-6.29	6.32	-0.01	-0.01	-0.11	0.00	20.97
31 Mx	1.02	0.26	0.06	0.19	0.25	0.08	0.19	0.79	0.00	0.00	0.00	0.00	-0.02	0.00	0.85
31 My	0.50	0.05	0.08	-0.03	-0.02	0.05	0.08	0.12	2.25	4.77	132.45	-166.7	-0.11	3.67	0.41
36 Pz	43.32	9.52	3.96	5.56	5.61	8.67	4.75	-1.23	0.03	-0.03	0.31	-0.34	0.00	0.01	35.95
36 Mx	0.03	0.00	-0.01	0.01	0.00	0.00	0.00	0.95	-3.33	3.79	-0.02	-0.15	-0.07	0.00	0.02
36 My	3.56	0.85	0.35	0.51	0.51	0.77	0.43	0.29	0.00	-0.01	-0.59	0.65	0.00	-0.02	2.95
57 Pz	33.64	7.21	0.83	6.38	3.73	7.14	3.54	-0.93	0.15	-0.15	-0.36	0.23	0.00	-0.01	27.92
57 Mx	0.16	0.03	0.00	0.03	0.03	0.02	0.01	0.76	-3.36	3.82	0.08	-0.26	-0.07	0.00	0.13
57 My	2.64	0.63	0.10	0.54	0.34	0.61	0.32	0.24	-0.01	0.01	-0.55	0.56	0.00	-0.01	2.19
58 Pz	-2.67	-1.76	-0.69	-1.06	-1.10	-1.48	-0.94	-3.76	-22.96	26.12	0.57	-2.05	-0.49	0.01	-2.22
58 Mx	-0.62	-0.21	-0.10	-0.12	-0.14	-0.19	-0.10	2.42	-8.56	9.77	0.02	-0.49	-0.17	0.00	-0.51
58 My	2.65	0.64	0.19	0.45	0.36	0.59	0.32	0.26	0.00	0.00	0.00	0.00	0.00	-0.01	2.20
74 Pz	8.60	0.50	-0.19	0.50	0.50	-0.36	0.50	-1.55	-4.14	3.89	4.39	-5.28	-0.07	0.12	7.14
74 Mx	-0.02	0.00	0.00	0.00	0.00	0.00	0.00	0.13	-0.36	0.32	0.00	0.02	-0.01	0.00	-0.02
74 My	-0.48	-0.11	-0.03	-0.08	-0.10	-0.04	-0.08	-0.29	-0.12	-0.05	-2.77	3.50	0.00	-0.08	-0.39
84 Pz	2.77	-0.45	-0.03	-0.42	-0.37	-0.30	-0.24	-1.41	-5.14	6.01	-8.37	7.25	-0.12	-0.24	2.30
84 Mx	-1.23	-0.26	-0.21	-0.06	-0.06	-0.29	-0.18	2.91	-19.58	22.14	7.45	-8.10	-0.42	0.20	-1.02
84 My	1.11	0.27	0.04	0.22	0.14	0.26	0.13	0.16	0.00	0.00	0.00	0.00	0.00	-0.02	0.93
87 Pz	37.15	7.90	3.74	4.17	7.02	4.74	4.04	-1.64	-1.07	1.00	0.80	-1.09	-0.02	0.02	30.83
87 Mx	-0.19	-0.04	-0.01	-0.03	-0.03	-0.03	-0.03	1.13	-3.59	3.17	0.09	0.06	-0.05	0.00	-0.16
87 My	-2.89	-0.70	-0.33	-0.37	-0.59	-0.46	-0.35	-0.26	-0.02	0.01	-0.49	0.59	0.00	-0.01	-2.40
88 Pz	1.72	-1.18	-0.70	-0.48	-0.58	-1.44	-0.34	-5.61	-21.46	19.80	13.49	-15.97	-0.34	0.38	1.42
88 Mx	1.82	0.51	0.16	0.35	0.36	0.34	0.31	0.35	2.75	-1.93	8.30	-10.59	0.03	0.23	1.51
88 My	-1.50	-0.36	-0.16	-0.20	-0.30	-0.24	-0.18	-0.17	0.00	0.00	0.00	0.00	0.00	-0.01	-1.25
98 Pz	3.12	-0.17	-0.08	-0.09	-0.05	-0.08	-0.21	0.30	0.47	-0.49	-1.86	1.67	0.01	-0.05	2.59
98 Mx	0.13	0.02	0.00	0.02	0.02	0.02	0.01	0.59	-3.34	3.79	0.14	-0.33	-0.07	0.00	0.11
98 My	0.07	0.02	0.01	0.01	0.01	0.02	0.01	0.06	0.00	0.01	-0.40	0.37	0.00	-0.01	0.05
99 Pz	7.12	0.84	0.38	0.47	0.44	0.84	0.36	0.09	0.46	-0.49	-1.45	1.31	0.01	-0.04	5.91
99 Mx	-0.01	0.00	0.03	-0.04	-0.03	0.00	0.02	0.08	0.00	0.00	0.00	0.00	-0.01	0.00	-0.01
99 My	-1.48	-0.37	-0.15	-0.22	-0.18	-0.36	-0.20	-1.59	-0.11	-0.08	12.30	-11.28	0.00	0.34	-1.23
108 Pz	15.67	2.74	0.26	2.47	2.06	2.74	0.67	0.58	0.44	-0.48	-1.29	1.16	0.00	-0.04	13.01
108 Mx	-0.03	-0.01	0.07	-0.08	-0.06	-0.01	0.05	0.12	-0.46	0.49	0.01	-0.02	-0.01	0.00	-0.02
108 My	0.47	0.11	0.05	0.06	0.05	0.11	0.06	0.38	-0.02	0.06	-3.68	3.38	0.00	-0.10	0.39
123 Pz	43.23	9.49	3.92	5.57	5.62	8.65	4.72	-1.19	-0.12	0.10	-0.36	0.38	0.00	-0.01	35.88
123 Mx	0.02	0.00	-0.01	0.01	0.00	0.00	0.00	0.90	-3.66	3.24	0.04	0.11	-0.06	0.00	0.02
123 My	-3.56	-0.85	-0.35	-0.51	-0.51	-0.77	-0.43	-0.29	0.00	0.00	-0.59	0.65	0.00	-0.02	-2.95
127 Pz	-4.27	-2.31	-0.92	-1.38	-1.44	-2.02	-1.15	-5.22	-27.95	24.75	0.50	0.70	-0.43	0.02	-3.54
127 Mx	-0.69	-0.18	-0.08	-0.10	-0.10	-0.16	-0.10	2.94	-8.31	7.33	0.64	-0.35	-0.13	0.02	-0.57
127 My	-2.96	-0.71	-0.30	-0.41	-0.50	-0.57	-0.35	-0.28	0.00	0.00	0.00	0.00	0.00	-0.01	-2.46
129 Pz	5.83	0.40	0.27	0.14	0.21	0.40	0.19	-0.32	1.20	-1.29	-2.58	2.29	0.03	-0.08	4.84
129 Mx	0.07	0.01	0.00	0.01	0.01	0.00	0.01	0.48	-3.28	3.72	0.20	-0.39	-0.07	0.01	0.06
129 My	0.09	0.02	0.02	0.00	0.00	0.02	0.02	0.13	0.01	0.00	-0.30	0.25	0.00	-0.01	0.07
131 Pz	4.34	0.29	-0.06	0.29	0.29	0.29	-0.03	-1.37	-7.81	9.01	-6.72	5.51	-0.18	-0.19	3.60
131 Mx	0.48	0.09	0.03	0.05	0.05	0.09	0.05	0.65	-2.47	2.82	-1.30	1.03	-0.05	-0.04	0.40
131 My	0.06	0.01	0.01	0.01	0.01	0.01	0.01	0.06	0.00	0.00	0.00	0.00	0.00	-0.01	0.05
144 Pz	5.79	0.30	0.15	0.15	0.18	0.28	0.15	0.57	2.01	-2.14	-3.36	2.92	0.04	-0.10	4.80
144 Mx	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.06	-0.33	0.38	0.00	-0.02	-0.01	0.00	0.00
144 My	0.11	0.02	0.02	0.00	0.00	0.02	0.02	0.27	-0.03	0.19	-2.46	1.91	0.00	-0.08	0.09
148 Pz	34.70	7.36	0.92	6.43	3.77	7.29	3.65	-0.91	-0.18	0.14	0.60	-0.43	0.00	0.01	28.80
148 Mx	0.21	0.04	0.01	0.03	0.03	0.03	0.02	0.70	-3.65	3.24	-0.05	0.21	-0.06	0.00	0.17
148 My	-2.64	-0.63	-0.10	-0.54	-0.34	-0.61	-0.32	-0.24	0.01	-0.01	-0.55	0.56	0.00	-0.01	-2.19

RADYE NOKTA YÜKLERİ (t) - (m)

Nokta no	1 g	2 q	3 q	4 q	5 q	6 q	7 q	8 s	9 e	10 e	11 e	12 e	13 w	14 w	17 Ez
150 Pz	-1.38	-1.59	-0.55	-1.04	-1.08	-1.30	-0.79	-3.32	-25.29	22.38	-0.12	1.51	-0.39	0.00	-1.15
150 Mx	-0.97	-0.27	-0.15	-0.12	-0.14	-0.25	-0.15	2.29	-9.49	8.38	-0.08	0.49	-0.14	0.00	-0.80
150 My	-2.65	-0.64	-0.19	-0.45	-0.36	-0.59	-0.32	-0.26	0.00	0.00	0.00	0.00	0.00	-0.01	-2.20
159 Pz	3.41	0.02	-0.11	0.05	0.06	0.00	-0.11	0.18	-4.44	5.29	-4.75	3.51	-0.11	-0.15	2.83
159 Mx	0.03	-0.02	-0.04	0.02	0.01	-0.03	-0.02	0.96	-7.64	8.61	1.52	-1.76	-0.17	0.04	0.02
159 My	0.03	0.01	0.01	0.00	0.00	0.01	0.01	0.05	0.00	0.00	0.00	0.00	0.00	-0.01	0.02
160 Pz	4.53	0.29	0.20	0.09	0.11	0.27	0.20	0.56	1.27	-1.36	-1.78	1.57	0.03	-0.05	3.76
160 Mx	-0.09	-0.02	-0.03	0.00	0.00	-0.02	-0.02	-0.09	0.00	0.00	0.00	0.00	0.00	0.00	-0.07
160 My	0.31	-0.02	-0.04	0.02	0.03	-0.02	-0.05	-0.38	0.34	-0.76	5.31	-4.04	0.02	0.16	0.26
167 Pz	29.95	4.70	2.34	2.36	2.07	4.70	2.56	3.16	0.58	-0.88	20.63	-18.85	0.02	0.58	24.86
167 Mx	-0.24	-0.06	0.14	-0.20	-0.16	-0.06	0.10	0.27	0.00	0.00	0.00	0.00	-0.01	0.00	-0.20
167 My	6.08	1.17	0.86	0.32	0.26	1.15	0.93	4.22	-1.64	0.80	70.31	-64.23	-0.02	1.85	5.05
171 Pz	12.13	1.72	1.72	-0.06	0.00	1.71	1.72	-1.42	0.72	-0.72	-1.77	1.46	0.02	-0.05	10.07
171 Mx	-0.28	-0.07	-0.08	0.01	0.01	-0.07	-0.08	-0.24	-0.44	0.47	0.00	-0.01	-0.01	0.00	-0.23
171 My	0.11	0.02	0.03	0.00	0.00	0.02	0.03	0.13	-0.05	0.20	-2.41	1.86	0.00	-0.07	0.09
174 Pz	6.93	0.42	0.42	0.00	0.02	0.42	0.31	0.12	0.29	-0.31	2.88	-2.55	0.01	0.08	5.75
174 Mx	0.22	0.04	0.02	0.02	0.02	0.03	0.03	0.57	-3.56	3.15	-0.07	0.23	-0.05	0.00	0.18
174 My	-0.08	-0.02	-0.01	-0.01	-0.01	-0.02	-0.01	-0.05	0.01	-0.01	-0.39	0.36	0.00	-0.01	-0.07
176 Pz	5.20	-0.12	0.10	-0.37	-0.34	0.01	0.02	-0.32	-5.93	5.06	10.91	-9.56	-0.09	0.30	4.32
176 Mx	-0.52	-0.15	-0.12	-0.02	-0.02	-0.17	-0.10	3.35	-21.01	18.71	-8.73	9.13	-0.32	-0.23	-0.43
176 My	-1.12	-0.27	-0.04	-0.22	-0.14	-0.26	-0.13	-0.14	0.00	0.00	0.00	0.00	0.00	-0.02	-0.93
193 Pz	21.22	2.17	1.99	0.18	0.23	2.13	1.98	2.03	4.40	-5.05	13.99	-11.04	0.10	0.43	17.61
193 Mx	-0.48	-0.13	-0.14	0.01	0.01	-0.13	-0.14	-0.39	0.00	0.00	0.00	0.00	-0.01	0.00	-0.40
193 My	2.63	0.66	0.79	-0.13	-0.13	0.68	0.77	5.05	2.29	-5.08	56.10	-44.33	0.09	1.58	2.18
197 Pz	13.79	1.37	1.08	0.29	0.32	1.37	1.03	0.22	1.81	-2.39	20.74	-17.74	0.04	0.58	11.45
197 Mx	0.90	0.19	-0.05	0.23	0.17	0.18	0.02	1.51	-22.61	20.52	0.14	-0.08	-0.36	-0.01	0.75
197 My	-0.13	-0.03	-0.02	-0.01	0.00	-0.03	-0.02	-0.08	0.00	0.00	0.00	0.00	0.00	-0.02	-0.11
200 Pz	11.94	1.25	1.12	0.13	0.16	1.23	1.11	-0.04	3.97	-3.74	5.06	-4.41	0.06	0.14	9.91
200 Mx	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.02	-0.37	0.33	-0.01	0.03	-0.01	0.00	0.00
200 My	-0.12	-0.03	-0.03	0.01	0.01	-0.03	-0.03	-0.27	0.06	0.09	-2.32	1.79	0.00	-0.07	-0.10

Tg= 416.69 (t) Tq= 58.85 (t) Radye temele etkiyen yükler
Tg= 416.69 (t) Tq= 58.85 (t) Tüm yapının temel yükü

NOKTALARIN X YÖNÜ STATİK SONUÇLARI Mx (tm)

Nokta no	1 Mg	2 Mq	3 Mq	4 Mq	5 Mq	6 Mq	7 Mq	8 Ms	9 Me	10 Me	11 Me	12 Me	13 Mw	14 Mw	17 Mez
1	-0.35	-0.04	0.00	-0.04	-0.04	-0.02	-0.01	0.11	0.33	-0.35	-0.31	0.57	0.01	-0.01	-0.30
2	0.43	0.09	0.05	0.05	0.07	0.06	0.06	-0.09	-0.22	0.26	-0.40	0.61	0.00	-0.01	0.34
3	1.33	0.24	0.09	0.15	0.19	0.16	0.13	-0.27	-0.69	0.75	-0.48	0.68	-0.01	-0.01	1.12
4	1.85	0.24	0.05	0.17	0.20	0.11	0.14	-0.48	-1.41	1.56	-1.44	1.59	-0.03	-0.04	1.44
5	1.42	0.18	0.04	0.13	0.16	0.08	0.11	-0.38	-1.11	1.24	-1.36	1.56	-0.02	-0.04	1.19
6	-0.02	0.00	-0.01	-0.03	-0.04	0.02	-0.03	0.06	0.09	-0.14	0.34	-0.22	0.00	0.01	0.06
7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
8	-0.72	-0.06	0.02	-0.07	-0.07	0.02	-0.04	0.23	0.67	-0.76	0.77	-0.66	0.01	0.02	-0.60
9	0.28	0.11	0.07	0.05	0.08	0.10	0.05	-0.04	-0.04	0.04	0.14	-0.02	0.00	0.00	0.21
10	6.28	0.83	0.15	0.58	0.69	0.40	0.45	-1.49	-4.47	4.81	-2.98	3.22	-0.09	-0.08	5.40
11	0.41	0.04	-0.02	-0.02	-0.03	0.05	-0.03	-0.01	-0.19	0.15	0.33	-0.25	0.00	0.01	0.50
12	-0.20	0.05	0.06	0.01	0.01	0.10	0.01	0.13	0.35	-0.42	0.86	-0.79	0.01	0.02	-0.18
13	-1.12	-0.11	0.00	-0.11	-0.14	0.01	-0.08	0.36	0.99	-1.09	0.92	-0.86	0.02	0.03	-0.93
14	2.36	0.40	0.13	0.25	0.31	0.27	0.20	-0.43	-1.27	1.38	-0.54	0.64	-0.02	-0.02	2.37
15	0.70	0.13	0.05	0.08	0.09	0.10	0.06	-0.13	-0.37	0.40	-0.06	0.11	-0.01	0.00	1.38
16	8.73	1.16	0.19	0.77	0.92	0.57	0.60	-1.95	-6.01	6.29	-2.35	2.55	-0.11	-0.07	7.60
17	1.06	0.11	-0.02	0.02	0.02	0.10	0.00	-0.13	-0.62	0.61	0.19	-0.13	-0.01	0.01	1.11
18	-0.16	0.07	0.05	0.02	0.02	0.11	0.02	0.09	0.23	-0.29	0.89	-0.83	0.01	0.02	-0.14
19	-1.28	-0.09	0.05	-0.08	-0.10	0.04	-0.05	0.38	1.11	-1.20	0.91	-0.87	0.02	0.03	-1.18
20	-1.49	-0.17	-0.01	-0.14	-0.19	0.00	-0.12	0.45	1.24	-1.32	0.74	-0.71	0.02	0.02	-1.26
21	2.43	0.44	0.14	0.27	0.30	0.35	0.21	-0.42	-1.39	1.50	-0.10	0.19	-0.03	0.00	2.08
22	9.92	1.32	0.22	0.85	1.03	0.65	0.68	-2.13	-6.72	6.85	-0.84	0.93	-0.12	-0.02	8.70
23	1.47	0.16	-0.02	0.05	0.05	0.13	0.02	-0.21	-0.88	0.89	0.15	-0.12	-0.02	0.00	1.49
24	-1.34	-0.08	0.06	-0.05	-0.07	0.04	-0.03	0.35	1.05	-1.14	0.93	-0.89	0.02	0.03	-1.26
25	-0.16	0.09	0.06	0.05	0.04	0.13	0.04	0.08	0.21	-0.27	0.97	-0.93	0.01	0.03	-0.17
26	-2.12	-0.19	0.05	-0.13	-0.17	0.00	-0.09	0.56	1.67	-1.75	0.74	-0.71	0.03	0.02	-1.96
27	-1.62	-0.19	-0.01	-0.15	-0.20	-0.01	-0.13	0.47	1.31	-1.34	0.33	-0.31	0.02	0.01	-1.37
28	0.83	0.16	0.05	0.10	0.10	0.13	0.07	-0.12	-0.43	0.47	0.02	0.00	-0.01	0.00	1.56
29	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
30	9.93	1.32	0.23	0.85	1.02	0.66	0.69	-2.08	-6.69	6.64	1.10	-1.18	-0.12	0.03	8.70
31	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
32	1.46	0.16	-0.02	0.05	0.05	0.12	0.02	-0.22	-0.88	0.89	0.13	-0.11	-0.02	0.00	1.48
33	-1.18	-0.04	0.06	-0.02	-0.04	0.05	-0.01	0.26	0.84	-0.91	0.87	-0.84	0.02	0.02	-1.13
34	-2.25	-0.18	0.06	-0.10	-0.14	-0.01	-0.07	0.52	1.64	-1.71	0.66	-0.64	0.03	0.02	-2.14
35	0.37	0.14	0.05	0.10	0.08	0.16	0.06	-0.03	-0.14	0.12	0.62	-0.62	0.00	0.02	-0.28
36	3.98	0.71	0.21	0.46	0.45	0.60	0.32	-0.53	-1.88	2.06	-0.40	0.36	-0.04	-0.01	3.40

NOKTALARIN X YÖNÜ STATİK SONUÇLARI Mx (tm)

Nokta no	1 Mg	2 Mq	3 Mq	4 Mq	5 Mq	6 Mq	7 Mq	8 Ms	9 Me	10 Me	11 Me	12 Me	13 Mw	14 Mw	17 Mez
37	-2.50	-0.24	0.04	-0.15	-0.21	-0.02	-0.11	0.63	1.91	-1.95	0.28	-0.26	0.03	0.01	-2.33
38	-1.63	-0.19	-0.02	-0.15	-0.20	-0.01	-0.14	0.46	1.30	-1.27	-0.17	0.19	0.02	0.00	-1.38
39	0.50	0.18	0.08	0.12	0.10	0.21	0.08	-0.06	-0.24	0.25	0.43	-0.43	0.00	0.01	0.37
40	8.73	1.18	0.23	0.76	0.91	0.59	0.64	-1.82	-5.94	5.72	2.54	-2.73	-0.10	0.07	7.59
41	1.03	0.11	-0.03	0.02	0.02	0.09	-0.01	-0.14	-0.62	0.65	0.05	-0.06	-0.01	0.00	1.09
42	-2.25	-0.18	0.05	-0.08	-0.11	-0.03	-0.06	0.43	1.45	-1.52	0.59	-0.58	0.03	0.02	-2.15
43	-1.28	-0.06	0.03	-0.01	-0.03	0.02	-0.02	0.21	0.73	-0.81	0.86	-0.85	0.01	0.02	-1.21
44	-2.74	-0.25	0.05	-0.13	-0.17	-0.04	-0.10	0.60	1.93	-1.96	0.19	-0.18	0.03	0.01	-2.60
45	-0.42	0.02	0.00	0.03	0.00	0.05	0.00	0.05	0.16	-0.23	0.79	-0.80	0.00	0.02	-0.33
46	2.46	0.47	0.13	0.31	0.28	0.43	0.20	-0.33	-1.19	1.29	0.12	-0.15	-0.02	0.00	2.10
47	-2.51	-0.25	0.03	-0.15	-0.20	-0.02	-0.12	0.62	1.89	-1.87	-0.27	0.28	0.03	-0.01	-2.34
48	-1.52	-0.18	-0.02	-0.14	-0.18	-0.01	-0.13	0.41	1.19	-1.12	-0.60	0.61	0.02	-0.02	-1.28
49	6.26	0.85	0.19	0.56	0.67	0.42	0.49	-1.32	-4.37	4.09	3.06	-3.30	-0.07	0.08	5.37
50	0.36	0.03	-0.03	-0.02	-0.03	0.04	-0.04	-0.03	-0.21	0.27	-0.15	0.11	-0.01	0.00	0.47
51	-2.26	-0.18	0.03	-0.06	-0.08	-0.07	-0.05	0.33	1.23	-1.30	0.52	-0.52	0.02	0.01	-2.15
52	-2.78	-0.24	0.04	-0.11	-0.14	-0.08	-0.08	0.50	1.73	-1.76	0.10	-0.10	0.03	0.00	-2.65
53	-1.32	-0.07	0.01	0.00	-0.03	-0.01	-0.02	0.15	0.61	-0.70	0.81	-0.82	0.01	0.02	-1.24
54	-2.75	-0.25	0.05	-0.13	-0.17	-0.05	-0.10	0.58	1.90	-1.88	-0.35	0.35	0.03	-0.01	-2.61
55	0.63	0.19	0.04	0.17	0.11	0.20	0.08	-0.06	-0.21	0.19	0.45	-0.50	0.00	0.01	0.50
56	2.16	0.41	0.10	0.29	0.23	0.39	0.17	-0.25	-1.05	1.15	0.08	-0.15	-0.02	0.00	1.84
57	2.16	0.39	0.09	0.28	0.21	0.37	0.17	-0.18	-0.73	0.82	-0.26	0.18	-0.02	-0.01	2.50
58	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
59	-2.14	-0.20	0.03	-0.12	-0.16	-0.01	-0.11	0.51	1.60	-1.54	-0.73	0.73	0.03	-0.02	-1.99
60	-1.15	-0.13	-0.02	-0.10	-0.13	0.00	-0.11	0.30	0.90	-0.81	-0.81	0.79	0.01	-0.02	-0.96
61	1.81	0.24	0.06	0.17	0.20	0.12	0.15	-0.41	-1.37	1.24	1.45	-1.59	-0.02	0.04	1.38
62	-0.06	-0.01	-0.02	-0.02	-0.03	0.01	-0.04	0.02	0.01	0.04	-0.26	0.15	0.00	-0.01	0.02
63	-2.76	-0.24	0.02	-0.09	-0.11	-0.11	-0.08	0.38	1.46	-1.50	0.00	-0.02	0.03	0.00	-2.64
64	-2.15	-0.16	0.01	-0.04	-0.05	-0.09	-0.05	0.23	0.97	-1.05	0.45	-0.47	0.02	0.01	-2.05
65	-2.79	-0.25	0.04	-0.10	-0.14	-0.08	-0.09	0.48	1.70	-1.68	-0.45	0.44	0.03	-0.01	-2.67
66	-0.94	-0.02	0.00	0.04	0.02	0.01	-0.01	0.05	0.31	-0.39	0.61	-0.66	0.01	0.02	-0.90
67	-2.28	-0.19	0.04	-0.09	-0.13	-0.02	-0.09	0.47	1.56	-1.50	-0.81	0.80	0.03	-0.02	-2.16
68	-0.22	0.02	-0.03	0.05	0.02	0.03	-0.01	-0.01	-0.02	-0.03	0.39	-0.47	0.00	0.01	-0.65
69	0.32	0.13	0.02	0.13	0.07	0.16	0.05	-0.04	-0.14	0.14	0.22	-0.29	0.00	0.01	0.23
70	0.11	0.05	0.01	0.05	0.03	0.06	0.02	-0.02	-0.04	0.03	0.06	-0.09	0.00	0.00	0.18
71	-1.31	-0.10	0.02	-0.06	-0.08	0.03	-0.07	0.31	0.99	-0.91	-0.91	0.88	0.02	-0.03	-1.21
72	-0.75	-0.07	-0.01	-0.05	-0.06	0.01	-0.07	0.16	0.54	-0.45	-0.74	0.64	0.01	-0.02	-0.63
73	-0.40	-0.05	-0.02	-0.02	-0.03	-0.03	-0.04	0.07	0.20	-0.18	0.29	-0.56	0.00	0.01	-0.36
74	1.37	0.18	0.05	0.13	0.15	0.09	0.12	-0.32	-1.09	0.98	1.36	-1.55	-0.02	0.04	1.14
75	0.39	0.08	0.03	0.07	0.09	0.05	0.04	-0.12	-0.37	0.34	0.34	-0.57	-0.01	0.01	0.29
76	-2.78	-0.24	0.02	-0.08	-0.10	-0.11	-0.09	0.36	1.43	-1.42	-0.56	0.53	0.03	-0.02	-2.65
77	-2.60	-0.22	0.00	-0.05	-0.07	-0.13	-0.07	0.25	1.13	-1.17	-0.10	0.05	0.02	0.00	-2.48
78	-1.68	-0.11	-0.01	0.01	0.00	-0.07	-0.03	0.09	0.54	-0.62	0.31	-0.39	0.01	0.01	-1.62
79	-2.28	-0.18	0.03	-0.07	-0.10	-0.04	-0.08	0.38	1.36	-1.31	-0.89	0.87	0.02	-0.02	-2.18
80	-0.49	0.01	-0.03	0.08	0.05	0.02	-0.02	-0.05	-0.10	0.01	0.30	-0.46	0.00	0.01	-0.47
81	-1.38	-0.09	0.03	-0.04	-0.06	0.03	-0.06	0.28	0.92	-0.85	-1.04	1.01	0.01	-0.03	-1.30
82	0.23	0.07	-0.01	0.09	0.07	0.08	0.00	-0.05	-0.24	0.24	-0.34	0.16	0.00	-0.01	0.11
83	0.92	0.20	0.04	0.16	0.11	0.21	0.08	-0.05	-0.31	0.35	-0.06	-0.03	-0.01	0.00	0.75
84	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
85	-0.20	0.05	0.04	0.03	0.04	0.09	-0.01	0.06	0.19	-0.13	-0.86	0.80	0.00	-0.02	-0.20
86	1.30	0.24	0.08	0.16	0.20	0.15	0.12	-0.27	-0.84	0.79	0.43	-0.64	-0.01	0.01	1.08
87	2.78	0.50	0.16	0.32	0.40	0.33	0.25	-0.49	-1.62	1.49	0.74	-0.97	-0.03	0.02	2.32
88	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
89	-2.30	-0.19	0.01	-0.05	-0.07	-0.07	-0.07	0.28	1.14	-1.09	-1.00	0.97	0.02	-0.03	-2.20
90	-2.62	-0.22	-0.01	-0.05	-0.06	-0.13	-0.08	0.23	1.10	-1.08	-0.67	0.61	0.02	-0.02	-2.51
91	-1.97	-0.14	-0.01	0.01	0.00	-0.09	-0.05	0.09	0.60	-0.64	-0.20	0.10	0.01	-0.01	-1.91
92	-0.36	0.05	-0.01	0.12	0.10	0.05	0.01	-0.10	-0.24	0.18	-0.02	-0.18	0.00	0.00	-0.42
93	-1.21	-0.05	0.03	0.01	-0.02	0.05	-0.03	0.20	0.69	-0.63	-1.08	1.04	0.01	-0.03	-1.17
94	1.26	0.20	0.00	0.19	0.15	0.19	0.04	-0.19	-0.80	0.84	-0.77	0.47	-0.02	-0.02	1.24
95	-0.22	0.05	0.02	0.04	0.03	0.09	-0.01	0.03	0.07	-0.02	-0.98	0.92	0.00	-0.03	-0.20
96	-0.18	0.08	-0.02	0.13	0.08	0.12	-0.01	0.07	0.08	-0.10	0.54	-0.47	0.00	0.02	-0.21
97	0.34	0.12	0.01	0.14	0.09	0.15	0.03	0.01	-0.15	0.17	-0.04	-0.10	0.00	0.00	0.23
98	0.70	0.16	0.01	0.17	0.12	0.18	0.04	-0.07	-0.38	0.42	-0.35	0.20	-0.01	-0.01	0.49
99	0.93	0.23	0.04	0.28	0.22	0.28	0.06	0.03	-0.18	0.28	-1.55	1.05	-0.01	-0.04	0.57
100	1.51	0.28	0.09	0.18	0.21	0.20	0.12	-0.27	-0.93	0.87	0.16	-0.25	-0.02	0.00	1.34
101	0.14	0.06	0.03	0.04	0.05	0.06	0.02	-0.04	-0.11	0.11	-0.13	0.06	0.00	0.00	0.16
102	-1.31	-0.07	0.01	0.01	-0.01	0.01	-0.04	0.14	0.59	-0.52	-1.19	1.16	0.01	-0.03	-1.26
103	-2.22	-0.18	-0.02	-0.02	-0.04	-0.10	-0.07	0.18	0.88	-0.82	-1.11	1.05	0.01	-0.03	-2.12
104	-1.98	-0.14	-0.02	0.01	0.00	-0.10	-0.05	0.07	0.57	-0.56	-0.73	0.62	0.01	-0.02	-1.92
105	-0.19	0.07	0.00	0.14	0.12	0.07	0.02	-0.15	-0.37	0.35	-0.35	0.15	-0.01	-0.01	-0.29
106	2.43	0.36	0.00	0.30	0.25	0.31	0.09	-0.39	-1.57	1.61	-1.10	0.65	-0.03	-0.03	2.56
107	-0.17	0.08	0.04	0.08	0.07	0.13	0.01	0.00	0.00	0.05	-1.11	1.05	0.00	-0.03	-0.20
108	4.79	0.65	0.03	0.53	0.44	0.59	0.17	-0.62	-2.70	2.90	-3.08	2.12	-0.05	-0.09	4.14
109	0.58	0.17	0.04	0.16	0.11	0.20	0.06	0.07	0.04	-0.01	0.89	-0.55	0.00	0.03	0.43
110	2.24	0.32	0.01	0.32	0.27	0.31	0.07	-0.31	-1.38	1.51	-2.57	1.72	-0.03	-0.07	1.84
111	2.42	0.44	0.13	0.29	0.32	0.35	0.20	-0.43	-1.59	1.49	0.12	-0.23	-0.03	0.00	2.05
112	-1.16	-0.10	-0.08	0.00	-0.01	-0.08	-0.08	-0.01	0.14	-0.24	0.53	-0.55	0.00	0.01	-1.00
113	-0.33	0.09	-0.03	0.21	0.13	0.17	-0.02	0.03	-0.15	0.14	-0.23	-0.07	0.00	-0.01	-0.43
114	-0.40	0.02	-0.03	0.09	0.05	0.06	-0.03	0.06	0.06	-0.09	-0.08	-0.15	0.00	0.00	-0.42
115	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
116	-1.41	-0.08	-0.02	0.02	-0.01	-0.02	-0.05	0.09	0.49	-0.41	-1.28	1.23	0.01	-0.04	-1.33
117	-0.29	0.06	0.01	0.08	0.04	0.11	0.00	0.01	0.04	0.01	-1.17	1.16	0.00	-0.03	-0.

FİRMA : ESPO MUH. DAN. INS. LTD. STI.

30-09-2025

SAYFA: 64

PROJE : CERRAHPAŞA YURT SU DEPOSU

(250929-ES374-CERRAH-SU-D-D04.ST4)

NOKTALARIN X YÖNÜ STATİK SONUÇLARI Mx (tm)

Nokta no	1 Mg	2 Mq	3 Mq	4 Mq	5 Mq	6 Mq	7 Mq	8 Ms	9 Me	10 Me	11 Me	12 Me	13 Mw	14 Mw	17 Mez
120	3.59	0.51	0.03	0.38	0.32	0.43	0.16	-0.52	-2.12	2.14	-0.53	0.21	-0.04	-0.02	3.18
121	3.99	0.55	0.10	0.36	0.28	0.53	0.19	-0.24	-1.48	1.63	-0.34	0.36	-0.03	-0.01	3.49
122	0.83	0.16	0.05	0.10	0.10	0.13	0.07	-0.12	-0.50	0.47	0.00	-0.02	-0.01	0.00	1.52
123	4.02	0.72	0.22	0.46	0.45	0.62	0.34	-0.47	-1.98	1.82	0.65	-0.59	-0.03	0.02	3.42
124	1.09	0.24	0.09	0.19	0.12	0.28	0.11	0.13	0.09	-0.04	1.15	-0.68	0.00	0.03	0.84
125	-1.60	-0.14	-0.09	-0.03	-0.03	-0.14	-0.10	-0.01	0.22	-0.33	0.69	-0.63	0.01	0.02	-1.37
126	1.89	0.32	0.14	0.19	0.13	0.35	0.16	0.12	0.03	0.12	0.83	-0.28	0.00	0.02	1.56
127	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
128	0.03	0.07	-0.02	0.14	0.09	0.12	-0.02	-0.01	-0.07	0.06	-0.53	0.25	0.00	-0.02	-0.08
129	0.30	0.06	0.00	0.09	0.06	0.09	0.00	0.01	-0.06	0.08	-0.56	0.34	0.00	-0.02	0.18
130	-0.88	-0.11	-0.06	-0.04	-0.02	-0.12	-0.07	-0.05	0.01	-0.10	-0.05	-0.12	0.00	0.00	-0.74
131	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
132	-0.42	0.03	-0.02	0.08	0.04	0.08	-0.02	-0.02	-0.01	0.07	-1.20	1.18	0.00	-0.03	-0.40
133	-1.10	-0.05	-0.04	0.05	0.02	-0.01	-0.04	0.00	0.23	-0.16	-1.21	1.15	0.00	-0.03	-1.05
134	2.50	0.48	0.13	0.33	0.29	0.44	0.20	-0.31	-1.34	1.25	0.03	0.00	-0.02	0.00	2.12
135	-0.30	0.05	-0.02	0.12	0.10	0.05	0.00	-0.14	-0.31	0.35	-0.81	0.68	-0.01	-0.02	-0.36
136	3.68	0.52	0.05	0.36	0.31	0.44	0.18	-0.50	-2.08	2.05	0.09	-0.28	-0.04	0.00	3.27
137	5.63	0.75	0.13	0.45	0.35	0.70	0.27	-0.34	-2.10	2.18	0.49	-0.40	-0.04	0.01	5.01
138	0.44	0.17	0.07	0.14	0.12	0.20	0.06	-0.08	-0.34	0.33	-0.55	0.53	-0.01	-0.02	0.31
139	1.17	0.24	0.10	0.18	0.12	0.28	0.11	0.13	0.05	-0.02	1.07	-0.69	0.00	0.03	0.91
140	-1.79	-0.17	-0.10	-0.04	-0.03	-0.17	-0.10	-0.02	0.26	-0.34	0.47	-0.40	0.01	0.01	-1.55
141	-1.27	-0.18	-0.11	-0.09	-0.06	-0.20	-0.11	-0.10	-0.05	-0.03	-0.36	0.09	0.00	-0.01	-1.02
142	-0.06	0.03	-0.02	0.07	0.05	0.05	-0.02	-0.05	-0.09	0.07	-0.20	0.08	0.00	-0.01	-0.09
143	0.04	0.01	0.00	0.01	0.01	0.01	0.00	0.00	0.00	0.00	-0.14	0.09	0.00	0.00	0.03
144	0.94	0.09	0.05	0.03	0.03	0.09	0.05	-0.03	-0.15	0.23	-0.66	0.59	0.00	-0.02	0.49
145	0.44	-0.04	0.01	-0.07	-0.03	-0.07	0.00	-0.10	-0.33	0.40	-2.19	1.50	-0.01	-0.06	0.39
146	2.24	0.43	0.10	0.31	0.25	0.42	0.18	-0.23	-1.16	1.07	0.16	-0.06	-0.02	0.00	1.89
147	0.43	0.16	0.01	0.16	0.10	0.17	0.05	-0.07	-0.24	0.27	-0.62	0.65	0.00	-0.02	0.33
148	2.30	0.43	0.10	0.32	0.24	0.42	0.20	-0.19	-0.92	0.82	0.62	-0.52	-0.01	0.02	1.93
149	-0.50	0.00	-0.05	0.08	0.05	0.02	-0.03	-0.09	-0.15	0.23	-0.98	0.90	0.00	-0.03	-0.47
150	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
151	3.13	0.46	0.05	0.32	0.27	0.39	0.17	-0.40	-1.73	1.68	0.49	-0.59	-0.03	0.01	2.77
152	5.75	0.77	0.15	0.44	0.34	0.71	0.30	-0.30	-2.04	2.00	1.54	-1.37	-0.04	0.04	5.13
153	1.17	0.23	0.10	0.17	0.11	0.27	0.12	0.13	0.04	-0.04	1.09	-0.77	0.00	0.03	0.90
154	-1.75	-0.17	-0.10	-0.04	-0.03	-0.17	-0.10	-0.04	0.22	-0.25	0.04	0.00	0.01	0.00	-1.51
155	-1.12	-0.16	-0.10	-0.09	-0.06	-0.19	-0.10	-0.10	-0.07	0.02	-0.50	0.26	0.00	-0.01	-1.18
156	1.09	0.07	0.05	0.00	0.02	0.06	0.05	-0.07	-0.35	0.42	-1.63	1.17	-0.01	-0.05	0.92
157	1.16	0.07	0.05	0.01	0.02	0.06	0.05	-0.07	-0.41	0.49	-1.74	1.24	-0.01	-0.05	0.98
158	-0.60	-0.13	-0.05	-0.08	-0.04	-0.15	-0.07	-0.01	-0.09	0.07	-1.33	0.76	0.00	-0.04	-0.51
159	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
160	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
161	0.12	0.06	0.01	0.06	0.03	0.07	0.02	-0.01	-0.05	0.05	-0.13	0.16	0.00	0.00	0.16
162	-0.38	-0.01	-0.04	0.04	0.01	0.01	-0.03	-0.02	0.00	0.07	-0.72	0.72	0.00	-0.02	-0.30
163	0.63	0.17	0.04	0.15	0.09	0.20	0.07	0.00	-0.18	0.15	0.21	-0.07	0.00	0.01	0.48
164	0.09	0.05	0.01	0.05	0.03	0.06	0.02	-0.01	-0.02	0.02	-0.09	0.12	0.00	0.00	0.12
165	1.98	0.30	0.03	0.22	0.18	0.26	0.11	-0.26	-1.15	1.10	0.49	-0.52	-0.02	0.01	1.74
166	5.35	0.72	0.19	0.40	0.31	0.68	0.31	-0.20	-1.74	1.59	2.55	-2.29	-0.03	0.07	4.72
167	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
168	1.14	0.22	0.10	0.15	0.10	0.25	0.12	0.13	0.03	-0.06	1.13	-0.86	0.00	0.03	0.88
169	-1.78	-0.18	-0.10	-0.04	-0.03	-0.18	-0.11	-0.06	0.19	-0.17	-0.44	0.42	0.00	-0.01	-1.53
170	-1.66	-0.24	-0.15	-0.12	-0.09	-0.27	-0.15	-0.14	-0.06	0.03	-0.74	0.49	0.00	-0.02	-1.31
171	0.84	0.06	0.04	0.01	0.02	0.06	0.04	-0.04	-0.26	0.30	-0.88	0.61	-0.01	-0.02	1.71
172	1.91	0.17	0.10	0.06	0.05	0.18	0.11	-0.05	-0.52	0.60	-1.31	0.91	-0.01	-0.04	1.60
173	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
174	0.10	0.10	0.04	0.12	0.07	0.14	0.04	0.09	0.12	-0.13	0.52	-0.32	0.00	0.01	-0.02
175	0.72	0.14	0.01	0.12	0.09	0.14	0.04	-0.11	-0.52	0.50	0.25	-0.24	-0.01	0.01	0.61
176	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
177	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-0.43
178	4.33	0.61	0.22	0.34	0.27	0.59	0.31	-0.08	-1.22	1.00	2.95	-2.66	-0.02	0.08	3.71
179	-1.82	-0.19	-0.12	-0.05	-0.03	-0.20	-0.13	-0.07	0.17	-0.10	-0.91	0.83	0.00	-0.03	-1.56
180	0.88	0.17	0.08	0.12	0.08	0.20	0.09	0.11	0.04	-0.08	0.96	-0.76	0.00	0.03	0.68
181	-1.69	-0.24	-0.16	-0.12	-0.09	-0.26	-0.16	-0.15	-0.06	0.07	-0.95	0.72	0.00	-0.03	-1.34
182	3.27	0.33	0.19	0.11	0.09	0.33	0.21	-0.03	-0.71	0.76	-1.00	0.56	-0.01	-0.03	2.73
183	-0.23	0.00	0.00	0.01	0.00	0.02	0.00	0.06	0.21	-0.19	-0.04	0.13	0.00	0.00	-0.22
184	2.30	0.35	0.16	0.21	0.16	0.36	0.20	0.02	-0.50	0.34	2.06	-1.83</			

NOKTALARIN Y YÖNÜ STATİK SONUÇLARI My (tm)

Nokta no	1 Mg	2 Mq	3 Mq	4 Mq	5 Mq	6 Mq	7 Mq	8 Ms	9 Me	10 Me	11 Me	12 Me	13 Mw	14 Mw	17 Mez
1	-0.18	-0.02	0.00	-0.02	-0.02	-0.01	0.00	0.06	0.19	-0.21	-0.04	0.13	0.00	0.00	-0.16
2	2.06	0.35	0.12	0.24	0.31	0.18	0.22	-0.42	-1.11	1.24	-1.09	1.30	-0.02	-0.03	1.67
3	4.93	0.76	0.20	0.50	0.63	0.41	0.41	-0.99	-2.83	3.08	-1.85	2.07	-0.05	-0.05	4.19
4	0.52	0.07	0.01	0.05	0.06	0.03	0.04	-0.12	-0.36	0.39	-0.48	0.57	-0.01	-0.01	0.44
5	0.30	0.04	0.01	0.03	0.04	0.02	0.02	-0.08	-0.23	0.25	-0.26	0.29	0.00	-0.01	0.20
6	-0.03	0.00	-0.01	-0.03	-0.03	0.01	-0.02	0.09	0.20	-0.28	0.65	-0.62	0.01	0.02	0.04
7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
8	0.64	0.11	0.02	0.03	0.05	0.08	0.04	0.02	-0.07	-0.04	1.01	-0.98	0.00	0.03	0.65
9	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.05
10	1.46	0.19	0.03	0.13	0.16	0.09	0.11	-0.33	-1.00	1.07	-0.78	0.86	-0.02	-0.02	1.25
11	-0.48	-0.07	-0.02	-0.07	-0.08	-0.03	-0.05	0.17	0.43	-0.51	0.63	-0.61	0.01	0.02	-0.35
12	1.30	0.21	0.04	0.09	0.12	0.14	0.08	-0.08	-0.40	0.29	1.22	-1.20	0.00	0.03	1.26
13	-1.49	-0.19	-0.03	-0.15	-0.18	-0.08	-0.11	0.42	1.17	-1.36	1.48	-1.50	0.02	0.04	-1.24
14	2.44	0.38	0.10	0.24	0.30	0.23	0.19	-0.44	-1.30	1.41	-0.63	0.72	-0.03	-0.02	3.83
15	4.87	0.75	0.18	0.47	0.56	0.46	0.37	-0.87	-2.67	2.88	-1.14	1.27	-0.05	-0.03	4.23
16	2.05	0.27	0.04	0.18	0.22	0.13	0.14	-0.44	-1.36	1.42	-0.66	0.74	-0.03	-0.02	1.79
17	-0.41	-0.06	-0.02	-0.05	-0.07	-0.02	-0.04	0.14	0.35	-0.40	0.32	-0.30	0.01	0.01	-0.31
18	1.44	0.22	0.02	0.09	0.11	0.15	0.07	-0.09	-0.44	0.31	1.47	-1.44	0.00	0.04	1.43
19	-1.91	-0.24	-0.03	-0.18	-0.21	-0.11	-0.12	0.51	1.46	-1.70	1.88	-1.89	0.03	0.05	-1.62
20	-1.96	-0.25	-0.02	-0.16	-0.20	-0.11	-0.12	0.48	1.42	-1.55	0.99	-0.99	0.03	0.03	-1.74
21	8.57	1.30	0.30	0.81	0.92	0.86	0.62	-1.43	-4.63	4.99	-1.70	1.82	-0.09	-0.05	7.48
22	2.35	0.31	0.05	0.20	0.24	0.15	0.16	-0.48	-1.53	1.55	-0.31	0.37	-0.03	-0.01	2.07
23	-0.29	-0.04	-0.02	-0.04	-0.05	-0.02	-0.03	0.10	0.26	-0.28	0.09	-0.07	0.00	0.00	-0.22
24	-1.94	-0.23	-0.03	-0.17	-0.19	-0.12	-0.11	0.49	1.47	-1.72	1.99	-2.00	0.03	0.05	-1.67
25	1.63	0.26	0.04	0.12	0.13	0.19	0.10	-0.13	-0.56	0.47	1.13	-1.10	-0.01	0.03	1.78
26	-2.89	-0.35	-0.01	-0.21	-0.25	-0.17	-0.14	0.66	2.01	-2.19	1.31	-1.33	0.04	0.04	-2.63
27	-2.08	-0.26	-0.02	-0.16	-0.20	-0.12	-0.12	0.47	1.45	-1.50	0.31	-0.31	0.03	0.01	-1.88
28	5.71	0.88	0.20	0.54	0.57	0.63	0.40	-0.84	-2.86	3.08	-0.83	0.86	-0.06	-0.02	5.00
29	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
30	2.36	0.31	0.05	0.20	0.24	0.15	0.17	-0.47	-1.52	1.51	0.38	-0.43	-0.03	0.01	2.07
31	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
32	-0.29	-0.05	-0.02	-0.04	-0.05	-0.02	-0.03	0.10	0.26	-0.24	-0.05	0.04	0.00	0.00	-0.22
33	-2.13	-0.25	-0.04	-0.18	-0.19	-0.16	-0.12	0.48	1.49	-1.75	2.07	-2.07	0.03	0.06	-1.84
34	-3.40	-0.40	-0.01	-0.24	-0.27	-0.21	-0.15	0.71	2.27	-2.47	1.43	-1.45	0.04	0.04	-3.13
35	1.73	0.28	0.03	0.13	0.13	0.21	0.10	-0.11	-0.52	0.40	1.50	-1.47	-0.01	0.04	1.69
36	5.67	0.87	0.20	0.54	0.55	0.65	0.40	-0.77	-2.66	2.87	-0.69	0.70	-0.05	-0.02	5.00
37	-3.25	-0.39	-0.01	-0.22	-0.27	-0.19	-0.16	0.68	2.17	-2.25	0.40	-0.41	0.04	0.01	-3.00
38	-2.09	-0.26	-0.03	-0.16	-0.20	-0.12	-0.13	0.45	1.44	-1.40	-0.37	0.38	0.02	-0.01	-1.89
39	0.12	0.05	0.02	0.03	0.03	0.05	0.02	-0.02	-0.06	0.06	0.11	-0.11	0.00	0.00	0.09
40	2.05	0.28	0.05	0.18	0.21	0.13	0.15	-0.41	-1.34	1.30	0.71	-0.78	-0.02	0.02	1.79
41	-0.42	-0.07	-0.03	-0.05	-0.06	-0.03	-0.05	0.11	0.34	-0.28	-0.28	0.27	0.00	-0.01	-0.32
42	-3.64	-0.43	-0.01	-0.24	-0.27	-0.26	-0.16	0.69	2.30	-2.51	1.43	-1.45	0.05	0.04	-3.36
43	-2.13	-0.25	-0.04	-0.17	-0.18	-0.17	-0.11	0.42	1.39	-1.65	2.01	-2.00	0.03	0.06	-1.83
44	-3.95	-0.47	-0.01	-0.25	-0.29	-0.25	-0.18	0.76	2.53	-2.61	0.39	-0.42	0.05	0.01	-3.68
45	1.19	0.20	0.01	0.09	0.08	0.16	0.06	-0.03	-0.21	0.08	1.49	-1.46	0.00	0.04	1.20
46	4.15	0.63	0.14	0.39	0.38	0.49	0.28	-0.52	-1.89	2.05	-0.54	0.53	-0.04	-0.02	7.30
47	-3.26	-0.40	-0.02	-0.22	-0.26	-0.20	-0.17	0.64	2.15	-2.10	-0.60	0.59	0.04	-0.02	-3.01
48	-1.99	-0.26	-0.05	-0.16	-0.19	-0.12	-0.14	0.41	1.37	-1.25	-1.02	1.03	0.02	-0.03	-1.76
49	1.46	0.20	0.04	0.13	0.16	0.10	0.12	-0.29	-0.98	0.92	0.80	-0.88	-0.02	0.02	1.25
50	-0.50	-0.08	-0.04	-0.06	-0.08	-0.04	-0.07	0.13	0.39	-0.31	-0.57	0.57	0.00	-0.02	-0.37
51	-3.57	-0.41	-0.02	-0.22	-0.23	-0.27	-0.15	0.61	2.12	-2.33	1.33	-1.36	0.04	0.04	-3.30
52	-4.24	-0.50	-0.01	-0.26	-0.29	-0.30	-0.18	0.74	2.57	-2.66	0.34	-0.37	0.05	0.01	-3.97
53	-1.99	-0.23	-0.05	-0.14	-0.15	-0.17	-0.10	0.35	1.20	-1.45	1.81	-1.81	0.03	0.05	-1.72
54	-3.96	-0.48	-0.02	-0.25	-0.29	-0.26	-0.19	0.72	2.49	-2.43	-0.75	0.73	0.04	-0.02	-3.69
55	0.85	0.15	0.01	0.08	0.06	0.13	0.05	-0.01	-0.11	0.04	0.90	-0.89	0.00	0.02	0.89
56	7.43	1.12	0.24	0.71	0.65	0.93	0.50	-0.80	-3.12	3.43	-0.98	0.93	-0.06	-0.03	6.51
57	3.88	0.60	0.13	0.38	0.32	0.52	0.27	-0.32	-1.28	1.44	-0.43	0.43	-0.03	-0.01	3.40
58	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
59	-2.91	-0.36	-0.04	-0.20	-0.24	-0.18	-0.17	0.56	1.92	-1.77	-1.46	1.47	0.03	-0.04	-2.64
60	-1.51	-0.21	-0.07	-0.14	-0.17	-0.10	-0.14	0.32	1.08	-0.91	-1.46	1.48	0.02	-0.04	-1.25
61	0.50	0.07	0.02	0.05	0.06	0.03	0.04	-0.11	-0.36	0.33	0.48	-0.57	-0.01	0.01	0.43
62	-0.02	0.00	-0.02	-0.01	-0.01	0.01	-0.03	0.04	0.12	-0.04	-0.59	0.56	0.00	-0.02	0.05
63	-4.13	-0.48	-0.01	-0.24	-0.25	-0.31	-0.17	0.65	2.36	-2.45	0.25	-0.30	0.04	0.01	-3.88
64	-3.20	-0.36	-0.02	-0.18	-0.18	-0.25	-0.13	0.48	1.77	-1.96	1.14	-1.18	0.04	0.03	-2.97
65	-4.25	-0.51	-0.03	-0.25	-0.28	-0.30	-0.19	0.69	2.52	-2.46	-0.86	0.82			

NOKTALARIN Y YÖNÜ STATİK SONUÇLARI My (tm)

Nokta no	1 Mg	2 Mq	3 Mq	4 Mq	5 Mq	6 Mq	7 Mq	8 Ms	9 Me	10 Me	11 Me	12 Me	13 Mw	14 Mw	17 Mez
84	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
85	1.39	0.22	0.01	0.12	0.15	0.14	0.06	-0.19	-0.65	0.75	-1.11	1.07	-0.01	-0.03	1.32
86	4.96	0.77	0.21	0.51	0.63	0.42	0.42	-0.92	-3.01	2.78	1.78	-2.06	-0.05	0.05	4.21
87	4.33	0.66	0.16	0.41	0.50	0.39	0.33	-0.72	-2.47	2.31	1.14	-1.25	-0.04	0.03	3.85
88	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
89	-3.58	-0.43	-0.06	-0.21	-0.22	-0.29	-0.19	0.48	1.94	-1.76	-1.90	1.83	0.03	-0.05	-3.30
90	-3.62	-0.42	-0.03	-0.19	-0.19	-0.29	-0.15	0.46	1.87	-1.82	-0.91	0.82	0.03	-0.03	-3.42
91	-2.67	-0.29	-0.01	-0.12	-0.11	-0.21	-0.09	0.33	1.32	-1.39	0.02	-0.12	0.03	0.00	-2.55
92	-1.26	-0.11	-0.01	-0.02	-0.02	-0.08	-0.04	0.13	0.56	-0.66	0.27	-0.42	0.01	0.01	-1.21
93	-2.12	-0.28	-0.09	-0.15	-0.16	-0.18	-0.17	0.31	1.23	-1.00	-2.30	2.25	0.02	-0.06	-1.82
94	-1.08	-0.10	-0.05	-0.02	-0.02	-0.08	-0.07	0.09	0.45	-0.55	0.28	-0.43	0.01	0.01	-0.96
95	1.52	0.22	-0.01	0.12	0.14	0.15	0.04	-0.21	-0.73	0.85	-1.34	1.30	-0.02	-0.04	1.49
96	-0.99	-0.08	-0.04	-0.02	-0.03	-0.06	-0.06	0.15	0.67	-0.77	0.57	-0.59	0.01	0.02	-0.86
97	0.22	0.08	0.05	0.06	0.03	0.10	0.05	0.18	0.40	-0.39	0.09	-0.26	0.01	0.00	0.13
98	-0.03	0.03	0.02	0.03	0.01	0.05	0.02	0.11	0.29	-0.30	0.20	-0.25	0.01	0.00	0.17
99	-0.11	0.01	0.01	0.03	0.02	0.03	0.00	0.08	0.23	-0.24	0.02	-0.04	0.00	0.00	-0.47
100	4.92	0.76	0.19	0.47	0.56	0.47	0.38	-0.82	-2.84	2.66	1.27	-1.42	-0.05	0.04	4.26
101	0.06	0.02	0.01	0.02	0.02	0.02	0.01	-0.02	-0.04	0.04	-0.05	0.02	0.00	0.00	0.04
102	-2.10	-0.27	-0.10	-0.14	-0.15	-0.19	-0.16	0.25	1.09	-0.86	-2.32	2.25	0.01	-0.06	-1.81
103	-3.18	-0.38	-0.06	-0.17	-0.17	-0.27	-0.16	0.36	1.57	-1.41	-1.81	1.71	0.02	-0.05	-2.94
104	-2.65	-0.29	-0.02	-0.12	-0.11	-0.21	-0.10	0.29	1.26	-1.23	-0.79	0.69	0.02	-0.02	-2.53
105	-1.24	-0.11	0.00	-0.02	-0.02	-0.08	-0.03	0.12	0.53	-0.57	-0.11	0.00	0.01	0.00	-1.22
106	0.06	0.03	0.00	0.05	0.04	0.03	0.00	-0.03	-0.09	0.07	-0.11	0.00	0.00	0.00	0.20
107	2.01	0.31	0.01	0.18	0.19	0.22	0.09	-0.26	-0.95	1.06	-1.25	1.21	-0.02	-0.03	1.90
108	1.38	0.19	0.01	0.15	0.13	0.17	0.05	-0.15	-0.66	0.71	-0.88	0.61	-0.01	-0.02	1.51
109	-0.64	-0.04	-0.01	0.00	0.00	-0.03	-0.02	0.08	0.46	-0.51	0.47	-0.39	0.01	0.01	-0.58
110	0.32	0.06	0.00	0.08	0.07	0.06	0.00	-0.05	-0.22	0.24	-0.75	0.48	0.00	-0.02	0.22
111	8.72	1.33	0.32	0.82	0.92	0.89	0.65	-1.33	-4.91	4.58	2.15	-2.29	-0.08	0.06	7.59
112	-1.16	-0.12	-0.05	-0.06	-0.05	-0.12	-0.07	0.08	0.53	-0.65	0.68	-0.68	0.01	0.02	-0.98
113	0.04	0.07	0.01	0.13	0.08	0.12	0.01	0.09	0.11	-0.10	-0.71	0.32	0.00	-0.02	-0.10
114	-0.76	-0.05	-0.02	0.01	-0.01	-0.01	-0.04	0.18	0.48	-0.55	0.11	-0.42	0.01	0.00	-0.71
115	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
116	-1.95	-0.25	-0.10	-0.12	-0.12	-0.19	-0.15	0.17	0.89	-0.67	-2.22	2.13	0.01	-0.06	-1.68
117	1.93	0.29	0.00	0.18	0.17	0.22	0.08	-0.24	-0.91	1.01	-1.24	1.21	-0.02	-0.03	1.84
118	-2.42	-0.28	-0.05	-0.11	-0.11	-0.21	-0.12	0.22	1.08	-0.95	-1.53	1.42	0.02	-0.04	-2.26
119	-1.21	-0.11	0.00	-0.02	-0.02	-0.08	-0.04	0.10	0.50	-0.48	-0.51	0.42	0.01	-0.01	-1.19
120	0.53	0.09	0.01	0.08	0.07	0.08	0.03	-0.08	-0.32	0.31	-0.16	0.06	-0.01	0.00	0.44
121	0.58	0.09	0.02	0.06	0.05	0.09	0.03	-0.01	-0.14	0.17	-0.02	0.04	0.00	0.00	0.82
122	5.83	0.90	0.22	0.55	0.58	0.66	0.42	-0.78	-3.04	2.84	1.28	-1.29	-0.05	0.04	5.10
123	3.38	0.53	0.13	0.32	0.33	0.41	0.25	-0.40	-1.63	1.52	0.70	-0.67	-0.03	0.02	5.12
124	0.36	0.08	0.04	0.06	0.04	0.09	0.04	0.05	0.09	-0.07	0.30	-0.14	0.00	0.01	0.27
125	-1.13	-0.12	-0.05	-0.06	-0.05	-0.13	-0.06	0.03	0.40	-0.50	0.55	-0.51	0.01	0.02	-0.95
126	0.44	0.08	0.03	0.05	0.03	0.09	0.04	0.04	0.05	-0.02	0.24	-0.09	0.00	0.01	0.31
127	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
128	1.21	0.18	0.07	0.15	0.10	0.22	0.07	0.04	-0.03	0.10	-1.04	0.77	0.00	-0.03	0.92
129	0.79	0.11	0.05	0.07	0.05	0.12	0.05	0.02	0.01	0.04	-0.49	0.40	0.00	-0.01	0.78
130	-0.85	-0.10	-0.03	-0.06	-0.04	-0.11	-0.04	0.02	0.37	-0.47	0.25	-0.31	0.01	0.01	-0.72
131	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
132	1.37	0.21	-0.02	0.13	0.11	0.16	0.04	-0.16	-0.61	0.72	-1.22	1.21	-0.01	-0.03	1.35
133	-1.75	-0.23	-0.10	-0.10	-0.10	-0.19	-0.14	0.10	0.66	-0.47	-1.97	1.86	0.01	-0.05	-1.50
134	8.64	1.31	0.32	0.79	0.77	1.04	0.61	-0.95	-4.06	3.76	2.17	-2.06	-0.07	0.06	7.57
135	-1.15	-0.12	-0.02	-0.03	-0.02	-0.09	-0.05	0.07	0.44	-0.36	-0.92	0.84	0.01	-0.03	-1.10
136	0.61	0.10	0.01	0.08	0.07	0.09	0.04	-0.08	-0.34	0.33	-0.10	0.04	-0.01	0.00	0.52
137	1.28	0.18	0.03	0.11	0.09	0.17	0.06	-0.07	-0.44	0.45	0.06	-0.05	-0.01	0.00	1.13
138	0.06	0.02	0.01	0.02	0.01	0.03	0.01	-0.01	-0.04	0.04	-0.07	0.07	0.00	0.00	0.08
139	0.20	0.05	0.02	0.04	0.03	0.06	0.03	0.05	0.09	-0.08	0.22	-0.13	0.00	0.01	0.14
140	-0.65	-0.06	-0.02	-0.02	-0.01	-0.06	-0.03	0.01	0.21	-0.25	0.25	-0.20	0.00	0.01	-0.56
141	-0.85	-0.12	-0.05	-0.08	-0.06	-0.14	-0.06	-0.03	0.22	-0.30	0.00	-0.11	0.01	0.00	-0.69
142	0.33	0.04	0.01	0.00	0.00	0.03	0.02	-0.07	-0.15	0.16	0.13	0.01	0.00	0.00	0.51
143	0.81	0.10	0.05	0.05	0.04	0.11	0.06	0.03	0.04	0.01	-0.26	0.29	0.00	-0.01	0.66
144	-0.06	-0.02	0.00	-0.02	-0.01	-0.03	0.00	0.03	0.20	-0.21	-0.44	0.30	0.00	-0.01	-0.05
145	0.08	-0.01	0.01	-0.03	-0.02	-0.02	0.01	-0.02	0.12	-0.12	-0.48	0.36	0.00	-0.01	-0.05
146	7.96	1.21	0.30	0.73	0.66	1.01	0.57	-0.71	-3.42	3.13	2.38	-2.16	-0.05	0.07	6.96
147	0.93	0.14	-0.04	0.09	0.07	0.11	0.01	-0.12	-0.43	0.53	-1.09	1.08	-0.01	-0.03	0.95
148	3.44	0.53	0.14	0.32	0.27	0.46	0.25	-0.22	-1.20	1.					

NOKTALARIN Y YÖNÜ STATİK SONUÇLARI My (tm)

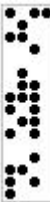
Nokta no	1 Mg	2 Mq	3 Mq	4 Mq	5 Mq	6 Mq	7 Mq	8 Ms	9 Me	10 Me	11 Me	12 Me	13 Mw	14 Mw	17 Mez
167	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
168	0.21	0.05	0.03	0.04	0.03	0.06	0.03	0.05	0.08	-0.08	0.26	-0.20	0.00	0.01	0.14
169	-0.53	-0.05	-0.03	-0.01	-0.01	-0.05	-0.03	-0.01	0.10	-0.10	-0.15	0.15	0.00	0.00	-0.47
170	-0.54	-0.07	-0.04	-0.04	-0.03	-0.08	-0.04	-0.04	0.04	-0.06	-0.14	0.10	0.00	0.00	-0.43
171	0.40	0.03	0.02	0.00	0.00	0.03	0.02	-0.03	-0.10	0.12	-0.48	0.34	0.00	-0.01	0.34
172	0.21	0.02	0.01	0.00	0.00	0.02	0.01	-0.01	-0.05	0.06	-0.19	0.14	0.00	-0.01	0.39
173	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
174	0.00	0.03	0.02	0.03	0.01	0.05	0.02	0.09	0.26	-0.25	0.11	0.03	0.00	0.00	0.25
175	0.04	0.01	-0.03	0.01	0.01	0.00	-0.02	-0.04	-0.11	0.14	-0.32	0.29	0.00	-0.01	0.08
176	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
177	-1.18	-0.11	0.01	-0.10	-0.11	-0.07	-0.01	0.40	1.45	-1.33	-0.79	1.25	0.02	-0.02	-1.01
178	1.00	0.15	0.05	0.08	0.06	0.14	0.07	0.00	-0.24	0.19	0.73	-0.66	0.00	0.02	0.85
179	-0.63	-0.06	-0.03	-0.01	-0.01	-0.07	-0.04	-0.02	0.10	-0.07	-0.38	0.34	0.00	-0.01	-0.55
180	0.07	0.03	0.02	0.02	0.02	0.03	0.02	0.04	0.07	-0.07	0.16	-0.12	0.00	0.00	0.03
181	-0.49	-0.07	-0.04	-0.03	-0.02	-0.07	-0.04	-0.04	0.03	-0.03	-0.25	0.20	0.00	-0.01	-0.39
182	0.78	0.08	0.05	0.02	0.02	0.08	0.05	-0.01	-0.14	0.15	-0.27	0.16	0.00	-0.01	0.65
183	-0.03	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.02	-0.02	-0.04	0.04	0.00	0.00	-0.43
184	0.51	0.08	0.04	0.05	0.04	0.08	0.05	0.02	-0.08	0.05	0.48	-0.42	0.00	0.01	0.41
185	-0.94	-0.12	-0.07	-0.04	-0.03	-0.12	-0.08	-0.04	0.11	-0.04	-0.79	0.71	0.00	-0.02	-0.79
186	-0.58	-0.08	-0.05	-0.04	-0.03	-0.08	-0.05	-0.04	0.04	-0.01	-0.40	0.34	0.00	-0.01	-0.47
187	-0.24	-0.03	-0.02	-0.01	-0.01	-0.03	-0.03	0.02	0.09	-0.06	-0.19	0.19	0.00	-0.01	-0.19
188	0.82	0.09	0.06	0.02	0.02	0.09	0.06	0.01	-0.10	0.09	0.03	-0.08	0.00	0.00	0.69
189	0.58	0.08	0.05	0.04	0.03	0.09	0.06	0.03	-0.03	-0.02	0.45	-0.41	0.00	0.01	0.46
190	-0.83	-0.11	-0.07	-0.05	-0.04	-0.12	-0.08	-0.06	0.05	0.01	-0.72	0.64	0.00	-0.02	-0.66
191	-1.01	-0.14	-0.10	-0.07	-0.06	-0.15	-0.11	-0.04	0.11	-0.02	-1.00	0.90	0.00	-0.03	-0.79
192	0.84	0.10	0.06	0.03	0.02	0.10	0.07	0.03	-0.07	0.04	0.42	-0.39	0.00	0.01	0.70
193	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
194	2.37	0.33	0.21	0.14	0.11	0.34	0.23	0.16	-0.08	-0.09	2.12	-1.85	0.00	0.06	1.90
195	0.76	0.09	0.06	0.03	0.02	0.10	0.07	0.04	-0.05	0.00	0.57	-0.51	0.00	0.02	0.63
196	-0.60	-0.09	-0.06	-0.04	-0.03	-0.09	-0.06	-0.04	0.03	0.02	-0.65	0.58	0.00	-0.02	-0.66
197	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
198	1.24	0.18	0.12	0.08	0.06	0.20	0.13	0.13	0.04	-0.13	1.36	-1.13	0.00	0.04	0.98
199	0.34	0.05	0.03	0.02	0.01	0.05	0.03	0.02	0.00	-0.02	0.36	-0.31	0.00	0.01	0.27
200	0.52	0.07	0.05	0.03	0.02	0.07	0.05	0.04	0.00	-0.03	0.48	-0.42	0.00	0.01	0.42
201	-0.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.02	-0.02	0.05	-0.02	0.00	0.00	-0.06

ANALİZ SONUÇLARI

Nokta no	dx cm	dy cm	X m	Y m	Z m	Mxalt (tm)	Mxust (tm)	Myalt (tm)	Myust (tm)	Asax cm ²	Asux cm ²	Asay cm ²	Asuy cm ²
1	50	50	-19.200	7.600	0.000	1.75	-0.72	0.63	-0.20	4.30	4.30	4.30	4.30
2	50	50	-18.221	7.600	0.000	1.05	-0.40	3.32	-0.28	4.30	4.30	4.30	4.30
3	50	50	-17.243	7.600	0.000	1.08	-0.45	3.56	-0.11	4.30	4.30	4.30	4.30
4	50	50	-19.200	8.556	0.000	6.26	-0.22	1.15	-0.15	5.22	4.30	4.30	4.30
5	50	50	-19.050	8.100	0.000	2.40	-0.54	0.63	-0.20	4.30	4.30	4.30	4.30
6	50	50	-18.221	8.556	0.000	1.26	-0.47	1.53	-0.50	4.30	4.30	4.30	4.30
7	500	500	-17.951	7.600	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
8	50	50	-17.243	8.556	0.000	1.30	-1.08	1.78	-1.08	4.30	4.30	4.30	4.30
9	50	50	-16.500	7.600	0.000	2.07	0.00	5.37	0.00	4.30	4.30	4.48	4.30
10	50	50	-19.200	9.511	0.000	8.14	-0.04	1.98	-0.34	6.82	4.30	4.30	4.30
11	50	50	-18.221	9.511	0.000	3.05	-0.55	0.85	-1.19	4.30	4.30	4.30	4.30
12	50	50	-16.114	8.556	0.000	1.42	-1.30	2.30	-1.13	4.30	4.30	4.30	4.30
13	50	50	-17.243	9.511	0.000	0.41	-1.90	0.59	-2.52	4.30	4.30	4.30	4.30
14	50	50	-16.500	7.750	0.000	1.86	-0.35	2.32	-0.02	4.30	4.30	4.30	4.30
15	50	50	-16.114	7.600	0.000	0.89	-0.35	3.75	-0.02	4.30	4.30	4.30	4.30
16	50	50	-19.200	10.467	0.000	11.99	0.00	2.70	-0.22	10.10	4.30	4.30	4.30
17	50	50	-18.221	10.467	0.000	4.31	-0.60	0.86	-1.29	4.30	4.30	4.30	4.30
18	50	50	-15.286	8.556	0.000	1.48	-1.15	4.85	-0.88	4.30	4.30	4.30	4.30
19	50	50	-16.264	9.511	0.000	0.40	-2.52	0.82	-3.37	4.30	4.30	4.30	4.30
20	50	50	-17.243	10.467	0.000	0.57	-2.51	0.11	-3.42	4.30	4.30	4.30	4.30
21	50	50	-15.286	7.600	0.000	2.00	-0.26	9.04	-0.04	4.30	4.30	7.58	4.30
22	50	50	-19.200	11.422	0.000	13.68	0.00	3.06	-0.15	11.55	4.30	4.30	4.30
23	50	50	-18.221	11.422	0.000	5.02	-0.63	0.89	-1.19	4.30	4.30	4.30	4.30
24	50	50	-15.286	9.511	0.000	0.31	-2.49	0.90	-3.82	4.30	4.30	4.30	4.30
25	50	50	-14.386	8.556	0.000	0.86	-1.07	4.05	-1.16	4.30	4.30	4.30	4.30
26	50	50	-16.264	10.467	0.000	0.21	-3.70	0.10	-5.07	4.30	4.30	4.30	4.30
27	50	50	-17.243	11.422	0.000	0.64	-2.80	0.03	-3.58	4.30	4.30	4.30	4.30
28	50	50	-14.386	7.600	0.000	2.28	-0.37	9.18	0.00	4.30	4.30	7.70	4.30
29	500	500	-15.250	7.600	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
30	50	50	-19.200	12.378	0.000	13.60	0.00	3.03	-0.15	11.47	4.30	4.30	4.30
31	500	500	-19.200	11.900	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
32	50	50	-18.221	12.378	0.000	4.97	-0.63	0.86	-1.17	4.30	4.30	4.30	4.30
33	50	50	-14.307	9.511	0.000	0.25	-2.39	0.84	-3.92	4.30	4.30	4.30	4.30
34	50	50	-15.286	10.467	0.000	0.10	-3.93	0.11	-5.89	4.30	4.30	4.30	4.92
35	50	50	-13.329	8.556	0.000	1.88	-0.97	3.81	-0.96	4.30	4.30	4.30	4.30
36	50	50	-14.000	7.750	0.000	2.59	-0.28	5.59	0.00	4.30	4.30	4.67	4.30
37	50	50	-16.264	11.422	0.000	0.12	-4.30	0.00	-5.60	4.30	4.30	4.30	4.67
38	50	50	-17.243	12.378	0.000	0.58	-2.77	0.01	-3.53	4.30	4.30	4.30	4.30
39	50	50	-14.000	7.600	0.000	4.03	0.00	5.51	0.00	4.30	4.30	4.59	4.30

ANALİZ SONUÇLARI

Nokta no	dx cm	dy cm	X m	Y m	Z m	Mxalt (tm)	Mxust (tm)	Myalt (tm)	Myust (tm)	Asax cm ²	Asux cm ²	Asay cm ²	Asuy cm ²
40	50	50	-19.200	13.333	0.000	11.76	0.00	2.62	-0.21	9.90	4.30	4.30	4.30
41	50	50	-18.221	13.333	0.000	4.18	-0.58	0.78	-1.24	4.30	4.30	4.30	4.30
42	50	50	-14.307	10.467	0.000	0.02	-3.75	0.08	-6.20	4.30	4.30	4.30	5.18
43	50	50	-13.329	9.511	0.000	0.24	-2.11	0.85	-3.84	4.30	4.30	4.30	4.30
44	50	50	-15.286	11.422	0.000	0.03	-4.69	0.00	-6.70	4.30	4.30	4.30	5.60
45	50	50	-12.350	8.556	0.000	1.34	-0.93	4.68	-1.11	4.30	4.30	4.30	4.30
46	50	50	-13.329	7.600	0.000	2.56	-0.07	5.71	0.00	4.30	4.30	4.76	4.30
47	50	50	-16.264	12.378	0.000	0.05	-4.26	0.00	-5.52	4.30	4.30	4.30	4.60
48	50	50	-17.243	13.333	0.000	0.40	-2.43	0.05	-3.33	4.30	4.30	4.30	4.30
49	50	50	-19.200	14.289	0.000	7.91	-0.03	1.90	-0.33	6.62	4.30	4.30	4.30
50	50	50	-18.221	14.289	0.000	2.84	-0.51	0.73	-1.16	4.30	4.30	4.30	4.30
51	50	50	-13.329	10.467	0.000	0.00	-3.55	0.05	-5.97	4.30	4.30	4.30	4.98
52	50	50	-14.307	11.422	0.000	0.00	-4.58	0.00	-7.07	4.30	4.30	4.30	5.91
53	50	50	-12.350	9.511	0.000	0.10	-2.12	0.65	-3.59	4.30	4.30	4.30	4.30
54	50	50	-15.286	12.378	0.000	0.01	-4.65	0.00	-6.60	4.30	4.30	4.30	5.51
55	50	50	-11.371	8.556	0.000	1.36	-0.71	2.23	-0.84	4.30	4.30	4.30	4.30
56	50	50	-12.350	7.600	0.000	1.89	-0.25	5.48	-0.10	4.30	4.30	4.57	4.30
57	50	50	-11.500	7.750	0.000	1.56	-0.31	2.79	-0.14	4.30	4.30	4.30	4.30
58	500	500	-12.750	7.600	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
59	50	50	-16.264	13.333	0.000	0.02	-3.59	0.07	-4.94	4.30	4.30	4.30	4.30
60	50	50	-17.243	14.289	0.000	0.19	-1.81	0.49	-2.48	4.30	4.30	4.30	4.30
61	50	50	-19.200	15.244	0.000	5.11	-0.38	1.26	-0.12	4.30	4.30	4.30	4.30
62	50	50	-18.221	15.244	0.000	1.04	-0.53	1.37	-0.45	4.30	4.30	4.30	4.30
63	50	50	-13.329	11.422	0.000	0.00	-4.29	0.00	-6.75	4.30	4.30	4.30	5.64
64	50	50	-12.350	10.467	0.000	0.00	-3.16	0.02	-5.22	4.30	4.30	4.30	4.36
65	50	50	-14.307	12.378	0.000	0.00	-4.53	0.00	-6.95	4.30	4.30	4.30	5.81
66	50	50	-11.371	9.511	0.000	0.28	-1.47	0.40	-2.88	4.30	4.30	4.30	4.30
67	50	50	-15.286	13.333	0.000	0.00	-3.84	0.09	-5.73	4.30	4.30	4.30	4.78
68	50	50	-10.393	8.556	0.000	1.40	-0.44	2.53	-0.92	4.30	4.30	4.30	4.30
69	50	50	-11.500	7.600	0.000	2.10	0.00	4.13	-0.03	4.30	4.30	4.30	4.30
70	50	50	-11.371	7.600	0.000	2.10	0.00	2.11	-0.04	4.30	4.30	4.30	4.30
71	50	50	-16.264	14.289	0.000	0.17	-2.42	0.75	-3.36	4.30	4.30	4.30	4.30
72	50	50	-17.243	15.244	0.000	0.70	-1.02	2.83	-1.03	4.30	4.30	4.30	4.30
73	50	50	-19.200	16.200	0.000	1.46	-0.58	1.45	-0.11	4.30	4.30	4.30	4.30
74	50	50	-19.050	15.700	0.000	1.66	-0.74	0.31	-0.17	4.30	4.30	4.30	4.30
75	50	50	-18.221	16.200	0.000	0.97	-0.41	3.27	-0.21	4.30	4.30	4.30	4.30
76	50	50	-13.329	12.378	0.000	0.00	-4.26	0.00	-6.62	4.30	4.30	4.30	5.53
77	50	50	-12.350	11.422	0.000	0.00	-3.77	0.00	-5.78	4.30	4.30	4.30	4.82
78	50	50	-11.371	10.467	0.000	0.00	-2.24	0.00	-3.95	4.30	4.30	4.30	4.30
79	50	50	-14.307	13.333	0.000	0.02	-3.71	0.08	-6.03	4.30	4.30	4.30	5.03
80	50	50	-10.393	9.511	0.000	0.53	-0.82	0.21	-2.22	4.30	4.30	4.30	4.30
81	50	50	-15.286	14.289	0.000	0.20	-2.50	0.85	-3.82	4.30	4.30	4.30	4.30
82	50	50	-9.414	8.556	0.000	1.14	-0.22	0.48	-1.03	4.30	4.30	4.30	4.30
83	50	50	-10.393	7.600	0.000	0.73	-0.18	1.20	-0.38	4.30	4.30	4.30	4.30
84	500	500	-10.400	7.600	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
85	50	50	-16.114	15.244	0.000	0.92	-1.25	3.27	-0.89	4.30	4.30	4.30	4.30
86	50	50	-17.243	16.200	0.000	0.98	-0.46	3.58	-0.07	4.30	4.30	4.30	4.30
87	50	50	-16.500	16.050	0.000	2.01	-0.36	3.44	0.00	4.30	4.30	4.30	4.30
88	500	500	-17.951	16.200	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
89	50	50	-13.329	13.333	0.000	0.01	-3.60	0.09	-5.84	4.30	4.30	4.30	4.87
90	50	50	-12.350	12.378	0.000	0.00	-3.80	0.00	-5.70	4.30	4.30	4.30	4.75
91	50	50	-11.371	11.422	0.000	0.06	-2.64	0.00	-4.15	4.30	4.30	4.30	4.30
92	50	50	-10.393	10.467	0.000	0.95	-1.00	0.04	-2.13	4.30	4.30	4.30	4.30
93	50	50	-14.307	14.289	0.000	0.24	-2.50	0.97	-3.99	4.30	4.30	4.30	4.30
94	50	50	-9.414	9.511	0.000	3.81	-0.26	0.67	-1.05	4.30	4.30	4.30	4.30
95	50	50	-15.286	15.244	0.000	1.44	-1.21	4.96	-0.87	4.30	4.30	4.30	4.30
96	50	50	-8.436	8.556	0.000	0.98	-0.73	0.24	-1.20	4.30	4.30	4.30	4.30
97	50	50	-9.414	7.600	0.000	1.22	0.00	1.34	-0.18	4.30	4.30	4.30	4.30
98	50	50	-9.300	7.750	0.000	1.60	-0.24	0.52	-0.29	4.30	4.30	4.30	4.30
99	50	50	-8.800	8.649	0.000	1.33	-0.40	0.17	-1.02	4.30	4.30	4.30	4.30
100	50	50	-16.114	16.200	0.000	4.02	0.00	10.31	0.00	4.30	4.30	8.66	4.30
101	50	50	-16.500	16.200	0.000	2.53	0.00	5.44	0.00	4.30	4.30	4.54	4.30
102	50	50	-13.329	14.289	0.000	0.23	-2.55	0.95	-3.95	4.30	4.30	4.30	4.30
103	50	50	-12.350	13.333	0.000	0.00	-3.39	0.09	-5.18	4.30	4.30	4.30	4.32
104	50	50	-11.371	12.378	0.000	0.11	-2.79	0.00	-4.12	4.30	4.30	4.30	4.30
105	50	50	-10.393	11.422	0.000	1.42	-1.07	0.19	-2.04	4.30	4.30	4.30	4.30
106	50	50	-9.414	10.467	0.000	3.67	-0.15	0.42	-0.77	4.30	4.30	4.30	4.30
107	50	50	-14.386	15.244	0.000	2.44	-0.99	3.92	-0.01	4.30	4.30	4.30	4.30
108	50	50	-8.950	9.900	0.000	5.07	0.00	0.89	-0.61	4.30	4.30	4.30	4.30
109	50	50	-8.436	9.511	0.000	2.25	-0.73	0.32	-0.97	4.30	4.30	4.30	4.30
110	50	50	-8.833	9.511	0.000	4.70	-0.25	1.47	-0.16	4.30	4.30	4.30	4.30
111	50	50	-15.286	16.200	0.000	2.38	-0.30	9.08	-0.01	4.30	4.30	7.61	4.30
112	50	50	-7.457	8.556	0.000	0.14	-1.63	0.00	-1.76	4.30	4.30	4.30	4.30
113	50	50	-8.436	7.600	0.000	0.54	-0.49	0.87	-0.97	4.30	4.30	4.30	4.30
114	50	50	-8.800	7.600	0.000	1.36	-0.43	0.22	-0.68	4.30	4.30	4.30	4.30
115	500	500	-8.800	9.400	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
116	50	50	-12.350	14.289	0.000	0.22	-2.58	0.82	-3.70	4.30	4.30	4.30	4.30
117	50	50	-13.329	15.244	0.000	1.95	-1.39	3.17	-0.95	4.30	4.30	4.30	4.30
118	50	50	-11.371	13.333	0.000	0.17	-2.63	0.08	-3.99	4.30	4.30	4.30	4.30
119	50	50	-10.393	12.378	0.000	1.56	-1.18	0.21	-2.04	4.30	4.30	4.30	4.30
120	50	50	-9.414	11.422	0.000	4.83	-0.12	0.85	-0.40	4.30	4.30	4.30	4.30
121	50	50	-8.800	10.467	0.000	6.22	-0.03	1.30	-0.02	5.19	4.30	4.30	4.30
122	50	50	-14.386	16.200	0.000	2.38	-0.05	8.29	-0.01	4.30	4.30	6.94	4.30



ANALİZ SONUÇLARI

Nokta no	dx cm	dy cm	X m	Y m	Z m	Mxalt (tm)	Mxust (tm)	Myalt (tm)	Myust (tm)	Asax cm ²	Asux cm ²	Asay cm ²	Asuy cm ²
123	50	50	-14.000	16.050	0.000	3.16	-0.05	5.17	-0.01	4.30	4.30	4.31	4.30
124	50	50	-8.436	10.467	0.000	2.98	-0.56	0.46	-0.45	4.30	4.30	4.30	4.30
125	50	50	-7.457	9.511	0.000	0.35	-1.95	0.00	-1.48	4.30	4.30	4.30	4.30
126	50	50	-8.800	9.511	0.000	4.19	-0.25	0.73	-0.42	4.30	4.30	4.30	4.30
127	500	500	-15.250	16.200	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
128	50	50	-7.457	7.600	0.000	0.25	-0.67	1.00	-0.66	4.30	4.30	4.30	4.30
129	50	50	-7.100	7.750	0.000	0.41	-0.55	0.83	-0.36	4.30	4.30	4.30	4.30
130	50	50	-6.479	8.556	0.000	0.66	-1.88	0.14	-1.33	4.30	4.30	4.30	4.30
131	500	500	-8.200	7.600	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
132	50	50	-12.350	15.244	0.000	1.74	-0.85	5.38	-0.09	4.30	4.30	4.49	4.30
133	50	50	-11.371	14.289	0.000	0.41	-2.01	0.68	-3.07	4.30	4.30	4.30	4.30
134	50	50	-13.329	16.200	0.000	2.59	-0.40	7.72	0.00	4.30	4.30	6.46	4.30
135	50	50	-10.393	13.333	0.000	1.41	-1.37	0.25	-2.14	4.30	4.30	4.30	4.30
136	50	50	-9.414	12.378	0.000	5.05	-0.16	1.00	-0.37	4.30	4.30	4.30	4.30
137	50	50	-8.800	11.422	0.000	6.74	0.00	1.32	-0.01	5.63	4.30	4.30	4.30
138	50	50	-14.000	16.200	0.000	3.44	-0.04	7.43	0.00	4.30	4.30	6.21	4.30
139	50	50	-8.436	11.422	0.000	3.88	-0.50	0.78	-0.18	4.30	4.30	4.30	4.30
140	50	50	-7.457	10.467	0.000	0.53	-2.06	0.16	-1.01	4.30	4.30	4.30	4.30
141	50	50	-6.479	9.511	0.000	0.96	-1.61	0.00	-1.23	4.30	4.30	4.30	4.30
142	50	50	-7.300	7.600	0.000	0.37	-0.32	1.47	0.00	4.30	4.30	4.30	4.30
143	50	50	-6.479	7.600	0.000	0.38	-0.91	0.51	-0.54	4.30	4.30	4.30	4.30
144	50	50	-5.650	8.100	0.000	1.44	-1.14	0.33	-0.80	4.30	4.30	4.30	4.30
145	50	50	-5.500	8.556	0.000	1.78	-1.02	0.39	-0.67	4.30	4.30	4.30	4.30
146	50	50	-12.350	16.200	0.000	2.34	-0.43	7.57	-0.02	4.30	4.30	6.33	4.30
147	50	50	-11.371	15.244	0.000	1.32	-1.10	2.06	-0.87	4.30	4.30	4.30	4.30
148	50	50	-11.500	16.050	0.000	1.56	-0.43	3.23	-0.01	4.30	4.30	4.30	4.30
149	50	50	-10.393	14.289	0.000	1.04	-1.29	0.46	-1.92	4.30	4.30	4.30	4.30
150	500	500	-12.750	16.200	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
151	50	50	-9.414	13.333	0.000	4.49	-0.23	0.87	-0.46	4.30	4.30	4.30	4.30
152	50	50	-8.800	12.378	0.000	7.19	-0.01	1.56	-0.01	6.01	4.30	4.30	4.30
153	50	50	-8.436	12.378	0.000	3.92	-0.51	0.75	-0.20	4.30	4.30	4.30	4.30
154	50	50	-7.457	11.422	0.000	0.53	-2.30	0.11	-0.73	4.30	4.30	4.30	4.30
155	50	50	-6.479	10.467	0.000	0.85	-1.96	0.11	-0.84	4.30	4.30	4.30	4.30
156	50	50	-5.500	9.511	0.000	2.36	-1.11	0.39	-0.19	4.30	4.30	4.30	4.30
157	50	50	-5.533	9.511	0.000	1.89	-0.94	0.38	-0.38	4.30	4.30	4.30	4.30
158	50	50	-5.500	7.600	0.000	1.21	-1.37	0.70	-0.40	4.30	4.30	4.30	4.30
159	500	500	-6.200	7.600	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
160	500	500	-5.500	8.999	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
161	50	50	-11.500	16.200	0.000	2.09	-0.03	6.64	-0.02	4.30	4.30	5.55	4.30
162	50	50	-10.393	15.244	0.000	0.92	-0.47	2.00	-0.38	4.30	4.30	4.30	4.30
163	50	50	-10.393	16.200	0.000	0.46	-0.30	1.56	-0.92	4.30	4.30	4.30	4.30
164	50	50	-11.371	16.200	0.000	0.74	-0.02	2.22	0.00	4.30	4.30	4.30	4.30
165	50	50	-9.414	14.289	0.000	3.46	-0.30	0.77	-0.57	4.30	4.30	4.30	4.30
166	50	50	-8.800	13.333	0.000	6.75	-0.02	1.50	-0.01	5.64	4.30	4.30	4.30
167	500	500	-8.800	13.150	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
168	50	50	-8.436	13.333	0.000	3.57	-0.55	0.68	-0.26	4.30	4.30	4.30	4.30
169	50	50	-7.457	12.378	0.000	0.53	-2.35	0.10	-0.73	4.30	4.30	4.30	4.30
170	50	50	-6.479	11.422	0.000	1.02	-2.17	0.24	-0.80	4.30	4.30	4.30	4.30
171	50	50	-5.650	9.900	0.000	1.73	-0.72	0.44	-0.51	4.30	4.30	4.30	4.30
172	50	50	-5.500	10.467	0.000	2.57	-0.54	0.64	-0.38	4.30	4.30	4.30	4.30
173	500	500	-5.500	9.400	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
174	50	50	-9.300	16.050	0.000	0.48	-0.34	0.52	-0.87	4.30	4.30	4.30	4.30
175	50	50	-9.414	15.244	0.000	1.65	-0.35	0.73	-0.86	4.30	4.30	4.30	4.30
176	500	500	-10.400	16.200	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
177	50	50	-9.414	16.200	0.000	0.36	-0.11	1.66	-0.94	4.30	4.30	4.30	4.30
178	50	50	-8.800	14.289	0.000	5.37	-0.03	1.13	-0.04	4.48	4.30	4.30	4.30
179	50	50	-7.457	13.333	0.000	0.53	-2.53	0.12	-1.00	4.30	4.30	4.30	4.30
180	50	50	-8.436	14.289	0.000	2.83	-0.62	0.55	-0.51	4.30	4.30	4.30	4.30
181	50	50	-6.479	12.378	0.000	1.09	-2.45	0.26	-0.75	4.30	4.30	4.30	4.30
182	50	50	-5.500	11.422	0.000	3.49	-0.74	0.73	-0.24	4.30	4.30	4.30	4.30
183	50	50	-8.800	16.200	0.000	1.25	-0.11	0.73	-0.71	4.30	4.30	4.30	4.30
184	50	50	-8.800	15.244	0.000	2.99	-0.11	0.67	-0.18	4.30	4.30	4.30	4.30
185	50	50	-7.457	14.289	0.000	0.43	-2.45	0.08	-1.40	4.30	4.30	4.30	4.30
186	50	50	-6.479	13.333	0.000	1.14	-2.55	0.28	-0.96	4.30	4.30	4.30	4.30
187	50	50	-8.436	15.244	0.000	1.56	-0.45	0.53	-0.55	4.30	4.30	4.30	4.30
188	50	50	-5.500	12.378	0.000	4.06	-0.77	0.97	-0.22	4.30	4.30	4.30	4.30
189	50	50	-8.436	16.200	0.000	0.47	-0.13	1.54	-0.13	4.30	4.30	4.30	4.30
190	50	50	-6.479	14.289	0.000	1.17	-2.44	0.32	-1.22	4.30	4.30	4.30	4.30
191	50	50	-7.457	15.244	0.000	0.43	-1.63	1.04	-1.19	4.30	4.30	4.30	4.30
192	50	50	-5.500	13.333	0.000	4.23	-0.84	1.04	-0.28	4.30	4.30	4.30	4.30
193	500	500	-5.500	12.800	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
194	50	50	-7.457	16.200	0.000	0.59	-0.65	2.29	-0.61	4.30	4.30	4.30	4.30
195	50	50	-5.500	14.289	0.000	3.18	-0.87	0.91	-0.45	4.30	4.30	4.30	4.30
196	50	50	-6.479	15.244	0.000	0.55	-1.22	0.98	-0.97	4.30	4.30	4.30	4.30
197	500	500	-7.299	16.200	0.000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
198	50	50	-6.479	16.200	0.000	1.17	-0.08	3.02	-0.08	4.30	4.30	4.30	4.30
199	50	50	-5.500	15.244	0.000	0.43	-0.89	0.30	-0.51	4.30	4.30	4.30	4.30
200	50	50	-5.650	15.700	0.000	0.46	-0.87	0.41	-0.49	4.30	4.30	4.30	4.30
201	50	50	-5.500	16.200	0.000	0.76	-0.17	1.36	-0.11	4.30	4.30	4.30	4.30

Noktaların tasarım momentleri, bağlı düğüm noktalarının tasarım momentlerinin ortalaması alınmıştır.

TEMEL DONATI SONUÇLARI

Genel donatılar:

H cm	X üst	X alt	Y üst	Y alt
50	ø16 / 20	ø16 / 20	ø16 / 20	ø16 / 20

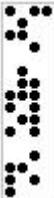
Donatı Asal açısı=0°

İLAVE DONATILAR

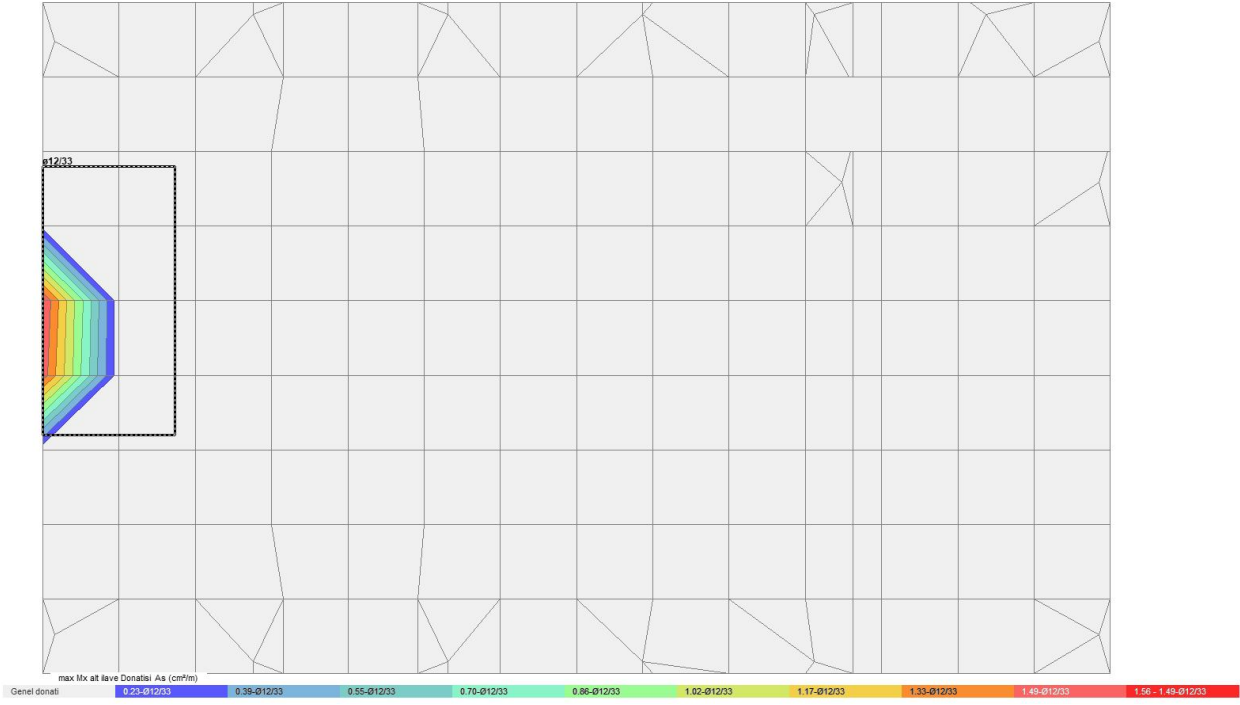
İLAVE DONATI	As (cm ² /m)	donati koordinati	Adet	Boy (m)
ø12/33 X alt	3.43	X=(-19.20÷-17.50) Y=(9.70÷13.14)	11	2.05

└ 50 ø ┘ As>0 ───┐ 50 ø ┘

Ek donatılar, gerekli donatialani kenarından 50 ø uzatılmaktadır



X yonu Alt Ek donati alani grafigi



WINKLER YAY YÜKLERİ (t)

Nokta no	1 g	2 q	3 q	4 q	5 q	6 q	7 q	8 s	9 e	10 e	11 e	12 e	13 w	14 w	17 Ez
1	1.21	0.24	0.13	0.21	0.24	0.15	0.19	-0.28	-0.73	0.84	-1.00	1.06	-0.02	-0.03	0.78
2	2.80	0.56	0.32	0.49	0.54	0.38	0.43	-0.59	-1.58	1.84	-2.20	2.33	-0.03	-0.06	1.80
3	2.44	0.49	0.29	0.43	0.46	0.36	0.38	-0.47	-1.29	1.52	-1.82	1.91	-0.03	-0.05	1.56
4	2.01	0.40	0.23	0.35	0.40	0.25	0.32	-0.45	-1.20	1.35	-1.31	1.39	-0.02	-0.04	1.29
5	1.51	0.30	0.17	0.26	0.30	0.19	0.24	-0.34	-0.89	1.02	-1.10	1.17	-0.02	-0.03	0.97
6	5.86	1.18	0.69	1.03	1.15	0.81	0.93	-1.20	-3.25	3.69	-3.63	3.85	-0.07	-0.10	3.72
7	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
8	5.43	1.13	0.67	0.97	1.06	0.83	0.87	-1.00	-2.79	3.19	-3.20	3.36	-0.06	-0.09	3.41
9	0.79	0.16	0.09	0.14	0.15	0.12	0.12	-0.14	-0.40	0.47	-0.57	0.59	-0.01	-0.02	0.51
10	3.25	0.64	0.37	0.56	0.64	0.40	0.52	-0.71	-1.92	2.10	-1.54	1.63	-0.04	-0.04	2.07
11	5.53	1.13	0.67	0.98	1.09	0.78	0.90	-1.09	-3.03	3.32	-2.50	2.64	-0.06	-0.07	3.47
12	4.60	0.98	0.60	0.84	0.89	0.77	0.74	-0.75	-2.16	2.50	-2.57	2.66	-0.05	-0.07	2.86
13	4.25	0.91	0.56	0.79	0.85	0.68	0.71	-0.75	-2.12	2.35	-1.84	1.93	-0.04	-0.05	2.59
14	1.67	0.34	0.20	0.29	0.31	0.26	0.26	-0.30	-0.84	0.98	-1.16	1.20	-0.02	-0.03	1.06
15	1.75	0.36	0.21	0.31	0.33	0.28	0.27	-0.30	-0.86	1.02	-1.24	1.28	-0.02	-0.03	1.12
16	3.24	0.64	0.37	0.56	0.64	0.41	0.52	-0.69	-1.91	2.02	-0.96	1.01	-0.04	-0.03	2.07
17	5.43	1.12	0.68	0.97	1.08	0.78	0.90	-1.04	-2.94	3.12	-1.52	1.60	-0.06	-0.04	3.37
18	5.11	1.10	0.68	0.94	0.98	0.91	0.83	-0.75	-2.24	2.62	-2.76	2.81	-0.05	-0.08	3.15
19	3.65	0.81	0.52	0.70	0.74	0.65	0.63	-0.56	-1.65	1.85	-1.52	1.58	-0.03	-0.04	2.17
20	3.60	0.79	0.50	0.68	0.74	0.59	0.63	-0.60	-1.75	1.87	-0.96	1.00	-0.03	-0.03	2.14
21	3.07	0.64	0.38	0.54	0.57	0.52	0.47	-0.49	-1.43	1.71	-2.10	2.14	-0.03	-0.06	1.96
22	3.24	0.64	0.38	0.56	0.64	0.41	0.52	-0.67	-1.90	1.94	-0.38	0.39	-0.03	-0.01	2.07
23	5.38	1.12	0.69	0.97	1.08	0.78	0.90	-1.00	-2.90	2.97	-0.57	0.58	-0.05	-0.02	3.33
24	3.45	0.79	0.52	0.68	0.71	0.66	0.61	-0.46	-1.41	1.60	-1.38	1.41	-0.03	-0.04	2.01
25	4.70	1.02	0.64	0.87	0.89	0.88	0.76	-0.61	-1.92	2.26	-2.45	2.46	-0.04	-0.07	2.89
26	2.69	0.62	0.42	0.54	0.57	0.50	0.50	-0.39	-1.16	1.26	-0.69	0.72	-0.02	-0.02	1.52
27	3.50	0.78	0.51	0.68	0.73	0.59	0.63	-0.57	-1.69	1.73	-0.34	0.34	-0.03	-0.01	2.05
28	1.91	0.40	0.24	0.34	0.35	0.34	0.29	-0.27	-0.84	1.01	-1.27	1.27	-0.02	-0.04	1.22
29	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
30	3.25	0.65	0.38	0.56	0.64	0.41	0.53	-0.65	-1.90	1.88	0.20	-0.24	-0.03	0.01	2.07
31	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
32	5.40	1.12	0.69	0.97	1.07	0.78	0.91	-0.97	-2.90	2.86	0.38	-0.43	-0.05	0.01	3.34
33	3.56	0.82	0.55	0.71	0.72	0.72	0.63	-0.41	-1.31	1.51	-1.37	1.37	-0.03	-0.04	2.04
34	2.58	0.62	0.43	0.54	0.56	0.53	0.50	-0.31	-0.98	1.07	-0.64	0.65	-0.02	-0.02	1.40
35	5.29	1.15	0.72	0.98	0.97	1.03	0.85	-0.59	-1.97	2.36	-2.69	2.63	-0.04	-0.08	3.24
36	1.59	0.33	0.20	0.28	0.29	0.29	0.24	-0.21	-0.67	0.81	-1.00	1.00	-0.02	-0.03	1.01
37	2.58	0.61	0.42	0.53	0.56	0.50	0.50	-0.35	-1.08	1.11	-0.22	0.23	-0.02	-0.01	1.41
38	3.52	0.78	0.51	0.68	0.73	0.59	0.64	-0.55	-1.69	1.66	0.28	-0.31	-0.03	0.01	2.06
39	0.74	0.15	0.09	0.13	0.13	0.13	0.11	-0.10	-0.31	0.38	-0.48	0.48	-0.01	-0.01	0.47
40	3.26	0.65	0.39	0.56	0.64	0.42	0.53	-0.64	-1.91	1.82	0.78	-0.87	-0.03	0.02	2.08
41	5.47	1.14	0.70	0.97	1.08	0.79	0.92	-0.96	-2.95	2.79	1.33	-1.45	-0.05	0.04	3.40
42	2.54	0.62	0.44	0.54	0.55	0.55	0.50	-0.26	-0.85	0.94	-0.60	0.59	-0.02	-0.02	1.35
43	3.62	0.84	0.56	0.72	0.72	0.76	0.64	-0.35	-1.21	1.41	-1.35	1.32	-0.03	-0.04	2.07
44	2.44	0.60	0.43	0.53	0.55	0.52	0.50	-0.27	-0.88	0.91	-0.19	0.19	-0.02	-0.01	1.26

WINKLER YAY YÜKLERİ (t)

Nokta no	1 g	2 q	3 q	4 q	5 q	6 q	7 q	8 s	9 e	10 e	11 e	12 e	13 w	14 w	17 Ez
45	5.38	1.16	0.74	0.99	0.96	1.07	0.85	-0.51	-1.82	2.22	-2.70	2.59	-0.04	-0.08	3.29
46	2.45	0.51	0.31	0.43	0.43	0.45	0.37	-0.31	-0.99	1.21	-1.59	1.56	-0.02	-0.04	1.56
47	2.59	0.61	0.43	0.53	0.56	0.50	0.50	-0.34	-1.08	1.06	0.23	-0.25	-0.02	0.01	1.42
48	3.63	0.80	0.52	0.68	0.74	0.61	0.65	-0.55	-1.76	1.65	0.91	-0.97	-0.03	0.03	2.16
49	3.29	0.66	0.39	0.56	0.64	0.42	0.54	-0.63	-1.93	1.77	1.36	-1.49	-0.03	0.04	2.09
50	5.60	1.16	0.71	0.98	1.09	0.81	0.94	-0.96	-3.04	2.77	2.31	-2.50	-0.05	0.06	3.51
51	2.57	0.63	0.45	0.55	0.54	0.58	0.50	-0.21	-0.77	0.86	-0.57	0.55	-0.02	-0.02	1.37
52	2.38	0.60	0.44	0.53	0.54	0.54	0.50	-0.21	-0.74	0.78	-0.16	0.15	-0.01	0.00	1.20
53	3.65	0.83	0.56	0.71	0.70	0.77	0.63	-0.30	-1.11	1.31	-1.31	1.25	-0.02	-0.04	2.11
54	2.45	0.61	0.44	0.53	0.55	0.53	0.50	-0.26	-0.88	0.85	0.24	-0.25	-0.02	0.01	1.27
55	3.48	0.74	0.48	0.63	0.60	0.70	0.54	-0.27	-1.06	1.32	-1.74	1.64	-0.02	-0.05	2.13
56	2.62	0.55	0.33	0.46	0.45	0.50	0.39	-0.28	-0.97	1.21	-1.70	1.63	-0.02	-0.05	1.66
57	3.08	0.64	0.40	0.54	0.52	0.60	0.46	-0.28	-1.03	1.31	-1.93	1.83	-0.02	-0.05	1.94
58	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
59	2.73	0.63	0.43	0.54	0.57	0.51	0.52	-0.35	-1.16	1.08	0.71	-0.74	-0.02	0.02	1.54
60	4.31	0.93	0.60	0.78	0.85	0.70	0.75	-0.65	-2.13	1.91	1.79	-1.90	-0.03	0.05	2.63
61	1.92	0.38	0.23	0.33	0.37	0.25	0.32	-0.36	-1.13	1.00	1.12	-1.22	-0.02	0.03	1.22
62	5.88	1.21	0.74	1.01	1.12	0.84	0.98	-0.99	-3.22	2.81	3.39	-3.65	-0.05	0.09	3.72
63	2.42	0.61	0.45	0.53	0.53	0.57	0.50	-0.17	-0.67	0.70	-0.13	0.12	-0.01	0.00	1.22
64	2.67	0.64	0.45	0.55	0.54	0.60	0.50	-0.18	-0.72	0.81	-0.55	0.52	-0.02	-0.02	1.45
65	2.40	0.61	0.45	0.53	0.54	0.55	0.50	-0.20	-0.74	0.72	0.27	-0.27	-0.01	0.01	1.21
66	3.77	0.84	0.56	0.71	0.68	0.80	0.63	-0.25	-1.04	1.24	-1.32	1.23	-0.02	-0.04	2.21
67	2.62	0.63	0.45	0.54	0.56	0.54	0.51	-0.27	-0.98	0.89	0.71	-0.72	-0.02	0.02	1.43
68	5.66	1.18	0.77	0.99	0.94	1.15	0.86	-0.35	-1.54	1.95	-2.86	2.63	-0.04	-0.08	3.48
69	0.88	0.18	0.11	0.15	0.15	0.17	0.13	-0.08	-0.30	0.38	-0.58	0.55	-0.01	-0.02	0.56
70	1.13	0.23	0.14	0.20	0.19	0.22	0.17	-0.10	-0.38	0.48	-0.74	0.70	-0.01	-0.02	0.71
71	3.72	0.83	0.55	0.70	0.74	0.67	0.67	-0.47	-1.65	1.46	1.56	-1.63	-0.02	0.04	2.21
72	5.34	1.13	0.70	0.93	1.01	0.84	0.90	-0.79	-2.69	2.32	3.05	-3.23	-0.04	0.08	3.35
73	1.21	0.24	0.15	0.20	0.23	0.16	0.20	-0.22	-0.72	0.61	0.91	-0.98	-0.01	0.03	0.77
74	1.40	0.28	0.17	0.24	0.27	0.18	0.23	-0.26	-0.82	0.71	0.93	-1.01	-0.01	0.03	0.90
75	2.87	0.59	0.36	0.49	0.54	0.41	0.47	-0.48	-1.59	1.33	2.12	-2.27	-0.02	0.06	1.83
76	2.44	0.62	0.46	0.53	0.53	0.57	0.50	-0.16	-0.66	0.63	0.30	-0.30	-0.01	0.01	1.24
77	2.54	0.62	0.46	0.54	0.53	0.59	0.50	-0.14	-0.63	0.66	-0.09	0.08	-0.01	0.00	1.33
78	2.83	0.65	0.46	0.55	0.53	0.62	0.50	-0.15	-0.70	0.79	-0.54	0.49	-0.01	-0.02	1.60
79	2.58	0.63	0.46	0.54	0.55	0.57	0.52	-0.21	-0.84	0.76	0.73	-0.73	-0.01	0.02	1.38
80	3.92	0.84	0.57	0.70	0.67	0.82	0.63	-0.20	-0.97	1.17	-1.34	1.22	-0.02	-0.04	2.35
81	3.53	0.81	0.55	0.68	0.70	0.68	0.65	-0.37	-1.39	1.21	1.50	-1.53	-0.02	0.04	2.06
82	4.62	0.94	0.63	0.78	0.73	0.93	0.69	-0.20	-1.08	1.42	-2.35	2.13	-0.03	-0.07	2.85
83	2.81	0.57	0.36	0.48	0.46	0.55	0.41	-0.20	-0.84	1.10	-1.87	1.73	-0.02	-0.05	1.76
84	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
85	4.43	0.96	0.61	0.78	0.83	0.76	0.75	-0.56	-2.01	1.71	2.50	-2.60	-0.03	0.07	2.76
86	2.50	0.52	0.32	0.42	0.46	0.38	0.41	-0.37	-1.28	1.07	1.81	-1.91	-0.02	0.05	1.60
87	1.40	0.29	0.18	0.24	0.25	0.23	0.23	-0.19	-0.67	0.56	0.96	-1.00	-0.01	0.03	0.89
88	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
89	2.62	0.64	0.47	0.54	0.54	0.59	0.52	-0.17	-0.75	0.66	0.77	-0.75	-0.01	0.02	1.41
90	2.56	0.63	0.47	0.54	0.52	0.60	0.51	-0.13	-0.62	0.59	0.35	-0.34	-0.01	0.01	1.35
91	2.75	0.64	0.47	0.54	0.52	0.62	0.51	-0.12	-0.63	0.66	-0.05	0.04	-0.01	0.00	1.52
92	3.05	0.66	0.46	0.55	0.52	0.65	0.51	-0.12	-0.69	0.79	-0.53	0.47	-0.01	-0.01	1.80
93	3.65	0.85	0.58	0.70	0.71	0.75	0.67	-0.31	-1.28	1.09	1.58	-1.57	-0.02	0.04	2.11
94	3.83	0.79	0.54	0.65	0.61	0.78	0.59	-0.13	-0.83	1.03	-1.28	1.15	-0.02	-0.04	2.35
95	5.25	1.15	0.74	0.93	0.97	0.95	0.89	-0.57	-2.20	1.84	2.96	-3.01	-0.03	0.08	3.25
96	4.73	0.94	0.65	0.77	0.71	0.95	0.69	-0.12	-0.91	1.25	-2.41	2.16	-0.02	-0.07	2.92
97	1.86	0.37	0.24	0.31	0.29	0.37	0.27	-0.10	-0.48	0.66	-1.26	1.15	-0.01	-0.04	1.16
98	0.87	0.17	0.11	0.15	0.14	0.17	0.13	-0.04	-0.22	0.30	-0.57	0.52	-0.01	-0.02	0.54
99	1.32	0.26	0.18	0.22	0.20	0.27	0.19	-0.04	-0.27	0.37	-0.65	0.59	-0.01	-0.02	0.82
100	1.70	0.36	0.22	0.29	0.31	0.28	0.28	-0.21	-0.80	0.65	1.21	-1.25	-0.01	0.03	1.09
101	0.80	0.17	0.10	0.14	0.15	0.13	0.13	-0.11	-0.39	0.32	0.57	-0.60	-0.01	0.02	0.51
102	3.73	0.87	0.60	0.71	0.71	0.79	0.68	-0.25	-1.15	0.97	1.66	-1.61	-0.02	0.05	2.16
103	2.73	0.65	0.47	0.54	0.53	0.61	0.52	-0.13	-0.69	0.60	0.83	-0.80	-0.01	0.02	1.50
104	2.77	0.65	0.47	0.54	0.52	0.63	0.52	-0.10	-0.61	0.59	0.43	-0.41	-0.01	0.01	1.54
105	3.02	0.66	0.47	0.55	0.52	0.65	0.51	-0.09	-0.64	0.67	0.00	-0.01	-0.01	0.00	1.77
106	2.83	0.58	0.41	0.47	0.44	0.58	0.44	-0.07	-0.57	0.66	-0.45	0.40	-0.01	-0.01	1.73
107	4.57	1.01	0.66	0.81	0.82	0.87	0.78	-0.42	-1.74	1.43	2.60	-2.59	-0.02	0.07	2.83
108	0.97	0.20	0.14	0.16	0.15	0.20	0.15	-0.02	-0.19	0.23	-0.25	0.22	0.00	-0.01	0.60
109	3.57	0.71	0.50	0.57	0.53	0.72	0.54	-0.06	-0.62						

FİRMA : ESPO MUH. DAN. INS. LTD. STI.

30-09-2025

SAYFA: 73

PROJE : CERRAHPAŞA YURT SU DEPOSU

(250929-ES374-CERRAH-SU-D-D04.ST4)

WINKLER YAY YÜKLERİ (t)

Nokta no	1 g	2 q	3 q	4 q	5 q	6 q	7 q	8 s	9 e	10 e	11 e	12 e	13 w	14 w	17 Ez
128	1.96	0.37	0.26	0.30	0.28	0.39	0.28	-0.03	-0.33	0.52	-1.37	1.22	-0.01	-0.04	1.22
129	0.98	0.18	0.13	0.15	0.13	0.19	0.14	-0.01	-0.15	0.23	-0.66	0.58	0.00	-0.02	0.61
130	4.74	0.87	0.66	0.67	0.62	0.92	0.67	0.07	-0.47	0.82	-2.41	2.14	-0.02	-0.07	2.95
131	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
132	5.42	1.19	0.80	0.93	0.91	1.09	0.91	-0.28	-1.58	1.22	3.26	-3.10	-0.02	0.09	3.36
133	3.91	0.87	0.62	0.69	0.66	0.83	0.68	-0.13	-0.92	0.73	1.88	-1.75	-0.01	0.05	2.34
134	2.55	0.54	0.35	0.42	0.42	0.48	0.41	-0.18	-0.89	0.68	1.83	-1.78	-0.01	0.05	1.63
135	3.14	0.68	0.49	0.54	0.51	0.66	0.54	-0.06	-0.62	0.53	1.07	-0.99	-0.01	0.03	1.88
136	2.69	0.56	0.40	0.43	0.41	0.55	0.43	-0.03	-0.48	0.46	0.53	-0.48	-0.01	0.01	1.66
137	1.68	0.34	0.24	0.26	0.24	0.34	0.26	-0.01	-0.28	0.30	0.06	-0.05	-0.01	0.00	1.04
138	0.75	0.16	0.10	0.12	0.13	0.14	0.12	-0.06	-0.29	0.22	0.53	-0.52	0.00	0.01	0.48
139	2.29	0.46	0.33	0.35	0.33	0.46	0.35	0.00	-0.34	0.36	0.10	-0.09	-0.01	0.00	1.43
140	4.06	0.79	0.59	0.60	0.56	0.81	0.61	0.04	-0.46	0.59	-0.51	0.46	-0.01	-0.01	2.52
141	5.05	0.93	0.72	0.71	0.64	0.99	0.74	0.11	-0.41	0.68	-1.58	1.41	-0.01	-0.04	3.15
142	0.37	0.07	0.05	0.06	0.05	0.07	0.05	0.00	-0.06	0.10	-0.26	0.23	0.00	-0.01	0.23
143	1.43	0.26	0.19	0.21	0.19	0.28	0.20	0.01	-0.17	0.31	-1.01	0.89	-0.01	-0.03	0.89
144	1.37	0.24	0.19	0.18	0.17	0.26	0.19	0.04	-0.09	0.21	-0.82	0.72	0.00	-0.02	0.86
145	1.89	0.33	0.27	0.25	0.22	0.36	0.26	0.07	-0.09	0.23	-0.94	0.84	-0.01	-0.03	1.19
146	2.74	0.58	0.39	0.44	0.43	0.53	0.45	-0.14	-0.83	0.61	2.04	-1.94	-0.01	0.06	1.76
147	4.61	0.99	0.68	0.76	0.73	0.93	0.77	-0.15	-1.14	0.84	2.90	-2.70	-0.01	0.08	2.88
148	3.16	0.67	0.45	0.50	0.48	0.62	0.51	-0.11	-0.83	0.58	2.36	-2.21	-0.01	0.07	2.02
149	4.10	0.88	0.63	0.68	0.64	0.85	0.69	-0.07	-0.82	0.63	2.07	-1.90	-0.01	0.06	2.52
150	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
151	2.74	0.57	0.41	0.43	0.40	0.56	0.44	-0.01	-0.46	0.39	1.01	-0.91	-0.01	0.03	1.70
152	1.69	0.34	0.25	0.26	0.24	0.34	0.26	0.00	-0.26	0.25	0.36	-0.32	0.00	0.01	1.06
153	2.31	0.46	0.34	0.35	0.32	0.47	0.36	0.01	-0.32	0.30	0.51	-0.46	-0.01	0.01	1.45
154	4.10	0.80	0.60	0.60	0.55	0.82	0.63	0.07	-0.41	0.46	0.25	-0.21	-0.01	0.01	2.56
155	5.45	1.01	0.79	0.75	0.68	1.07	0.81	0.16	-0.37	0.54	-0.64	0.58	-0.01	-0.02	3.41
156	1.78	0.31	0.26	0.23	0.21	0.34	0.25	0.08	-0.06	0.15	-0.53	0.47	0.00	-0.01	1.12
157	1.16	0.20	0.17	0.15	0.13	0.22	0.16	0.05	-0.04	0.10	-0.34	0.31	0.00	-0.01	0.73
158	1.17	0.20	0.16	0.16	0.14	0.22	0.16	0.03	-0.08	0.20	-0.82	0.73	0.00	-0.02	0.73
159	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
160	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
161	0.92	0.19	0.13	0.15	0.14	0.18	0.15	-0.03	-0.24	0.17	0.71	-0.67	0.00	0.02	0.59
162	5.95	1.25	0.88	0.94	0.89	1.20	0.98	-0.08	-1.21	0.83	3.93	-3.60	-0.01	0.11	3.75
163	3.01	0.62	0.44	0.46	0.43	0.60	0.49	-0.03	-0.62	0.37	2.45	-2.24	-0.01	0.07	1.93
164	0.08	0.02	0.01	0.01	0.01	0.02	0.01	0.00	-0.02	0.01	0.06	-0.06	0.00	0.00	0.05
165	3.49	0.72	0.52	0.53	0.50	0.71	0.56	0.00	-0.57	0.41	1.86	-1.69	-0.01	0.05	2.19
166	1.72	0.35	0.25	0.26	0.24	0.35	0.27	0.01	-0.25	0.20	0.66	-0.60	0.00	0.02	1.08
167	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
168	2.34	0.47	0.35	0.35	0.32	0.47	0.37	0.03	-0.30	0.23	0.93	-0.83	0.00	0.03	1.48
169	4.15	0.81	0.62	0.59	0.54	0.83	0.64	0.10	-0.37	0.34	1.01	-0.88	-0.01	0.03	2.60
170	5.76	1.07	0.85	0.77	0.71	1.13	0.87	0.21	-0.31	0.38	0.43	-0.36	-0.01	0.01	3.63
171	1.53	0.27	0.22	0.20	0.18	0.29	0.22	0.06	-0.05	0.12	-0.34	0.30	0.00	-0.01	0.97
172	2.17	0.38	0.32	0.27	0.24	0.41	0.31	0.11	-0.04	0.11	-0.21	0.20	0.00	-0.01	1.38
173	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
174	2.71	0.55	0.40	0.39	0.37	0.54	0.44	0.03	-0.40	0.19	2.26	-2.04	0.00	0.06	1.74
175	3.61	0.74	0.54	0.54	0.50	0.73	0.58	0.02	-0.57	0.34	2.52	-2.28	-0.01	0.07	2.30
176	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
177	1.21	0.25	0.18	0.18	0.16	0.24	0.20	0.01	-0.19	0.09	1.03	-0.94	0.00	0.03	0.78
178	2.18	0.44	0.32	0.32	0.30	0.44	0.35	0.03	-0.30	0.20	1.21	-1.09	0.00	0.03	1.38
179	4.20	0.82	0.63	0.58	0.54	0.84	0.66	0.13	-0.33	0.22	1.76	-1.56	0.00	0.05	2.65
180	2.97	0.59	0.44	0.43	0.40	0.59	0.47	0.06	-0.35	0.22	1.68	-1.50	0.00	0.05	1.88
181	5.83	1.09	0.87	0.77	0.70	1.14	0.89	0.26	-0.24	0.20	1.53	-1.32	0.00	0.04	3.69
182	3.36	0.60	0.50	0.41	0.37	0.64	0.49	0.19	-0.02	0.06	0.33	-0.26	0.00	0.01	2.14
183	1.67	0.33	0.25	0.23	0.22	0.33	0.27	0.04	-0.20	0.07	1.46	-1.31	0.00	0.04	1.07
184	2.90	0.58	0.43	0.42	0.39	0.58	0.46	0.05	-0.37	0.19	2.09	-1.87	0.00	0.06	1.85
185	4.69	0.91	0.71	0.64	0.58	0.93	0.74	0.18	-0.33	0.12	2.79	-2.46	0.00	0.08	2.98
186	5.90	1.10	0.89	0.76	0.69	1.16	0.91	0.30	-0.18	0.03	2.63	-2.29	0.00	0.07	3.75
187	4.22	0.84	0.63	0.59	0.55	0.84	0.67	0.10	-0.47	0.20	3.09	-2.77	0.00	0.09	2.70
188	3.40	0.61	0.51	0.41	0.36	0.65	0.51	0.22	0.02	-0.05	0.98	-0.84	0.00	0.03	2.18
189	2.46	0.49	0.37	0.34	0.31	0.49	0.39	0.07	-0.25	0.06	2.19	-1.96	0.00	0.06	1.58
190	5.98	1.12	0.91	0.75	0.68	1.17	0.93	0.35	-0.12	-0.15	3.73	-3.27	0.00	0.10	3.83
191	6.09	1.18	0.93	0.80	0.74	1.21	0.97	0.27	-0.37	-0.01	4.66	-4.13	0.00	0.13	3.91
192	3.44	0.62	0.52	0.40	0.36	0.66	0.52	0.24	0.06	-0.15	1.63	-1.41	0.00	0.05	2.22
193	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
194	3.58	0.69	0.54	0.46	0.42	0.70	0.57	0.18	-0.19	-0.10	3.33	-2.95	0.00	0.09	2.31
195	3.48	0.63	0.53	0.40	0.36	0.67	0.53	0.27	0.10	-0.25	2.28	-1.98	0.00	0.06	2.25
196	6.08	1.14	0.93	0.74	0.67	1.19	0.95	0.39	-0.07	-0.31	4.86	-4.26	0.01	0.14	3.92
197	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
198	2.89	0.54	0.45	0.34	0.31	0.56	0.46	0.20	-0.01	-0.22	2.80	-2.45	0.00	0.08	1.88
199	2.32	0.42	0.36	0.26	0.23	0.45	0.36	0.19	0.09	-0.23	1.93	-1.67	0.00	0.05	1.51
200	1.66	0.30	0.26	0.19	0.17	0.32	0.26	0.14	0.06	-0.18	1.51	-1.31	0.00	0.04	1.08
201	0.91	0.17	0.14	0.10	0.09	0.18	0.14	0.08	0.04	-0.12	0.91	-0.80	0.00	0.03	0.60

LOADS CHECK

DEAD LOADS CHECK

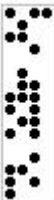
Wg=416.69 (t) (G JOINT LOADS) +147.28 (DEAD LOAD) =564.02 (t) (G WINKLER SPRING REACTION)

LIVE LOADS CHECK

Wq=58.85 (t) (Q JOINT LOADS) +58.91 (LIVE LOAD) =117.78 (t) (Q WINKLER SPRING REACTION)

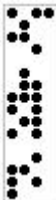
ZEMİN GERİLMESİNİN, ZEMİN TAŞIMA GÜCÜ TASARIM GERİLMESİNE GÖRE KONTROLU t/m^2

Nokta	G	Q	E	W	1.4 G + 1.6 Q		G + Q + E		G + Q + W	
1	3.496	0.689	3.740	0.080	5.997	< 38.000 ✓	7.925	< 38.000 ✓	4.265	< 38.000 ✓
2	3.556	0.709	3.646	0.078	6.112	< 38.000 ✓	7.911	< 38.000 ✓	4.342	< 38.000 ✓
3	3.620	0.734	3.538	0.075	6.242	< 38.000 ✓	7.892	< 38.000 ✓	4.429	< 38.000 ✓
4	3.482	0.686	3.077	0.063	5.972	< 38.000 ✓	7.244	< 38.000 ✓	4.231	< 38.000 ✓
5	3.496	0.687	3.380	0.071	5.995	< 38.000 ✓	7.563	< 38.000 ✓	4.254	< 38.000 ✓
6	3.471	0.701	2.938	0.060	5.980	< 38.000 ✓	7.110	< 38.000 ✓	4.231	< 38.000 ✓
8	3.452	0.716	2.790	0.057	5.979	< 38.000 ✓	6.959	< 38.000 ✓	4.225	< 38.000 ✓
9	3.665	0.752	3.449	0.073	6.334	< 38.000 ✓	7.866	< 38.000 ✓	4.490	< 38.000 ✓
10	3.471	0.685	2.906	0.046	5.954	< 38.000 ✓	7.062	< 38.000 ✓	4.201	< 38.000 ✓
11	3.379	0.691	2.668	0.042	5.835	< 38.000 ✓	6.737	< 38.000 ✓	4.112	< 38.000 ✓
12	3.444	0.733	2.635	0.054	5.995	< 38.000 ✓	6.812	< 38.000 ✓	4.231	< 38.000 ✓
13	3.236	0.691	2.382	0.039	5.635	< 38.000 ✓	6.309	< 38.000 ✓	3.965	< 38.000 ✓
14	3.653	0.752	3.341	0.071	6.316	< 38.000 ✓	7.745	< 38.000 ✓	4.475	< 38.000 ✓
15	3.686	0.760	3.402	0.072	6.376	< 38.000 ✓	7.848	< 38.000 ✓	4.518	< 38.000 ✓
16	3.466	0.686	2.819	0.038	5.950	< 38.000 ✓	6.971	< 38.000 ✓	4.190	< 38.000 ✓
17	3.315	0.685	2.527	0.034	5.737	< 38.000 ✓	6.527	< 38.000 ✓	4.034	< 38.000 ✓
18	3.439	0.742	2.530	0.052	6.002	< 38.000 ✓	6.711	< 38.000 ✓	4.233	< 38.000 ✓
19	3.127	0.693	2.141	0.036	5.487	< 38.000 ✓	5.961	< 38.000 ✓	3.856	< 38.000 ✓
20	3.076	0.672	2.151	0.029	5.382	< 38.000 ✓	5.900	< 38.000 ✓	3.777	< 38.000 ✓
21	3.721	0.774	3.304	0.071	6.448	< 38.000 ✓	7.799	< 38.000 ✓	4.566	< 38.000 ✓
22	3.468	0.689	2.740	0.037	5.957	< 38.000 ✓	6.897	< 38.000 ✓	4.193	< 38.000 ✓
23	3.288	0.684	2.424	0.032	5.698	< 38.000 ✓	6.396	< 38.000 ✓	4.004	< 38.000 ✓
24	3.062	0.697	1.954	0.034	5.403	< 38.000 ✓	5.713	< 38.000 ✓	3.794	< 38.000 ✓
25	3.453	0.751	2.443	0.050	6.036	< 38.000 ✓	6.647	< 38.000 ✓	4.254	< 38.000 ✓
26	2.881	0.665	1.831	0.024	5.097	< 38.000 ✓	5.376	< 38.000 ✓	3.570	< 38.000 ✓
27	2.998	0.665	2.005	0.026	5.261	< 38.000 ✓	5.668	< 38.000 ✓	3.689	< 38.000 ✓
28	3.747	0.783	3.206	0.069	6.499	< 38.000 ✓	7.736	< 38.000 ✓	4.600	< 38.000 ✓
30	3.476	0.693	2.701	0.035	5.975	< 38.000 ✓	6.870	< 38.000 ✓	4.204	< 38.000 ✓
32	3.297	0.687	2.387	0.031	5.716	< 38.000 ✓	6.372	< 38.000 ✓	4.015	< 38.000 ✓
33	3.043	0.703	1.818	0.033	5.384	< 38.000 ✓	5.563	< 38.000 ✓	3.778	< 38.000 ✓
34	2.761	0.662	1.594	0.021	4.925	< 38.000 ✓	5.018	< 38.000 ✓	3.444	< 38.000 ✓
35	3.460	0.754	2.394	0.049	6.049	< 38.000 ✓	6.608	< 38.000 ✓	4.262	< 38.000 ✓
36	3.735	0.784	3.070	0.066	6.483	< 38.000 ✓	7.589	< 38.000 ✓	4.585	< 38.000 ✓
37	2.756	0.651	1.643	0.021	4.901	< 38.000 ✓	5.051	< 38.000 ✓	3.429	< 38.000 ✓
38	3.008	0.669	1.971	0.025	5.280	< 38.000 ✓	5.647	< 38.000 ✓	3.701	< 38.000 ✓
39	3.753	0.785	3.179	0.069	6.510	< 38.000 ✓	7.717	< 38.000 ✓	4.606	< 38.000 ✓
40	3.491	0.698	2.714	0.034	6.004	< 38.000 ✓	6.903	< 38.000 ✓	4.223	< 38.000 ✓
41	3.343	0.696	2.427	0.030	5.793	< 38.000 ✓	6.465	< 38.000 ✓	4.068	< 38.000 ✓
42	2.717	0.665	1.440	0.018	4.867	< 38.000 ✓	4.821	< 38.000 ✓	3.400	< 38.000 ✓
43	3.061	0.707	1.720	0.032	5.416	< 38.000 ✓	5.488	< 38.000 ✓	3.800	< 38.000 ✓
44	2.605	0.645	1.380	0.017	4.679	< 38.000 ✓	4.630	< 38.000 ✓	3.267	< 38.000 ✓
45	3.468	0.750	2.379	0.049	6.056	< 38.000 ✓	6.597	< 38.000 ✓	4.267	< 38.000 ✓
46	3.753	0.785	3.153	0.068	6.510	< 38.000 ✓	7.690	< 38.000 ✓	4.606	< 38.000 ✓
47	2.768	0.655	1.611	0.020	4.923	< 38.000 ✓	5.034	< 38.000 ✓	3.442	< 38.000 ✓
48	3.106	0.684	2.057	0.024	5.442	< 38.000 ✓	5.847	< 38.000 ✓	3.814	< 38.000 ✓
49	3.513	0.703	2.737	0.040	6.044	< 38.000 ✓	6.954	< 38.000 ✓	4.257	< 38.000 ✓
50	3.425	0.709	2.502	0.039	5.929	< 38.000 ✓	6.636	< 38.000 ✓	4.173	< 38.000 ✓
51	2.747	0.671	1.356	0.017	4.919	< 38.000 ✓	4.773	< 38.000 ✓	3.434	< 38.000 ✓
52	2.549	0.646	1.214	0.015	4.602	< 38.000 ✓	4.409	< 38.000 ✓	3.210	< 38.000 ✓
53	3.120	0.711	1.665	0.031	5.505	< 38.000 ✓	5.496	< 38.000 ✓	3.862	< 38.000 ✓
54	2.618	0.649	1.348	0.016	4.704	< 38.000 ✓	4.615	< 38.000 ✓	3.283	< 38.000 ✓
55	3.492	0.744	2.391	0.049	6.079	< 38.000 ✓	6.627	< 38.000 ✓	4.285	< 38.000 ✓
56	3.735	0.778	3.128	0.067	6.474	< 38.000 ✓	7.641	< 38.000 ✓	4.581	< 38.000 ✓
57	3.690	0.765	3.010	0.065	6.391	< 38.000 ✓	7.466	< 38.000 ✓	4.520	< 38.000 ✓
59	2.916	0.676	1.739	0.021	5.164	< 38.000 ✓	5.331	< 38.000 ✓	3.613	< 38.000 ✓
60	3.287	0.710	2.221	0.038	5.737	< 38.000 ✓	6.217	< 38.000 ✓	4.034	< 38.000 ✓
61	3.541	0.710	2.929	0.057	6.093	< 38.000 ✓	7.180	< 38.000 ✓	4.308	< 38.000 ✓
62	3.536	0.727	2.868	0.057	6.113	< 38.000 ✓	7.130	< 38.000 ✓	4.319	< 38.000 ✓
63	2.586	0.654	1.136	0.013	4.666	< 38.000 ✓	4.376	< 38.000 ✓	3.253	< 38.000 ✓
64	2.851	0.681	1.333	0.016	5.081	< 38.000 ✓	4.865	< 38.000 ✓	3.548	< 38.000 ✓
65	2.564	0.650	1.181	0.013	4.630	< 38.000 ✓	4.396	< 38.000 ✓	3.228	< 38.000 ✓
66	3.223	0.715	1.697	0.032	5.655	< 38.000 ✓	5.635	< 38.000 ✓	3.969	< 38.000 ✓
67	2.801	0.675	1.501	0.021	5.000	< 38.000 ✓	4.976	< 38.000 ✓	3.496	< 38.000 ✓
68	3.502	0.731	2.411	0.049	6.071	< 38.000 ✓	6.643	< 38.000 ✓	4.282	< 38.000 ✓
69	3.706	0.766	3.118	0.067	6.414	< 38.000 ✓	7.590	< 38.000 ✓	4.540	< 38.000 ✓
70	3.701	0.764	3.117	0.067	6.403	< 38.000 ✓	7.582	< 38.000 ✓	4.532	< 38.000 ✓
71	3.185	0.713	1.978	0.037	5.600	< 38.000 ✓	5.876	< 38.000 ✓	3.935	< 38.000 ✓
72	3.524	0.744	2.794	0.056	6.124	< 38.000 ✓	7.063	< 38.000 ✓	4.324	< 38.000 ✓
73	3.573	0.716	3.595	0.074	6.148	< 38.000 ✓	7.885	< 38.000 ✓	4.364	< 38.000 ✓
74	3.565	0.717	3.246	0.065	6.137	< 38.000 ✓	7.527	< 38.000 ✓	4.347	< 38.000 ✓
75	3.638	0.743	3.580	0.074	6.283	< 38.000 ✓	7.961	< 38.000 ✓	4.456	< 38.000 ✓
76	2.604	0.658	1.101	0.012	4.699	< 38.000 ✓	4.363	< 38.000 ✓	3.275	< 38.000 ✓
77	2.718	0.667	1.133	0.013	4.873	< 38.000 ✓	4.519	< 38.000 ✓	3.398	< 38.000 ✓
78	3.028	0.694	1.361	0.016	5.350	< 38.000 ✓	5.083	< 38.000 ✓	3.738	< 38.000 ✓
79	2.763	0.678	1.341	0.021	4.953	< 38.000 ✓	4.782	< 38.000 ✓	3.463	< 38.000 ✓
80	3.351	0.717	1.751	0.032	5.838	< 38.000 ✓	5.818	< 38.000 ✓	4.100	< 38.000 ✓
81	3.129	0.719	1.904	0.037	5.531	< 38.000 ✓	5.752	< 38.000 ✓	3.885	< 38.000 ✓
82	3.518	0.716	2.439	0.050	6.070	< 38.000 ✓	6.673	< 38.000 ✓	4.284	< 38.000 ✓
83	3.652	0.743	3.113	0.068	6.301	< 38.000 ✓	7.508	< 38.000 ✓	4.463	< 38.000 ✓
85	3.527	0.763	2.725	0.055	6.159	< 38.000 ✓	7.015	< 38.000 ✓	4.345	< 38.000 ✓
86	3.710	0.771	3.551	0.074	6.427	< 38.000 ✓	8.031	< 38.000 ✓	4.555	< 38.000 ✓
87	3.748	0.788	3.413	0.072	6.508	< 38.000 ✓	7.949	< 38.000 ✓	4.607	< 38.000 ✓
89	2.801	0.685	1.270	0.023	5.017	< 38.000 ✓	4.756	< 38.000 ✓	3.509	< 38.000 ✓
90	2.740	0.672	1.094	0.011	4.912	< 38.000 ✓	4.506	< 38.000 ✓	3.423	< 38.000 ✓



ZEMİN GERİLMESİNİN, ZEMİN TAŞIMA GÜCÜ TASARIM GERİLMESİNE GÖRE KONTROLU t/m²

Nokta	G	Q	E	W	1.4 G + 1.6 Q		G + Q + E		G + Q + W	
91	2.940	0.687	1.192	0.013	5.216 <	38.000 ✓	4.820 <	38.000 ✓	3.640 <	38.000 ✓
92	3.258	0.710	1.417	0.016	5.698 <	38.000 ✓	5.385 <	38.000 ✓	3.984 <	38.000 ✓
93	3.120	0.726	1.892	0.037	5.530 <	38.000 ✓	5.739 <	38.000 ✓	3.884 <	38.000 ✓
94	3.478	0.715	1.803	0.033	6.013 <	38.000 ✓	5.997 <	38.000 ✓	4.226 <	38.000 ✓
95	3.531	0.774	2.686	0.055	6.181 <	38.000 ✓	6.991 <	38.000 ✓	4.360 <	38.000 ✓
96	3.500	0.703	2.428	0.050	6.026 <	38.000 ✓	6.631 <	38.000 ✓	4.253 <	38.000 ✓
97	3.597	0.719	3.112	0.068	6.187 <	38.000 ✓	7.428 <	38.000 ✓	4.384 <	38.000 ✓
98	3.581	0.716	3.007	0.065	6.160 <	38.000 ✓	7.305 <	38.000 ✓	4.363 <	38.000 ✓
99	3.519	0.709	2.385	0.048	6.061 <	38.000 ✓	6.613 <	38.000 ✓	4.276 <	38.000 ✓
100	3.788	0.799	3.509	0.075	6.581 <	38.000 ✓	8.095 <	38.000 ✓	4.661 <	38.000 ✓
101	3.763	0.790	3.523	0.074	6.532 <	38.000 ✓	8.076 <	38.000 ✓	4.627 <	38.000 ✓
102	3.151	0.732	1.949	0.039	5.582 <	38.000 ✓	5.831 <	38.000 ✓	3.922 <	38.000 ✓
103	2.915	0.697	1.372	0.025	5.196 <	38.000 ✓	4.984 <	38.000 ✓	3.637 <	38.000 ✓
104	2.967	0.693	1.148	0.013	5.262 <	38.000 ✓	4.807 <	38.000 ✓	3.672 <	38.000 ✓
105	3.228	0.710	1.284	0.013	5.655 <	38.000 ✓	5.222 <	38.000 ✓	3.951 <	38.000 ✓
106	3.481	0.720	1.448	0.015	6.026 <	38.000 ✓	5.650 <	38.000 ✓	4.217 <	38.000 ✓
107	3.559	0.785	2.682	0.056	6.238 <	38.000 ✓	7.026 <	38.000 ✓	4.400 <	38.000 ✓
108	3.532	0.716	1.561	0.025	6.091 <	38.000 ✓	5.810 <	38.000 ✓	4.274 <	38.000 ✓
109	3.497	0.707	1.772	0.031	6.026 <	38.000 ✓	5.976 <	38.000 ✓	4.235 <	38.000 ✓
110	3.522	0.713	1.808	0.032	6.072 <	38.000 ✓	6.043 <	38.000 ✓	4.267 <	38.000 ✓
111	3.835	0.815	3.483	0.075	6.672 <	38.000 ✓	8.132 <	38.000 ✓	4.724 <	38.000 ✓
112	3.466	0.688	2.407	0.049	5.952 <	38.000 ✓	6.561 <	38.000 ✓	4.203 <	38.000 ✓
113	3.547	0.704	3.111	0.068	6.093 <	38.000 ✓	7.362 <	38.000 ✓	4.320 <	38.000 ✓
114	3.564	0.708	3.111	0.068	6.123 <	38.000 ✓	7.383 <	38.000 ✓	4.341 <	38.000 ✓
116	3.225	0.738	2.052	0.041	5.696 <	38.000 ✓	6.015 <	38.000 ✓	4.004 <	38.000 ✓
117	3.583	0.790	2.748	0.058	6.280 <	38.000 ✓	7.121 <	38.000 ✓	4.431 <	38.000 ✓
118	3.106	0.712	1.533	0.028	5.488 <	38.000 ✓	5.351 <	38.000 ✓	3.846 <	38.000 ✓
119	3.261	0.716	1.233	0.016	5.712 <	38.000 ✓	5.210 <	38.000 ✓	3.993 <	38.000 ✓
120	3.499	0.726	1.342	0.013	6.059 <	38.000 ✓	5.566 <	38.000 ✓	4.238 <	38.000 ✓
121	3.550	0.719	1.401	0.014	6.120 <	38.000 ✓	5.670 <	38.000 ✓	4.283 <	38.000 ✓
122	3.874	0.827	3.482	0.076	6.747 <	38.000 ✓	8.183 <	38.000 ✓	4.777 <	38.000 ✓
123	3.866	0.828	3.394	0.074	6.737 <	38.000 ✓	8.087 <	38.000 ✓	4.767 <	38.000 ✓
124	3.532	0.714	1.333	0.013	6.086 <	38.000 ✓	5.578 <	38.000 ✓	4.259 <	38.000 ✓
125	3.462	0.689	1.731	0.030	5.950 <	38.000 ✓	5.882 <	38.000 ✓	4.182 <	38.000 ✓
126	3.522	0.713	1.805	0.032	6.072 <	38.000 ✓	6.040 <	38.000 ✓	4.267 <	38.000 ✓
128	3.512	0.690	3.111	0.069	6.021 <	38.000 ✓	7.314 <	38.000 ✓	4.271 <	38.000 ✓
129	3.500	0.684	3.002	0.066	5.995 <	38.000 ✓	7.187 <	38.000 ✓	4.250 <	38.000 ✓
130	3.517	0.673	2.408	0.049	6.001 <	38.000 ✓	6.598 <	38.000 ✓	4.239 <	38.000 ✓
132	3.610	0.790	2.844	0.060	6.317 <	38.000 ✓	7.244 <	38.000 ✓	4.460 <	38.000 ✓
133	3.348	0.745	2.208	0.045	5.878 <	38.000 ✓	6.301 <	38.000 ✓	4.137 <	38.000 ✓
134	3.899	0.832	3.556	0.078	6.791 <	38.000 ✓	8.288 <	38.000 ✓	4.810 <	38.000 ✓
135	3.355	0.730	1.749	0.032	5.866 <	38.000 ✓	5.835 <	38.000 ✓	4.117 <	38.000 ✓
136	3.537	0.733	1.346	0.019	6.126 <	38.000 ✓	5.617 <	38.000 ✓	4.290 <	38.000 ✓
137	3.583	0.725	1.303	0.012	6.176 <	38.000 ✓	5.611 <	38.000 ✓	4.320 <	38.000 ✓
138	3.887	0.830	3.506	0.077	6.769 <	38.000 ✓	8.223 <	38.000 ✓	4.793 <	38.000 ✓
139	3.567	0.720	1.235	0.011	6.146 <	38.000 ✓	5.522 <	38.000 ✓	4.298 <	38.000 ✓
140	3.511	0.694	1.152	0.012	6.026 <	38.000 ✓	5.357 <	38.000 ✓	4.217 <	38.000 ✓
141	3.543	0.675	1.729	0.030	6.040 <	38.000 ✓	5.947 <	38.000 ✓	4.248 <	38.000 ✓
142	3.508	0.688	3.111	0.069	6.011 <	38.000 ✓	7.306 <	38.000 ✓	4.264 <	38.000 ✓
143	3.511	0.673	3.103	0.068	5.993 <	38.000 ✓	7.288 <	38.000 ✓	4.253 <	38.000 ✓
144	3.581	0.661	2.729	0.058	6.071 <	38.000 ✓	6.972 <	38.000 ✓	4.300 <	38.000 ✓
145	3.613	0.662	2.397	0.048	6.117 <	38.000 ✓	6.672 <	38.000 ✓	4.323 <	38.000 ✓
146	3.903	0.829	3.650	0.081	6.790 <	38.000 ✓	8.382 <	38.000 ✓	4.812 <	38.000 ✓
147	3.656	0.786	2.982	0.064	6.376 <	38.000 ✓	7.424 <	38.000 ✓	4.506 <	38.000 ✓
148	3.877	0.818	3.638	0.080	6.736 <	38.000 ✓	8.333 <	38.000 ✓	4.775 <	38.000 ✓
149	3.506	0.751	2.414	0.049	6.110 <	38.000 ✓	6.671 <	38.000 ✓	4.306 <	38.000 ✓
151	3.594	0.743	1.991	0.037	6.220 <	38.000 ✓	6.328 <	38.000 ✓	4.374 <	38.000 ✓
152	3.624	0.732	1.452	0.022	6.244 <	38.000 ✓	5.807 <	38.000 ✓	4.377 <	38.000 ✓
153	3.629	0.727	1.481	0.022	6.244 <	38.000 ✓	5.837 <	38.000 ✓	4.379 <	38.000 ✓
154	3.571	0.701	1.052	0.008	6.121 <	38.000 ✓	5.324 <	38.000 ✓	4.280 <	38.000 ✓
155	3.594	0.682	1.064	0.011	6.122 <	38.000 ✓	5.339 <	38.000 ✓	4.287 <	38.000 ✓
156	3.670	0.669	1.709	0.029	6.209 <	38.000 ✓	6.048 <	38.000 ✓	4.368 <	38.000 ✓
157	3.667	0.670	1.712	0.029	6.205 <	38.000 ✓	6.049 <	38.000 ✓	4.365 <	38.000 ✓
158	3.568	0.656	3.083	0.068	6.046 <	38.000 ✓	7.307 <	38.000 ✓	4.292 <	38.000 ✓
161	3.894	0.820	3.749	0.083	6.764 <	38.000 ✓	8.464 <	38.000 ✓	4.798 <	38.000 ✓
162	3.699	0.778	3.142	0.068	6.422 <	38.000 ✓	7.618 <	38.000 ✓	4.544 <	38.000 ✓
163	3.870	0.802	3.893	0.088	6.701 <	38.000 ✓	8.565 <	38.000 ✓	4.760 <	38.000 ✓
164	3.892	0.818	3.766	0.084	6.758 <	38.000 ✓	8.476 <	38.000 ✓	4.794 <	38.000 ✓
165	3.668	0.754	2.652	0.055	6.342 <	38.000 ✓	7.074 <	38.000 ✓	4.477 <	38.000 ✓
166	3.691	0.740	2.114	0.040	6.351 <	38.000 ✓	6.544 <	38.000 ✓	4.470 <	38.000 ✓
168	3.699	0.734	2.141	0.040	6.353 <	38.000 ✓	6.573 <	38.000 ✓	4.473 <	38.000 ✓
169	3.635	0.708	1.527	0.024	6.223 <	38.000 ✓	5.871 <	38.000 ✓	4.368 <	38.000 ✓
170	3.653	0.689	0.929	0.007	6.216 <	38.000 ✓	5.270 <	38.000 ✓	4.349 <	38.000 ✓
171	3.682	0.674	1.444	0.021	6.233 <	38.000 ✓	5.800 <	38.000 ✓	4.378 <	38.000 ✓
172	3.734	0.678	1.023	0.009	6.313 <	38.000 ✓	5.435 <	38.000 ✓	4.422 <	38.000 ✓
174	3.878	0.777	3.937	0.089	6.673 <	38.000 ✓	8.592 <	38.000 ✓	4.744 <	38.000 ✓
175	3.777	0.768	3.333	0.073	6.516 <	38.000 ✓	7.878 <	38.000 ✓	4.617 <	38.000 ✓
177	3.885	0.781	4.026	0.091	6.689 <	38.000 ✓	8.692 <	38.000 ✓	4.758 <	38.000 ✓
178	3.765	0.749	2.777	0.058	6.469 <	38.000 ✓	7.291 <	38.000 ✓	4.571 <	38.000 ✓
179	3.705	0.716	2.189	0.042	6.332 <	38.000 ✓	6.610 <	38.000 ✓	4.463 <	38.000 ✓
180	3.772	0.741	2.804	0.059	6.467 <	38.000 ✓	7.318 <	38.000 ✓	4.572 <	38.000 ✓
181	3.719	0.697	1.610	0.026	6.322 <	38.000 ✓	6.026 <	38.000 ✓	4.442 <	38.000 ✓
182	3.801	0.687	1.039	0.010	6.420 <	38.000 ✓	5.526 <	38.000 ✓	4.498 <	38.000 ✓
183	3.924	0.768	4.111	0.094	6.721 <	38.000 ✓	8.802 <	38.000 ✓	4.785 <	38.000 ✓



ZEMİN GERİLMESİNİN, ZEMİN TAŞIMA GÜCÜ TASARIM GERİLMESİNE GÖRE KONTROLU t/m²

Nokta	G	Q	E	W	1.4 G + 1.6 Q	G + Q + E	G + Q + W
184	3.843	0.758	3.443	0.076	6.593 < 38.000 ✓	8.044 < 38.000 ✓	4.677 < 38.000 ✓
185	3.784	0.725	2.863	0.061	6.457 < 38.000 ✓	7.371 < 38.000 ✓	4.569 < 38.000 ✓
186	3.789	0.706	2.293	0.045	6.434 < 38.000 ✓	6.788 < 38.000 ✓	4.540 < 38.000 ✓
187	3.855	0.749	3.476	0.077	6.595 < 38.000 ✓	8.080 < 38.000 ✓	4.681 < 38.000 ✓
188	3.870	0.696	1.748	0.030	6.532 < 38.000 ✓	6.314 < 38.000 ✓	4.595 < 38.000 ✓
189	3.948	0.759	4.162	0.095	6.742 < 38.000 ✓	8.869 < 38.000 ✓	4.803 < 38.000 ✓
190	3.868	0.716	2.985	0.064	6.561 < 38.000 ✓	7.569 < 38.000 ✓	4.648 < 38.000 ✓
191	3.888	0.737	3.566	0.080	6.622 < 38.000 ✓	8.191 < 38.000 ✓	4.705 < 38.000 ✓
192	3.940	0.706	2.459	0.049	6.646 < 38.000 ✓	7.105 < 38.000 ✓	4.695 < 38.000 ✓
194	4.015	0.752	4.300	0.099	6.825 < 38.000 ✓	9.067 < 38.000 ✓	4.867 < 38.000 ✓
195	4.013	0.716	3.166	0.068	6.763 < 38.000 ✓	7.895 < 38.000 ✓	4.797 < 38.000 ✓
196	3.969	0.729	3.700	0.083	6.724 < 38.000 ✓	8.399 < 38.000 ✓	4.782 < 38.000 ✓
198	4.086	0.744	4.438	0.103	6.911 < 38.000 ✓	9.268 < 38.000 ✓	4.934 < 38.000 ✓
199	4.086	0.726	3.871	0.088	6.882 < 38.000 ✓	8.683 < 38.000 ✓	4.900 < 38.000 ✓
200	4.110	0.732	4.186	0.096	6.925 < 38.000 ✓	9.028 < 38.000 ✓	4.938 < 38.000 ✓
201	4.161	0.736	4.575	0.107	7.003 < 38.000 ✓	9.472 < 38.000 ✓	5.004 < 38.000 ✓
Gz min	2.549	0.645	0.929	0.007	4.602	4.363	3.210
Gz max	4.161	0.832	4.575	0.107	7.003	9.472	5.004
Gz ort	3.475	0.721	2.456	0.047	6.019	6.653	4.244

184 adet

NOKTA DEPLASMANLARI mm

Nokta no	1 g	2 q	3 q	4 q	5 q	6 q	7 q	8 s	9 e	10 e	11 e	12 e	13 w	14 w	17 Ez
1	1.748	0.342	0.193	0.302	0.344	0.215	0.272	-0.402	-1.047	1.215	-1.439	1.533	-0.022	-0.040	1.123
2	1.778	0.354	0.203	0.309	0.345	0.242	0.275	-0.376	-1.002	1.170	-1.398	1.481	-0.021	-0.039	1.140
3	1.810	0.367	0.213	0.317	0.345	0.268	0.279	-0.350	-0.957	1.127	-1.354	1.421	-0.021	-0.038	1.159
4	1.741	0.342	0.195	0.301	0.343	0.215	0.274	-0.390	-1.036	1.167	-1.132	1.204	-0.021	-0.031	1.115
5	1.748	0.344	0.195	0.303	0.344	0.219	0.273	-0.391	-1.034	1.182	-1.272	1.354	-0.021	-0.035	1.121
6	1.736	0.350	0.204	0.305	0.340	0.240	0.275	-0.354	-0.962	1.092	-1.075	1.138	-0.020	-0.030	1.102
8	1.726	0.358	0.214	0.309	0.336	0.264	0.276	-0.318	-0.886	1.014	-1.018	1.070	-0.018	-0.028	1.085
9	1.833	0.376	0.219	0.322	0.345	0.287	0.281	-0.330	-0.924	1.094	-1.320	1.373	-0.020	-0.037	1.172
10	1.735	0.342	0.197	0.300	0.342	0.216	0.276	-0.378	-1.026	1.121	-0.824	0.874	-0.020	-0.023	1.109
11	1.689	0.345	0.206	0.300	0.334	0.238	0.274	-0.333	-0.925	1.016	-0.763	0.806	-0.018	-0.021	1.061
12	1.722	0.367	0.223	0.314	0.333	0.290	0.278	-0.280	-0.809	0.936	-0.962	0.996	-0.017	-0.027	1.070
13	1.618	0.345	0.214	0.299	0.325	0.258	0.272	-0.284	-0.807	0.895	-0.700	0.734	-0.016	-0.019	0.987
14	1.826	0.376	0.220	0.321	0.345	0.287	0.281	-0.326	-0.916	1.080	-1.269	1.320	-0.020	-0.035	1.167
15	1.843	0.380	0.222	0.324	0.345	0.297	0.282	-0.319	-0.907	1.077	-1.303	1.348	-0.020	-0.036	1.178
16	1.733	0.343	0.199	0.300	0.341	0.217	0.278	-0.367	-1.020	1.078	-0.516	0.542	-0.019	-0.014	1.105
17	1.658	0.342	0.207	0.297	0.330	0.237	0.275	-0.317	-0.899	0.954	-0.464	0.488	-0.017	-0.013	1.031
18	1.719	0.371	0.229	0.316	0.330	0.306	0.278	-0.253	-0.755	0.882	-0.927	0.947	-0.016	-0.026	1.061
19	1.563	0.347	0.222	0.300	0.318	0.277	0.272	-0.241	-0.706	0.792	-0.650	0.674	-0.014	-0.018	0.928
20	1.538	0.336	0.215	0.293	0.317	0.254	0.270	-0.258	-0.750	0.802	-0.411	0.430	-0.014	-0.011	0.913
21	1.861	0.387	0.228	0.328	0.343	0.315	0.283	-0.296	-0.868	1.039	-1.270	1.295	-0.019	-0.035	1.188
22	1.734	0.345	0.201	0.300	0.341	0.219	0.280	-0.358	-1.017	1.039	-0.205	0.208	-0.018	-0.006	1.105
23	1.644	0.342	0.209	0.296	0.329	0.238	0.276	-0.305	-0.887	0.907	-0.174	0.177	-0.016	-0.005	1.017
24	1.531	0.349	0.229	0.301	0.313	0.293	0.271	-0.206	-0.625	0.710	-0.612	0.625	-0.013	-0.017	0.889
25	1.726	0.376	0.234	0.319	0.326	0.322	0.279	-0.226	-0.704	0.831	-0.900	0.903	-0.015	-0.025	1.061
26	1.441	0.332	0.224	0.290	0.307	0.269	0.268	-0.208	-0.621	0.671	-0.370	0.383	-0.012	-0.010	0.814
27	1.499	0.332	0.217	0.289	0.313	0.252	0.270	-0.242	-0.721	0.740	-0.143	0.146	-0.013	-0.004	0.876
28	1.874	0.392	0.232	0.331	0.338	0.332	0.283	-0.269	-0.820	0.992	-1.241	1.245	-0.018	-0.035	1.193
30	1.738	0.346	0.204	0.299	0.341	0.220	0.283	-0.350	-1.018	1.004	0.107	-0.129	-0.018	0.003	1.107
32	1.649	0.344	0.212	0.296	0.328	0.240	0.279	-0.297	-0.888	0.874	0.115	-0.133	-0.015	0.003	1.020
33	1.521	0.351	0.234	0.303	0.308	0.308	0.271	-0.176	-0.562	0.647	-0.586	0.586	-0.012	-0.016	0.873
34	1.380	0.331	0.230	0.290	0.300	0.283	0.267	-0.168	-0.524	0.572	-0.340	0.346	-0.010	-0.010	0.749
35	1.730	0.377	0.237	0.320	0.319	0.336	0.277	-0.194	-0.644	0.771	-0.879	0.862	-0.014	-0.025	1.059
36	1.867	0.392	0.234	0.331	0.335	0.338	0.283	-0.252	-0.786	0.951	-1.180	1.174	-0.018	-0.033	1.185
37	1.378	0.326	0.225	0.285	0.301	0.266	0.267	-0.187	-0.578	0.595	-0.120	0.121	-0.011	-0.003	0.755
38	1.504	0.334	0.220	0.289	0.313	0.254	0.273	-0.235	-0.722	0.709	0.118	-0.131	-0.012	0.003	0.879
39	1.876	0.393	0.234	0.332	0.336	0.338	0.282	-0.257	-0.798	0.969	-1.231	1.226	-0.018	-0.034	1.194
40	1.746	0.349	0.206	0.300	0.341	0.223	0.286	-0.344	-1.024	0.973	0.418	-0.464	-0.017	0.012	1.112
41	1.671	0.348	0.215	0.297	0.330	0.243	0.282	-0.294	-0.902	0.854	0.407	-0.444	-0.015	0.011	1.039
42	1.358	0.332	0.236	0.291	0.295	0.297	0.266	-0.138	-0.456	0.503	-0.319	0.317	-0.009	-0.009	0.722
43	1.531	0.353	0.238	0.304	0.303	0.321	0.271	-0.150	-0.513	0.597	-0.569	0.556	-0.011	-0.016	0.877
44	1.302	0.323	0.232	0.284	0.293	0.279	0.265	-0.145	-0.470	0.487	-0.101	0.101	-0.009	-0.003	0.676
45	1.734	0.375	0.238	0.318	0.311	0.345	0.275	-0.165	-0.588	0.714	-0.872	0.835	-0.013	-0.024	1.060
46	1.876	0.392	0.235	0.332	0.331	0.347	0.281	-0.235	-0.757	0.929	-1.219	1.196	-0.017	-0.034	1.191
47	1.384	0.327	0.228	0.285	0.301	0.268	0.269	-0.180	-0.578	0.565	0.123	-0.131	-0.010	0.003	0.759
48	1.553	0.342	0.223	0.292	0.317	0.259	0.278	-0.236	-0.752	0.706	0.389	-0.417	-0.012	0.011	0.923
49	1.757	0.352	0.209	0.300	0.341	0.225	0.289	-0.338	-1.032	0.946	0.726	-0.795	-0.016	0.020	1.120
50	1.712	0.355	0.218	0.300	0.333	0.247	0.287	-0.294	-0.929	0.845	0.707	-0.764	-0.014	0.020	1.074
51	1.373	0.335	0.239	0.292	0.291	0.309	0.267	-0.114	-0.411	0.459	-0.303	0.294	-0.008	-0.009	0.730
52	1.274	0.323	0.238	0.284	0.288	0.291	0.265	-0.114	-0.398	0.414	-0.084	0.082	-0.007	-0.002	0.642
53	1.560	0.355	0.240	0.304	0.297	0.331	0.270	-0.127	-0.474	0.558	-0.562	0.536	-0.010	-0.016	0.901
54	1.309	0.325	0.235	0.284	0.293	0.281	0.268	-0.138	-0.470	0.457	0.130	-0.135	-0.008	0.004	0.680
55	1.746	0.372	0.239	0.314	0.302	0.352	0.271	-0.137	-0.534	0.660	-0.875	0.821	-0.013	-0.024	1.069
56	1.868	0.389	0.236	0.329	0.322	0.355	0.277	-0.202	-0.692	0.863	-1.210	1.163	-0.016	-0.034	1.180
57	1.845	0.383	0.237	0.323	0.311	0.359	0.273	-0.168	-0.619	0.781	-1.157	1.094	-0.015	-0.032	1.159
59	1.458	0.338	0.231	0.290	0.306	0.275	0.275	-0.186	-0.622	0.577	0.378	-0.397	-0.010	0.010	0.826

FİRMA : ESPO MUH. DAN. INS. LTD. STI.

30-09-2025

SAYFA: 77

PROJE : CERRAHPAŞA YURT SU DEPOSU

(250929-ES374-CERRAH-SU-D-D04.ST4)

NOKTA DEPLASMANLARI mm

Nokta no	1 g	2 q	3 q	4 q	5 q	6 q	7 q	8 s	9 e	10 e	11 e	12 e	13 w	14 w	17 Ez
60	1.643	0.355	0.227	0.299	0.324	0.267	0.285	-0.246	-0.810	0.728	0.682	-0.725	-0.012	0.019	1.003
61	1.771	0.355	0.212	0.301	0.342	0.228	0.292	-0.334	-1.044	0.921	1.034	-1.125	-0.016	0.029	1.131
62	1.768	0.364	0.222	0.304	0.338	0.253	0.293	-0.298	-0.968	0.846	1.020	-1.098	-0.014	0.028	1.121
63	1.293	0.327	0.242	0.286	0.284	0.304	0.266	-0.092	-0.356	0.372	-0.068	0.064	-0.007	-0.002	0.654
64	1.426	0.340	0.242	0.294	0.287	0.321	0.268	-0.096	-0.386	0.434	-0.293	0.276	-0.008	-0.008	0.775
65	1.282	0.325	0.241	0.284	0.287	0.293	0.268	-0.107	-0.396	0.383	0.142	-0.144	-0.007	0.004	0.648
66	1.611	0.357	0.241	0.303	0.292	0.341	0.269	-0.106	-0.443	0.529	-0.565	0.525	-0.010	-0.016	0.946
67	1.400	0.337	0.238	0.289	0.299	0.289	0.275	-0.146	-0.521	0.477	0.378	-0.388	-0.008	0.010	0.764
68	1.751	0.365	0.239	0.307	0.291	0.354	0.266	-0.107	-0.475	0.601	-0.883	0.812	-0.012	-0.025	1.075
69	1.853	0.383	0.236	0.324	0.312	0.359	0.273	-0.173	-0.630	0.799	-1.209	1.143	-0.015	-0.034	1.166
70	1.850	0.382	0.236	0.323	0.310	0.359	0.272	-0.168	-0.620	0.789	-1.210	1.141	-0.015	-0.034	1.164
71	1.593	0.357	0.236	0.299	0.317	0.286	0.285	-0.203	-0.705	0.625	0.667	-0.696	-0.011	0.018	0.947
72	1.762	0.372	0.232	0.308	0.335	0.277	0.296	-0.262	-0.887	0.767	1.005	-1.065	-0.013	0.028	1.107
73	1.786	0.358	0.215	0.302	0.343	0.231	0.295	-0.330	-1.058	0.898	1.341	-1.455	-0.015	0.037	1.143
74	1.782	0.358	0.215	0.302	0.343	0.233	0.294	-0.328	-1.043	0.902	1.181	-1.281	-0.015	0.033	1.139
75	1.819	0.372	0.226	0.308	0.343	0.258	0.300	-0.302	-1.006	0.846	1.344	-1.441	-0.014	0.037	1.163
76	1.302	0.329	0.245	0.285	0.283	0.306	0.270	-0.084	-0.352	0.339	0.161	-0.159	-0.006	0.004	0.661
77	1.359	0.334	0.245	0.288	0.282	0.317	0.268	-0.076	-0.337	0.353	-0.051	0.044	-0.006	-0.001	0.711
78	1.514	0.347	0.245	0.295	0.284	0.334	0.269	-0.080	-0.375	0.424	-0.287	0.263	-0.008	-0.008	0.854
79	1.382	0.339	0.244	0.289	0.293	0.303	0.276	-0.114	-0.449	0.405	0.388	-0.388	-0.007	0.011	0.739
80	1.675	0.358	0.242	0.300	0.285	0.349	0.268	-0.084	-0.413	0.501	-0.574	0.522	-0.010	-0.016	1.005
81	1.564	0.359	0.243	0.300	0.311	0.303	0.286	-0.166	-0.618	0.539	0.664	-0.678	-0.009	0.018	0.913
82	1.759	0.358	0.239	0.298	0.279	0.355	0.262	-0.076	-0.413	0.540	-0.894	0.810	-0.011	-0.025	1.084
83	1.826	0.372	0.236	0.314	0.297	0.359	0.266	-0.133	-0.544	0.712	-1.214	1.125	-0.014	-0.034	1.142
85	1.764	0.382	0.243	0.311	0.330	0.304	0.299	-0.221	-0.801	0.681	0.996	-1.033	-0.012	0.028	1.098
86	1.855	0.385	0.237	0.314	0.343	0.285	0.305	-0.273	-0.953	0.792	1.344	-1.419	-0.013	0.037	1.186
87	1.874	0.394	0.245	0.318	0.341	0.305	0.307	-0.250	-0.904	0.749	1.293	-1.347	-0.013	0.036	1.197
89	1.400	0.343	0.249	0.290	0.288	0.316	0.277	-0.090	-0.399	0.355	0.409	-0.400	-0.006	0.011	0.752
90	1.370	0.336	0.249	0.287	0.280	0.319	0.272	-0.067	-0.331	0.317	0.188	-0.182	-0.006	0.005	0.720
91	1.470	0.344	0.249	0.290	0.279	0.332	0.271	-0.063	-0.335	0.353	-0.029	0.021	-0.006	-0.001	0.812
92	1.629	0.355	0.247	0.295	0.280	0.347	0.270	-0.065	-0.369	0.420	-0.284	0.253	-0.008	-0.008	0.961
93	1.560	0.363	0.250	0.300	0.305	0.319	0.288	-0.134	-0.547	0.468	0.675	-0.673	-0.008	0.019	0.903
94	1.739	0.358	0.244	0.294	0.275	0.355	0.266	-0.059	-0.375	0.465	-0.582	0.523	-0.009	-0.016	1.065
95	1.766	0.387	0.250	0.313	0.326	0.321	0.301	-0.192	-0.739	0.619	0.997	-1.015	-0.010	0.028	1.094
96	1.750	0.346	0.240	0.284	0.263	0.352	0.257	-0.043	-0.336	0.464	-0.890	0.799	-0.009	-0.025	1.080
97	1.799	0.360	0.235	0.302	0.283	0.356	0.259	-0.097	-0.466	0.632	-1.220	1.113	-0.012	-0.034	1.119
98	1.791	0.358	0.236	0.301	0.280	0.356	0.259	-0.089	-0.448	0.608	-1.170	1.064	-0.012	-0.033	1.112
99	1.759	0.352	0.241	0.291	0.270	0.355	0.259	-0.054	-0.362	0.487	-0.867	0.780	-0.010	-0.024	1.085
100	1.894	0.399	0.249	0.320	0.340	0.315	0.310	-0.239	-0.888	0.727	1.345	-1.391	-0.012	0.037	1.212
101	1.881	0.395	0.245	0.318	0.341	0.305	0.308	-0.251	-0.911	0.750	1.344	-1.400	-0.013	0.037	1.204
102	1.575	0.366	0.255	0.300	0.298	0.332	0.289	-0.106	-0.488	0.409	0.700	-0.682	-0.007	0.019	0.913
103	1.458	0.348	0.253	0.290	0.284	0.328	0.279	-0.069	-0.366	0.322	0.446	-0.426	-0.006	0.012	0.802
104	1.484	0.346	0.253	0.289	0.278	0.334	0.276	-0.053	-0.327	0.313	0.227	-0.217	-0.006	0.006	0.824
105	1.614	0.355	0.252	0.292	0.277	0.347	0.275	-0.050	-0.340	0.359	-0.002	-0.005	-0.007	0.000	0.945
106	1.741	0.360	0.250	0.292	0.273	0.357	0.271	-0.045	-0.350	0.405	-0.276	0.244	-0.008	-0.008	1.065
107	1.779	0.392	0.257	0.314	0.321	0.338	0.303	-0.162	-0.676	0.557	1.011	-1.007	-0.009	0.028	1.101
108	1.766	0.357	0.248	0.289	0.269	0.358	0.267	-0.040	-0.339	0.416	-0.453	0.406	-0.008	-0.013	1.091
109	1.748	0.349	0.246	0.281	0.260	0.353	0.262	-0.027	-0.304	0.395	-0.563	0.506	-0.008	-0.016	1.079
110	1.761	0.355	0.246	0.288	0.268	0.357	0.264	-0.041	-0.338	0.430	-0.578	0.519	-0.008	-0.016	1.087
111	1.917	0.407	0.257	0.323	0.337	0.334	0.313	-0.212	-0.836	0.674	1.352	-1.373	-0.011	0.037	1.228
112	1.733	0.332	0.241	0.266	0.244	0.344	0.251	-0.009	-0.255	0.381	-0.882	0.787	-0.008	-0.025	1.071
113	1.773	0.347	0.235	0.289	0.267	0.352	0.252	-0.061	-0.384	0.550	-1.226	1.103	-0.011	-0.034	1.099
114	1.782	0.352	0.235	0.294	0.273	0.354	0.255	-0.074	-0.415	0.581	-1.224	1.106	-0.012	-0.034	1.106
116	1.613	0.369	0.259	0.298	0.291	0.344	0.290	-0.079	-0.436	0.357	0.742	-0.707	-0.006	0.021	0.945
117	1.791	0.395	0.263	0.313	0.312	0.353	0.304	-0.127	-0.599	0.480	1.041	-1.012	-0.008	0.029	1.108
118	1.553	0.356	0.258	0.290	0.279	0.342	0.282	-0.051	-0.347	0.302	0.500	-0.469	-0.005	0.014	0.889
119	1.631	0.358	0.257	0.289	0.275	0.350	0.280	-0.039	-0.328	0.314	0.281	-0.263	-0.006	0.008	0.960
120	1.749	0.363	0.256	0.288	0.270	0.360	0.277	-0.032	-0.329	0.349	0.034	-0.036	-0.007	0.001	1.073
121	1.775	0.358	0.251	0.285	0.264	0.359	0								

FİRMA : ESPO MUH. DAN. INS. LTD. STI.

30-09-2025

SAYFA: 78

PROJE : CERRAHPAŞA YURT SU DEPOSU

(250929-ES374-CERRAH-SU-D-D04.ST4)

NOKTA DEPLASMANLARI mm

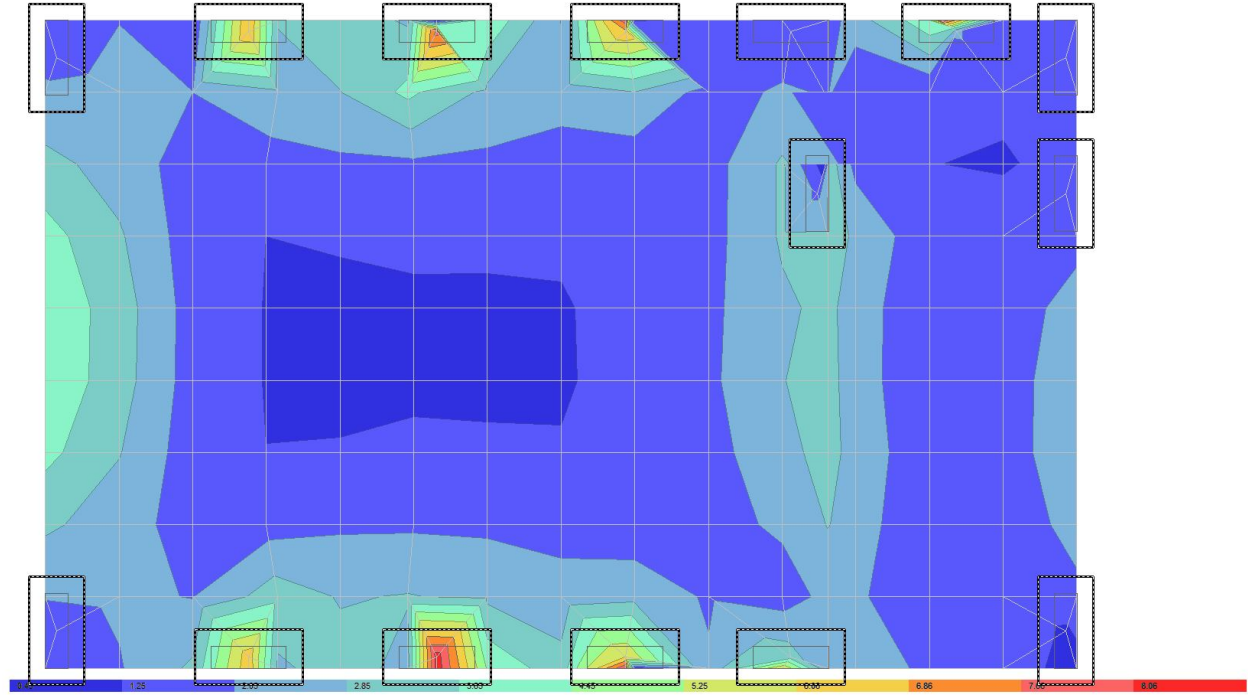
Nokta no	1 g	2 q	3 q	4 q	5 q	6 q	7 q	8 s	9 e	10 e	11 e	12 e	13 w	14 w	17 Ez
148	1.938	0.409	0.278	0.307	0.296	0.382	0.315	-0.068	-0.506	0.353	1.447	-1.352	-0.006	0.040	1.240
149	1.753	0.376	0.268	0.289	0.274	0.364	0.294	-0.028	-0.350	0.269	0.884	-0.812	-0.005	0.025	1.076
151	1.797	0.371	0.267	0.283	0.265	0.367	0.289	-0.009	-0.304	0.256	0.660	-0.600	-0.004	0.018	1.118
152	1.812	0.366	0.263	0.279	0.259	0.366	0.283	-0.002	-0.279	0.265	0.386	-0.347	-0.005	0.011	1.135
153	1.803	0.361	0.264	0.272	0.252	0.363	0.281	0.011	-0.246	0.233	0.401	-0.357	-0.004	0.011	1.130
154	1.754	0.340	0.258	0.255	0.235	0.351	0.269	0.032	-0.177	0.198	0.106	-0.090	-0.004	0.003	1.094
155	1.745	0.323	0.254	0.239	0.218	0.341	0.259	0.052	-0.117	0.173	-0.204	0.186	-0.004	-0.006	1.092
156	1.760	0.310	0.252	0.224	0.203	0.335	0.250	0.074	-0.058	0.151	-0.522	0.469	-0.004	-0.014	1.110
157	1.760	0.310	0.252	0.225	0.203	0.335	0.250	0.073	-0.061	0.154	-0.523	0.470	-0.004	-0.015	1.109
158	1.737	0.302	0.239	0.232	0.210	0.328	0.237	0.047	-0.124	0.289	-1.216	1.076	-0.007	-0.034	1.085
161	1.947	0.410	0.278	0.307	0.296	0.383	0.316	-0.067	-0.510	0.351	1.500	-1.402	-0.006	0.042	1.248
162	1.849	0.389	0.274	0.292	0.276	0.374	0.303	-0.025	-0.375	0.257	1.222	-1.120	-0.004	0.034	1.164
163	1.935	0.401	0.282	0.293	0.278	0.384	0.313	-0.021	-0.397	0.240	1.574	-1.443	-0.004	0.044	1.241
164	1.946	0.409	0.279	0.306	0.294	0.383	0.316	-0.062	-0.497	0.338	1.509	-1.406	-0.005	0.042	1.247
165	1.834	0.377	0.272	0.281	0.263	0.371	0.296	0.000	-0.299	0.216	0.980	-0.888	-0.004	0.027	1.153
166	1.835	0.370	0.269	0.276	0.257	0.369	0.289	0.010	-0.266	0.216	0.710	-0.638	-0.004	0.020	1.156
168	1.826	0.365	0.270	0.269	0.250	0.367	0.287	0.023	-0.232	0.183	0.725	-0.647	-0.003	0.020	1.151
169	1.773	0.345	0.264	0.253	0.232	0.354	0.275	0.044	-0.159	0.146	0.430	-0.377	-0.003	0.012	1.112
170	1.761	0.328	0.260	0.236	0.215	0.345	0.265	0.065	-0.095	0.117	0.132	-0.110	-0.003	0.004	1.108
171	1.767	0.313	0.255	0.226	0.204	0.337	0.254	0.074	-0.062	0.140	-0.388	0.350	-0.003	-0.011	1.115
172	1.779	0.314	0.259	0.222	0.200	0.339	0.257	0.088	-0.034	0.091	-0.173	0.164	-0.002	-0.005	1.127
174	1.917	0.389	0.285	0.277	0.259	0.382	0.309	0.022	-0.285	0.135	1.599	-1.444	-0.002	0.045	1.230
175	1.879	0.384	0.279	0.280	0.262	0.377	0.303	0.009	-0.298	0.179	1.308	-1.184	-0.003	0.036	1.195
177	1.924	0.391	0.285	0.278	0.260	0.383	0.310	0.019	-0.296	0.140	1.642	-1.485	-0.002	0.046	1.236
178	1.861	0.374	0.275	0.273	0.254	0.373	0.295	0.022	-0.254	0.169	1.034	-0.929	-0.003	0.029	1.181
179	1.795	0.349	0.270	0.250	0.230	0.358	0.281	0.057	-0.142	0.095	0.755	-0.665	-0.002	0.021	1.133
180	1.851	0.369	0.276	0.266	0.247	0.371	0.293	0.035	-0.219	0.135	1.050	-0.938	-0.002	0.029	1.175
181	1.780	0.332	0.266	0.234	0.213	0.349	0.271	0.079	-0.075	0.062	0.467	-0.404	-0.001	0.013	1.126
182	1.798	0.319	0.265	0.219	0.198	0.343	0.264	0.102	-0.010	0.033	0.176	-0.141	-0.001	0.005	1.146
183	1.919	0.384	0.287	0.268	0.249	0.381	0.308	0.043	-0.234	0.079	1.685	-1.513	-0.001	0.047	1.235
184	1.889	0.379	0.281	0.270	0.252	0.377	0.302	0.033	-0.243	0.123	1.359	-1.220	-0.002	0.038	1.207
185	1.822	0.354	0.276	0.247	0.227	0.362	0.288	0.070	-0.127	0.045	1.084	-0.958	-0.001	0.030	1.158
186	1.802	0.337	0.273	0.231	0.211	0.353	0.278	0.092	-0.055	0.008	0.803	-0.700	0.000	0.022	1.147
187	1.881	0.374	0.282	0.264	0.244	0.375	0.300	0.046	-0.208	0.089	1.377	-1.231	-0.001	0.038	1.203
188	1.818	0.324	0.272	0.217	0.195	0.348	0.271	0.116	0.012	-0.025	0.525	-0.447	0.000	0.015	1.165
189	1.916	0.380	0.288	0.261	0.242	0.380	0.307	0.058	-0.198	0.043	1.710	-1.530	0.000	0.048	1.235
190	1.828	0.343	0.279	0.229	0.208	0.358	0.285	0.106	-0.038	-0.044	1.141	-0.998	0.001	0.032	1.171
191	1.862	0.360	0.283	0.245	0.225	0.368	0.295	0.083	-0.113	-0.004	1.425	-1.261	0.000	0.040	1.194
192	1.840	0.330	0.278	0.215	0.193	0.353	0.278	0.131	0.033	-0.081	0.874	-0.753	0.001	0.025	1.184
194	1.912	0.369	0.291	0.244	0.224	0.376	0.304	0.096	-0.101	-0.053	1.779	-1.575	0.002	0.050	1.237
195	1.862	0.335	0.285	0.213	0.191	0.358	0.285	0.145	0.053	-0.136	1.222	-1.058	0.003	0.034	1.205
196	1.865	0.349	0.286	0.228	0.207	0.365	0.293	0.120	-0.021	-0.096	1.489	-1.305	0.002	0.042	1.203
198	1.909	0.357	0.295	0.227	0.205	0.372	0.301	0.134	-0.006	-0.148	1.847	-1.621	0.003	0.052	1.242
199	1.885	0.340	0.291	0.211	0.189	0.363	0.292	0.158	0.072	-0.190	1.568	-1.362	0.004	0.044	1.226
200	1.896	0.345	0.294	0.213	0.190	0.366	0.295	0.159	0.066	-0.201	1.723	-1.500	0.004	0.048	1.235
201	1.908	0.346	0.298	0.209	0.187	0.368	0.298	0.172	0.091	-0.244	1.913	-1.665	0.005	0.054	1.248

TEMEL KİRİŞ STATİK SONUÇLARI

Temel Nokta no	1 g	2 q	3 q	4 q	5 q	6 q	7 q	8 s	9 e	10 e	11 e	12 e	13 w	14 w	17 Ez

RADYE TEMEL KOLON ZİMBALAMA HESABI

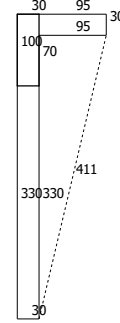
Deprem tesirleri, D=3 ile çarpılmaktadır.



SmaxV gerilmesi :8.11(kg/cm²) < fctd=13.79(kg/cm²)
Maksimum zimbalama gerilmesi, fctd kesme dayanımından küçüktür.

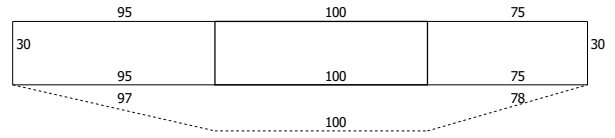
S101

d= 43 cm Ac =1.767m² $\Phi_x=0, \Phi_y=0$
 Ex =77.45 cm Ey =230.0 cm
 Ix = 0.581684 m⁴ Iy = 2.449195 m⁴
 Up = 411.13 cm fctd=137.94 t/m²
 Mx = 0.02 (tm) My = 1.15 (tm)
 Xt= 47.5 cm Yx=0.928 Yt= 200 cm Yy=0.955
 Vd = 11.03/ 11.03 (t) Vdq =4.3 (t) zemin
 Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
 Panel ara başlıklarında zimbalama kontrolu yapılmayabilir.



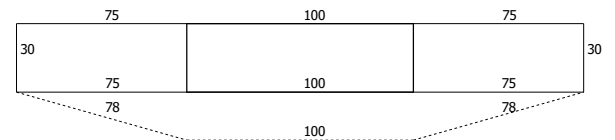
S102

d= 43 cm Ac =1.184m² $\Phi_x=0, \Phi_y=0$
 Ex =-9.72 cm Ey =44.57 cm
 Ix = 0.746549 m⁴ Iy = 0.017969 m⁴
 Up = 275.45 cm fctd=137.94 t/m²
 Mx = 0.12 (tm) My = 2.06 (tm)
 Xt= 135.33 cm Yx=1.0 Yt= 6.83 cm Yy=0.953
 Vd = 58.66/ 58.66 (t) Vdq =2.4 (t) zemin
 Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
 Panel ara başlıklarında zimbalama kontrolu yapılmayabilir.



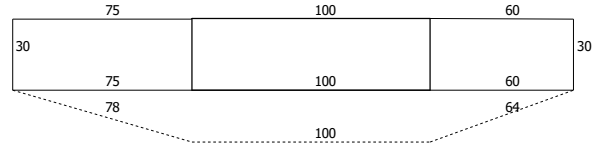
S103

d= 43 cm Ac =1.100m² $\Phi_x=0, \Phi_y=0$
 Ex = 0.00 cm Ey =44.86 cm
 Ix = 0.598729 m⁴ Iy = 0.015212 m⁴
 Up = 256.01 cm fctd=137.94 t/m²
 Mx = 0.02 (tm) My = 2.54 (tm)
 Xt= 124.99 cm Yx=1.0 Yt= 6.53 cm Yy=0.952
 Vd = 67.91/ 67.91 (t) Vdq =4.5 (t) zemin
 Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
 Panel ara başlıklarında zimbalama kontrolu yapılmayabilir.



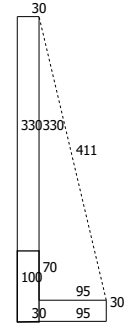
S104

d= 43 cm Ac =1.039m² $\Phi x=0, \Phi y=0$
 Ex =-7.13 cm Ey =45.11 cm
 Ix = 0.503635 m⁴ Iy = 0.013547 m⁴
 Up = 241.77 cm fctd=137.94 t/m²
 Mx = 0.11 (tm) My = 1.88 (tm)
 Xt= 117.87 cm Yx=1.0 Yt= 6.28 cm Yy=0.95
 Vd = 51.15/ 51.15 (t) Vdq =4.3 (t) zemin
 Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
 Panel ara başlıklarında zımbalama kontrolü yapılmayabilir.



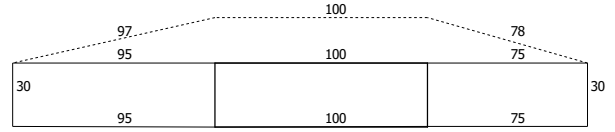
S110

d= 43 cm Ac =1.767m² $\Phi x=0, \Phi y=0$
 Ex =77.45 cm Ey =-230. cm
 Ix = 0.581684 m⁴ Iy = 2.449194 m⁴
 Up = 411.13 cm fctd=137.94 t/m²
 Mx = 0.02 (tm) My = 1.17 (tm)
 Xt= 47.5 cm Yx=0.925 Yt= 200 cm Yy=0.955
 Vd = 13.51/ 13.51 (t) Vdq =2.0 (t) zemin
 Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
 Panel ara başlıklarında zımbalama kontrolü yapılmayabilir.



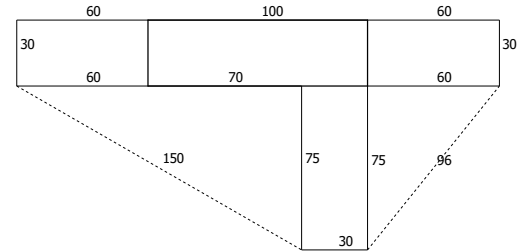
S111

d= 43 cm Ac =1.184m² $\Phi x=0, \Phi y=0$
 Ex =-9.72 cm Ey =-44.5 cm
 Ix = 0.746549 m⁴ Iy = 0.017969 m⁴
 Up = 275.45 cm fctd=137.94 t/m²
 Mx = 0.13 (tm) My = 2.06 (tm)
 Xt= 134.71 cm Yx=1.0 Yt= 6.83 cm Yy=0.953
 Vd = 58.11/ 58.11 (t) Vdq =2.4 (t) zemin
 Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
 Panel ara başlıklarında zımbalama kontrolü yapılmayabilir.



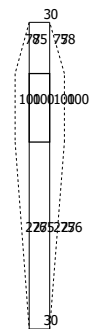
S105

d= 43 cm Ac =1.058m² $\Phi x=0, \Phi y=0$
 Ex =-46.1 cm Ey =67.43 cm
 Ix = 0.530812 m⁴ Iy = 0.095191 m⁴
 Up = 246.11 cm fctd=137.94 t/m²
 Mx = 0.03 (tm) My = 0.14 (tm)
 Xt= 113.79 cm Yx=0.997 Yt= 37.54 cm Yy=0.95
 Vd = 1.51/ 1.51 (t) Vdq =2.6 (t) zemin
 Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
 Panel ara başlıklarında zımbalama kontrolü yapılmayabilir.



S108

d= 43 cm Ac =3.903m² $\Phi x=0, \Phi y=0$
 Ex =-14.9 cm Ey =148.8 cm
 Ix = 0.448748 m⁴ Iy = 6.700532 m⁴
 Up = 907.83 cm fctd=137.94 t/m²
 Mx = 0.06 (tm) My = 0.30 (tm)
 Xt= 36.47 cm Yx=0.981 Yt= 226.11 cm Yy=0.996
 Vd = 9.88/ 9.88 (t) Vdq =7.6 (t) zemin
 Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
 Panel ara başlıklarında zımbalama kontrolü yapılmayabilir.



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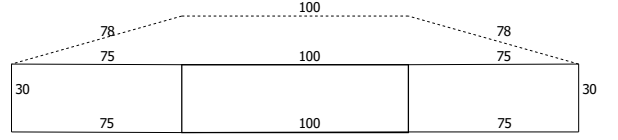
SAYFA: 81

PROJE : CERRAHPAŞA YURT SU DEPOSU

(250929-ES374-CERRAH-SU-D-D04.ST4)

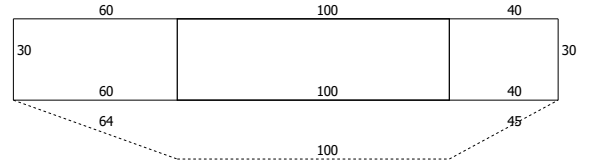
S112

d= 43 cm Ac =1.100m² $\Phi_x=0$, $\Phi_y=0$
 Ex = 0.00 cm Ey =-44.8 cm
 Ix = 0.598729 m⁴ Iy = 0.015212 m⁴
 Up = 256.01 cm fctd=137.94 t/m²
 Mx = 0.01 (tm) My = 2.54 (tm)
 Xt= 124.99 cm Yx=1.0 Yt= 6.53 cm Yy=0.952
 Vd = 68.67/ 68.67 (t) Vdq =3.4 (t) zemin
 Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
 Panel ara başlıklarında zımbalama kontrolü yapılmayabilir.



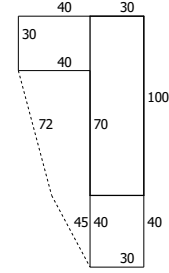
S106

d= 43 cm Ac =0.899m² $\Phi_x=0$, $\Phi_y=0$
 Ex =10.86 cm Ey =45.80 cm
 Ix = 0.324149 m⁴ Iy = 0.010127 m⁴
 Up = 209.10 cm fctd=137.94 t/m²
 Mx = 0.02 (tm) My = 0.12 (tm)
 Xt= 100.81 cm Yx=1.0 Yt= 5.59 cm Yy=0.978
 Vd = 6.31/ 6.31 (t) Vdq =3.7 (t) zemin
 Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
 Panel ara başlıklarında zımbalama kontrolü yapılmayabilir.



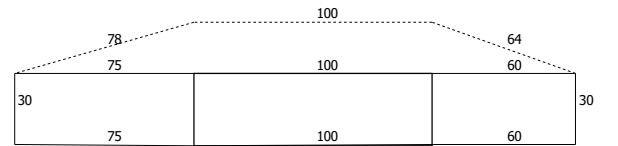
S107

d= 43 cm Ac =0.506m² $\Phi_x=0$, $\Phi_y=0$
 Ex =-52.9 cm Ey =86.15 cm
 Ix = 0.012529 m⁴ Iy = 0.059557 m⁴
 Up = 117.73 cm fctd=137.94 t/m²
 Mx = 0.00 (tm) My = 0.71 (tm)
 Xt= 16.99 cm Yx=0.906 Yt= 13.75 cm Yy=0.839
 Vd = 9.64/ 9.64 (t) Vdq =2.3 (t) zemin
 Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
 Panel ara başlıklarında zımbalama kontrolü yapılmayabilir.



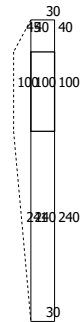
S113

d= 43 cm Ac =1.039m² $\Phi_x=0$, $\Phi_y=0$
 Ex =-7.13 cm Ey =-45.1 cm
 Ix = 0.503635 m⁴ Iy = 0.013547 m⁴
 Up = 241.77 cm fctd=137.94 t/m²
 Mx = 0.14 (tm) My = 1.88 (tm)
 Xt= 117.17 cm Yx=1.0 Yt= 6.28 cm Yy=0.951
 Vd = 52.63/ 52.63 (t) Vdq =4.3 (t) zemin
 Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
 Panel ara başlıklarında zımbalama kontrolü yapılmayabilir.



S109

d= 43 cm Ac =1.661m² $\Phi_x=0$, $\Phi_y=0$
 Ex =-43.4 cm Ey =147.7 cm
 Ix = 0.052890 m⁴ Iy = 2.066133 m⁴
 Up = 386.47 cm fctd=137.94 t/m²
 Mx = 0.21 (tm) My = 0.08 (tm)
 Xt= 7.96 cm Yx=0.979 Yt= 47.84 cm Yy=0.998
 Vd = 10.51/ 10.51 (t) Vdq =5.0 (t) zemin
 Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
 Panel ara başlıklarında zımbalama kontrolü yapılmayabilir.



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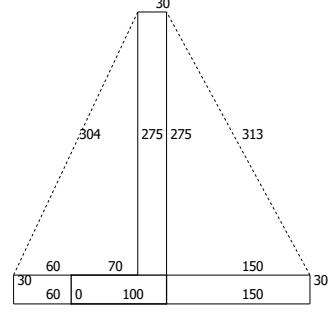
SAYFA: 82

PROJE : CERRAHPAŞA YURT SU DEPOSU

(250929-ES374-CERRAH-SU-D-D04.ST4)

S114

d= 43 cm Ac =2.655m² $\Phi x=0, \Phi y=0$
Ex =-8.68 cm Ey =-167. cm
Ix = 2.895716 m⁴ Iy = 1.915890 m⁴
Up = 617.52 cm fctd=137.94 t/m²
Mx = 0.09 (tm) My = 0.14 (tm)
Xt= 158.78 cm Yx=0.976 Yt= 137.46 cm Yy=0.976
Vd = -1.80/ -1.80 (t) Vdq =11.2 (t) zemin
Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
Panel ara başlıklarında zımbalama kontrolü yapılmayabilir.



S115

d= 43 cm Ac =1.480m² $\Phi x=0, \Phi y=0$
Ex =-104. cm Ey =-185. cm
Ix = 0.647413 m⁴ Iy = 1.337988 m⁴
Up = 344.38 cm fctd=137.94 t/m²
Mx = 0.00 (tm) My = 0.68 (tm)
Xt= 75 cm Yx=0.964 Yt= 155 cm Yy=0.969
Vd = 13.03/ 13.03 (t) Vdq =6.1 (t) zemin
Vp = Y · fctd · Up · d > Vd, Vd = Vdc - Vdq
Panel ara başlıklarında zımbalama kontrolü yapılmayabilir.

